# Chapter 6

## Results

This chapter presents two main results obtained regarding the model. First a validation through a synthetic example is developed. Then using a pair of angiographic image sequences the model is built and measurements are made on different vessel parameters like velocity, shape change, etc.

## 6.1 Experimental Results

### Results of the vessel detection process using the contrast coherence learning.

To illustrate the viability of the *eigensnakes*, a real application of detecting coronary vessels in angiographies is considered. The approach is tested on 23 images and 5 different vessels. Using five scales for the filters with parameter  $\rho = 9...13$  and the following derivatives (up to third degree)

$$\left(\frac{d}{dx},\frac{d}{dy}\right), \left(\frac{d^2}{dx^2},\frac{d^2}{dy^2}\right), \left(\frac{d^2}{dxdy},\frac{d^2}{dydx}\right), \left(\frac{d^3}{dx^3},\frac{d^3}{dy^3}\right) and \left(\frac{d^3}{dxdxdy},\frac{d^3}{dydxdx}\right)$$

together with 5.12 we obtain 25 outputs per pixel. Adding the original image pixel the sampling dimension is 26. 130 points are learned, a data matrix  $D_{m \times n}$ , m =130, n = 26 is constructed. Ought to the high number of pixels (samples) in any image, a dimensional space reduction by means of PCA is carried out from n = 26to l = 4. In this experiment, the first four principal axes (eigenvectors) explain up to 99% of the variances according to

$$(e_i)\% = 100 * \lambda_i / \sum_{i=0}^{n-1} \lambda_i;$$
 (6.1)

being  $e_i$  the percentage explained and  $\lambda_i$  the eigenvalues of **D** (fig. 5.6(c)).

For illustrative purposes a mahalanobis distance map is built projecting all image features onto the reduced space and measuring the distance to the training vessel cluster. The Mahalanobis distance map shows the snake convergence to a vessel. Due



Figure 6.1: Probabilistic external energy (a), Snake segmentation (b).

to the statistic learning, Mahalanobis distance is small mainly in vessel positions. As a result, false responses of vessel appearance are diminished and the snake local energy minima are significantly reduced. On the other hand, approaching the vessel, the Mahalanobis distance exponentially decreases driving the snake to lock on the vessel features. Figure 6.1 (a) shows the probabilistic external energy map as a function of the Mahalanobis distance. In fig.6.1 (b) a snake is used to segment a vessel. The snake has converged to the vessel in 30 iterations using the energy showed in figure 6.1 (a). One can notice that in a real application the built-in map approach (5.14) is preferable to obtain faster energy-minimisation scheme avoiding explicit construction of likelihood map for the whole image.

### 6.1.1 Results of the vessel detection process using vessel profiles and PPCA.

Tha approach is tested in a vessel tracking framework. To demonstrate the viability of the tracking approach by statistic snakes, a hybrid potential maps is built to track a coronary tree vessel in a sequence of angiographies. The vessels are dynamic elastic elongated objects in images with very low contrast and signal-to-noise rate. A more sophisticated approach to segment and track objects is obligatory in order to achieve good results. For each image frame I in the sequence, a likelihood map is built and the minimized snake in frame I - 1 is used as initialization. The first snake initialization is obtained using a path search through the vessel under analysis. The user provides the starting point of the path and the path search is carried out as follows: from the starting point the maximum likelihood vector is chosen and a set of coherence vectors is searched in the neighborhood for maximum scalar product. The process is repeated up to the end of the path (fig. 5.7(a)).

To build the maps a previous learning step is made with a set of twenty image

frames. We take two hundred samples from each image and each sample is of forty pixels width. The sampled profiles are obtained perpendicular to the centerline of the vessels. To obtain the centerline, we use a conventional snake and the perpendicular profiles are defined regarding the snake. For each learned vessel we obtain a matrix where the rows are the profiles along a vessel (fig. 5.2). Within the probabilistic framework we make the dimensional reduction through PPCA using the first five principal axes, which explain up to 97% of the observed data variance in feature space.

The built map comprises the extraction of coherent directions through the second moment matrix (fig. 5.3) discarding regions with low module of the coherent vectors to speed up the process of map generation. Afterwards, the profiles over the extracted directions are obtained using as the middle point of the profile the origin of each direction vector. The profiles length, as in the learning step, is forty pixels. The profiles are then compared against the learned ones and as a result a measure of the probability of being a true vessel profile is obtained. Although this probability map can be considered ready to use (fig. 5.8), it is open to further refinements. Using more specific knowledge about the domain, we could recover the coherence directions and after weighting them with the probabilities we could test for parallelisms. Non parallel vectors mean high probability of being a false profile.

### 6.2 Model Validation

Using a phantom of a right coronary artery a set of images were acquired from a cardiac angiographic equipment. The acquisition was done providing a rotation movement of 47 degrees to the "C" arm at 12.5 frames per sec.. From a total of 64 frames acquired, the first 32 swapped from 0 degree Left Anterior Oblique (LAO) to 23.5 and the others from 23.5 LAO to 47 LAO. Note that the rotation axis of the "C" arm is labeled as X. The experiment consists of a 3D reconstruction using pair of frames from both groups. The expected result is a rotation of the model.

The model of the RCA split in four segments (R1, R2, R3, and R4) with three points per segment sum a total of 12 points. The points are named using the words proximal, middle and distal, indicating the position of each point withing the segment and regarding the ostium as the origin. Also, the segment number increases with the distance to the ostium. From the 32 frames of each group, we took 1 every 4 for a total of 8 samples (the acquisition speed is 3.125 frames per sec.).

The expected result was measured testing the following:

- Invariance of the distance to the origin of coordinates
- Invariance of the minimal distance to the rotation axis
- Speed: points near the rotation axis have lower speed than points far from it.
- Path length: points near the rotation axis describe a distance shorter than points far from it.

For each point in every sampled frame, the distance to the origin, and to the rotation axis was computed. Also speed and space between points in consecutive frames were computed. Finally, mean values and mean deviation was computed:

Mean:

$$\bar{x} = \frac{\sum_{i=1}^{n} (x_i)}{n}$$
$$\sigma = \frac{\sum_{i=1}^{n} |x_i - \bar{x}|}{n}$$

Mean deviation:

each segment. Table 6.2 shows the mean distances to the rotation axis of the three points representing each segment, and table 6.3 is the mean deviation. Tables 6.4, 6.5 and 6.6 are the point speed measured as the space between two consequtive frames, the mean speed for each point and the mean deviation respectively. Table 6.7 shows the lenght of the trajectory of the points between consecutive frames.

Table 6.8 shows the distances covered by the points during the 8 frames, and table 6.9 is the distance mean deviation. Finally, tables 6.10 and 6.11 depict the distamnces of the points to the origin of coordinated and their mean deviation respectively.

	1	2	3	4	5	6
	R1prox	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
0	40,934	26,124	27,812	34,289	32,821	31,254
1	$41,\!635$	$26,\!620$	26,553	32,777	32,021	30,368
2	44,519	27,452	25,310	31,311	31,060	30,599
3	46,585	28,478	25,770	31,402	30,373	30,123
4	45,462	26,549	24,995	30,769	30,932	30,583
5	42,524	27,115	25,138	30,611	30,641	30,753
6	45,537	30,370	25,728	29,477	30,496	31,480
7	38,862	29,822	26,603	29,447	30,583	31,720
		/		/	/	
<u> </u>	7	8	9	10	11	12
	7 R3 <sub>prox</sub>	$\frac{8}{R3_{mid}}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$12 \\ R4_{dist}$
0	7 R3 <sub>prox</sub> 38,189		9 $R3_{dist}$ 47,372	$     \begin{array}{r} 10 \\ R4_{prox} \\ 35,419 \end{array} $	$11 \\ R4_{mid} \\ 19,399$	$\begin{array}{r}12\\R4_{dist}\\16,646\end{array}$
0 1	$7 \\ R3_{prox} \\ 38,189 \\ 37,768$	$egin{array}{c} 8 \\ R3_{mid} \\ 46,452 \\ 46,464 \end{array}$	9 $R3_{dist}$ 47,372 47,196	$\begin{array}{r} 10 \\ R4_{prox} \\ 35,419 \\ 36,784 \end{array}$	$\begin{array}{r} 11 \\ R4_{mid} \\ 19,399 \\ 18,522 \end{array}$	$\frac{12}{R4_{dist}}$ 16,646 18,596
0 1 2	$7 \\ R3_{prox} \\ 38,189 \\ 37,768 \\ 36,118 \\$	$egin{array}{c} 8 \\ R3_{mid} \\ 46,452 \\ 46,464 \\ 44,568 \end{array}$	$9 \\ R3_{dist} \\ 47,372 \\ 47,196 \\ 45,923$	$\begin{array}{r} 10 \\ R4_{prox} \\ 35,419 \\ 36,784 \\ 33,488 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 19,399 \\ 18,522 \\ 18,073 \end{array}$	$\begin{array}{r} 12 \\ R4_{dist} \\ 16,646 \\ 18,596 \\ 18,563 \end{array}$
0 1 2 3	$7 \\ R3_{prox} \\ 38,189 \\ 37,768 \\ 36,118 \\ 35,194$	$\begin{array}{r} 8\\ R3_{mid}\\ 46,452\\ 46,464\\ 44,568\\ 44,118\end{array}$	$9 \\ R3_{dist} \\ 47,372 \\ 47,196 \\ 45,923 \\ 43,902$	$\begin{array}{r} 10 \\ R4_{prox} \\ 35,419 \\ 36,784 \\ 33,488 \\ 34,520 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 19,399 \\ 18,522 \\ 18,073 \\ 18,478 \end{array}$	$\begin{array}{c} 12 \\ R4_{dist} \\ 16,646 \\ 18,596 \\ 18,563 \\ 18,587 \end{array}$
$\begin{array}{c} 0\\ 1\\ 2\\ 3\\ 4 \end{array}$	$\begin{array}{r} 7 \\ R3_{prox} \\ 38,189 \\ 37,768 \\ 36,118 \\ 35,194 \\ 36,132 \end{array}$	$\begin{array}{r} 8\\ R3_{mid}\\ 46,452\\ 46,464\\ 44,568\\ 44,118\\ 43,260\\ \end{array}$	$\begin{array}{c} 9\\ R3_{dist}\\ 47,372\\ 47,196\\ 45,923\\ 43,902\\ 42,549 \end{array}$	$\begin{array}{c} 10 \\ R4_{prox} \\ 35,419 \\ 36,784 \\ 33,488 \\ 34,520 \\ 32,759 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 19,399 \\ 18,522 \\ 18,073 \\ 18,478 \\ 18,284 \end{array}$	$\begin{array}{r} 12 \\ R4_{dist} \\ \hline 16,646 \\ 18,596 \\ 18,563 \\ 18,587 \\ 17,155 \end{array}$
$     \begin{array}{c}       0 \\       1 \\       2 \\       3 \\       4 \\       5     \end{array} $	$\begin{array}{r} 7\\ R3_{prox}\\ 38,189\\ 37,768\\ 36,118\\ 35,194\\ 36,132\\ 36,379\\ \end{array}$	$\begin{array}{r} 8\\ R3_{mid}\\ 46,452\\ 46,464\\ 44,568\\ 44,118\\ 43,260\\ 41,102\\ \end{array}$	$\begin{array}{c} 9\\ R3_{dist}\\ 47,372\\ 47,196\\ 45,923\\ 43,902\\ 42,549\\ 42,117\end{array}$	$\begin{array}{c} 10 \\ R4_{prox} \\ 35,419 \\ 36,784 \\ 33,488 \\ 34,520 \\ 32,759 \\ 30,877 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 19,399 \\ 18,522 \\ 18,073 \\ 18,478 \\ 18,284 \\ 17,894 \end{array}$	$\begin{array}{r} 12 \\ R4_{dist} \\ \hline 16,646 \\ 18,596 \\ 18,563 \\ 18,587 \\ 17,155 \\ 17,487 \end{array}$
$     \begin{array}{c}       0 \\       1 \\       2 \\       3 \\       4 \\       5 \\       6     \end{array} $	$\begin{array}{c} 7\\ R3_{prox}\\ 38,189\\ 37,768\\ 36,118\\ 35,194\\ 36,132\\ 36,379\\ 36,982 \end{array}$	$\begin{array}{c} 8\\ R3_{mid}\\ 46,452\\ 46,464\\ 44,568\\ 44,118\\ 43,260\\ 41,102\\ 39,844 \end{array}$	$\begin{array}{c} 9\\ R3_{dist}\\ 47,372\\ 47,196\\ 45,923\\ 43,902\\ 42,549\\ 42,117\\ 42,036\end{array}$	$\begin{array}{c} 10\\ R4_{prox}\\ 35,419\\ 36,784\\ 33,488\\ 34,520\\ 32,759\\ 30,877\\ 32,879 \end{array}$	$\begin{array}{c} 11\\ R4_{mid}\\ 19,399\\ 18,522\\ 18,073\\ 18,478\\ 18,284\\ 17,894\\ 19,291 \end{array}$	$\begin{array}{c} 12\\ R4_{dist}\\ 16,646\\ 18,596\\ 18,563\\ 18,587\\ 17,155\\ 17,487\\ 16,446 \end{array}$

Table 6.1: Distance to the rotation axis (mm).

ſ	1	2	3	4	5	6
	$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
ĺ	$43,\!257$	27,816	25,989	31,260	$31,\!116$	30,860
ſ	7	8	9	10	11	12
	7 R3 <sub>prox</sub>	$\frac{8}{R3_{mid}}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$12 \\ R4_{dist}$

Table 6.2: Mean Distance to the rotation axis (mm).

### 6.2. Model Validation

1	2	3	4	5	6
R1prox	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
$^{2,269}$	1,305	0,750	1,184	$0,\!653$	0,469
7	8	9	10	11	12
$7 R3_{prox}$	$\frac{8}{R3_{mid}}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$12 R4_{dist}$

 Table 6.3: Distance Mean Deviation (rotation axis).

	1	2	3	4	5	6
	R1prox	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
0 to 1	11,609	7,241	12,585	9,723	$^{8,011}$	11,985
1 to 2	15,954	10,174	12,143	16,427	14,220	9,236
2 to 3	11,823	10,281	$^{5,430}$	5,623	$10,\!647$	$^{8,969}$
3 to 4	5,139	$^{8,328}$	13,388	9,471	2,753	13,172
4 to 5	10,030	7,738	$^{3,425}$	9,521	$^{8,996}$	$^{8,732}$
5 to 6	12,691	18,174	$^{6,227}$	13,450	22,108	11,489
6 to 7	21,351	$^{4,623}$	7,723	9,043	4,371	4,329

	7	8	9	10	11	12
	$R3_{prox}$	$R3_{mid}$	$R3_{dist}$	$R4_{prox}$	$R4_{mid}$	$R4_{dist}$
0 to 1	11,763	6,769	$17,\!644$	7,508	6,112	$^{8,671}$
1 to 2	13,763	$16,\!605$	9,578	18,700	13,841	$^{3,022}$
2 to 3	18,158	10,303	20,508	6,567	2,803	$^{3,235}$
3 to 4	$^{8,462}$	$14,\!630$	12,400	6,968	5,935	4,603
4 to 5	11,923	21,446	26,497	12,323	6,615	5,361
5 to 6	13,262	13,589	7,850	12,009	6,214	3,593
6 to 7	$^{9,230}$	15,740	19,798	15,786	7,755	3,746

Table 6.4: Velocity (mm/seg).

1	2	3	4	5	6
$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
13,744	8,898	$^{8,580}$	10,288	9,434	$^{9,030}$
7	8	9	10	11	12
7 R3 <sub>prox</sub>	$8 R3_{mid}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$12 R4_{dist}$

 Table 6.5:
 Mean Velocity.

1	2	3	4	5	6
$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
4,357	2,984	3,094	2,326	4,668	2,440
7	8	9	10	11	12
7 $R3_{prox}$	8 R3 <sub>mid</sub>	$9 R3_{dist}$	10 <i>R4prox</i>	$11 R4_{mid}$	$12 R4_{dist}$

 Table 6.6:
 Velocity Mean Deviation.

	1	2	3	4	5	6
	$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
0 to 1	3,715	2,317	4,027	3,111	2,564	3,835
1 to 2	5,105	$^{3,256}$	3,886	$^{5,257}$	4,550	2,955
2 to 3	3,783	3,290	1,738	1,799	3,407	2,870
3 to 4	1,644	2,665	4,284	3,031	0,881	4,215
4 to 5	$^{3,210}$	2,476	1,096	$^{3,047}$	2,879	2,794
5 to 6	4,061	5,816	1,993	4,304	7,074	3,677
0 + - 7	6 020	1 470	9 471	0.004	1,200	1 295
0 t 0 7	0,052	1,479	2,471	2,894	1,599	1,565
6 t 0 7	0,852	1,479	9	2,894	1,399	1,385
0 t0 7	7 R3 <sub>prox</sub>	1,479 8 R3 <sub>mid</sub>	9 R3 <sub>dist</sub>	$\frac{10}{R4_{prox}}$	$\begin{array}{c} 1,399\\ \hline 11\\ R4_{mid} \end{array}$	$\frac{12}{R4_{dist}}$
0 to 1	7 <i>R3<sub>prox</sub></i> 3,764		$\begin{array}{r} 2,471 \\ 9 \\ R3_{dist} \\ 5,646 \end{array}$	$   \begin{array}{r}     2,894 \\     10 \\     R4_{prox} \\     2,402   \end{array} $	1,399 11 $R4_{mid}$ 1,956	1,383 12 $R4_{dist}$ 2,775
0 to 1 1 to 2	$     \begin{array}{r}                                     $	$ \begin{array}{r}     1,479 \\     8 \\     R3_{mid} \\     2,166 \\     5,314 \\ \end{array} $	$\begin{array}{r} 2,471\\ 9\\ R3_{dist}\\ 5,646\\ 3,065\end{array}$	$   \begin{array}{r}     2,894 \\     10 \\     R4_{prox} \\     2,402 \\     5,984   \end{array} $	$   \begin{array}{r}     1,399 \\     11 \\     R4_{mid} \\     1,956 \\     4,429   \end{array} $	$   \begin{array}{r} 1,383 \\     12 \\     R4_{dist} \\     2,775 \\     0,967 \\   \end{array} $
0 to 1 1 to 2 2 to 3	$\begin{array}{r} & & & & \\ & & & 7 \\ \hline & & & & \\ & & & & \\ & & & & \\ & & & &$	$\begin{array}{r} 1,479\\ \\ 8\\ R3_{mid}\\ 2,166\\ 5,314\\ 3,297 \end{array}$	$\begin{array}{r} 9\\ R3_{dist}\\ 5,646\\ 3,065\\ 6,563\end{array}$	$\begin{array}{r} 10 \\ R4_{prox} \\ 2,402 \\ 5,984 \\ 2,101 \end{array}$	$   \begin{array}{r}     1,399 \\     11 \\     R4_{mid} \\     1,956 \\     4,429 \\     0,897 \\   \end{array} $	$\begin{array}{r} 1,383\\ \hline 12\\ R4_{dist}\\ 2,775\\ 0,967\\ 1,035 \end{array}$
0 to 1 1 to 2 2 to 3 3 to 4	$\begin{array}{r} & & & \\ & & 7 \\ \hline & & & 7 \\ \hline & & & & 3 \\ & & 3,764 \\ & & 4,404 \\ & & 5,811 \\ & & 2,708 \end{array}$	$\begin{array}{r} 1,479\\ \\ 8\\ R3_{mid}\\ 2,166\\ 5,314\\ 3,297\\ 4,682 \end{array}$	$\begin{array}{r} 2,471\\ \hline 9\\ R3_{dist}\\ 5,646\\ 3,065\\ 6,563\\ 3,968\\ \end{array}$	$\begin{array}{r} 2,894\\\hline 10\\ R4_{prox}\\2,402\\5,984\\2,101\\2,230\\\end{array}$	$\begin{array}{c} 1,399\\ \hline 11\\ R4_{mid}\\ 1,956\\ 4,429\\ 0,897\\ 1,899\\ \end{array}$	$\begin{array}{r} 1,383\\ \hline 12\\ R4_{dist}\\ 2,775\\ 0,967\\ 1,035\\ 1,473\\ \end{array}$
0 to 1 1 to 2 2 to 3 3 to 4 4 to 5	$\begin{array}{r} 6,832\\ \hline 7\\ R3_{prox}\\ 3,764\\ 4,404\\ 5,811\\ 2,708\\ 3,815\\ \end{array}$	$\begin{array}{r} 1,479\\ \hline 8\\ R3_{mid}\\ \hline 2,166\\ 5,314\\ 3,297\\ 4,682\\ 6,863\\ \end{array}$	$\begin{array}{r} 2,471\\ \hline 9\\ R3_{dist}\\ \hline 5,646\\ 3,065\\ 6,563\\ 3,968\\ 8,479\end{array}$	$\begin{array}{r} 2,894\\ \hline 10\\ R4_{prox}\\ 2,402\\ 5,984\\ 2,101\\ 2,230\\ 3,943 \end{array}$	$\begin{array}{r} 1,399\\ \hline 11\\ R4_{mid}\\ 1,956\\ 4,429\\ 0,897\\ 1,899\\ 2,117\\ \end{array}$	$\begin{array}{r} 1,383\\ \hline 12\\ R4_{dist}\\ 2,775\\ 0,967\\ 1,035\\ 1,473\\ 1,716\end{array}$
0 to 1 1 to 2 2 to 3 3 to 4 4 to 5 5 to 6	$\begin{array}{r} & 6,832 \\ \hline & 7 \\ R3_{prox} \\ \hline & 3,764 \\ 4,404 \\ 5,811 \\ 2,708 \\ 3,815 \\ 4,244 \end{array}$	$\begin{array}{r} 1,479\\ \hline 8\\ R3_{mid}\\ \hline 2,166\\ 5,314\\ 3,297\\ 4,682\\ 6,863\\ 4,349\\ \end{array}$	$\begin{array}{r} 2,471\\ \hline 9\\ R3_{dist}\\ \hline 5,646\\ 3,065\\ 6,563\\ 3,968\\ 8,479\\ 2,512 \end{array}$	$\begin{array}{r} 2,894\\ \hline 10\\ R4_{prox}\\ 2,402\\ 5,984\\ 2,101\\ 2,230\\ 3,943\\ 3,843\\ \end{array}$	$\begin{array}{c} 1,399\\ \hline 11\\ R4_{mid}\\ \hline 1,956\\ 4,429\\ 0,897\\ \hline 1,899\\ 2,117\\ \hline 1,988\\ \end{array}$	$\begin{array}{r} 1,383\\\hline 12\\ R4_{dist}\\ 2,775\\ 0,967\\ 1,035\\ 1,473\\ 1,716\\ 1,150\\ \end{array}$

Table 6.7:Path length (mm).

1	2	3	4	5	6
$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
28,351	21,299	19,495	23,442	22,753	21,732
7	8	9	10	11	12
7 R3 <sub>prox</sub>	$\frac{8}{R3_{mid}}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$\begin{array}{c} 12 \\ R4_{dist} \end{array}$

Table 6.8: Total path length of each point (mm).

1	2	3	4	5	6
$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
1,100	0,924	1,098	0,818	1,509	$0,\!689$
7	8	9	10	11	12
7 R3 <sub>prox</sub>	$\frac{8}{R3_{mid}}$	$9 R3_{dist}$	$10 R4_{prox}$	$11 R4_{mid}$	$\begin{array}{c} 12 \\ R4_{dist} \end{array}$

Table 6.9: Mean Deviation of the path length.

	1	2	3	4	5	6
	$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
0	45,539	29,789	33,023	$37,\!191$	33,084	33,183
1	46,168	$30,\!205$	32,005	$35,\!685$	$32,\!240$	32,334
2	49,200	$30,\!914$	30,928	$34,\!397$	31,359	32,590
3	50,786	$31,\!798$	31,174	$34,\!317$	$30,\!650$	32,001
4	49,787	$30,\!126$	30,509	$33,\!880$	31,230	32,475
5	46,907	$30,\!437$	30,913	$33,\!780$	30,940	$32,\!680$
6	50,049	$33,\!457$	31,405	32,738	30,795	33,408
7	43,549	$32,\!974$	32,053	$32,\!521$	30,871	33,627
	7	8	9	10	11	12
	$7 R3_{prox}$	$rac{8}{R3_{mid}}$	$9 R3_{dist}$	$\frac{10}{R4_{prox}}$	$11 R4_{mid}$	$\frac{12}{R4_{dist}}$
0	$7$ $R3_{prox}$ $43,144$	$\frac{8}{R3_{mid}}$ $53,372$	9 $R3_{dist}$ 57,394	$ \begin{array}{r}10\\R4_{prox}\\51,217\end{array}$	$\frac{11}{R4_{mid}}$ $39,580$	$\begin{array}{c} 12 \\ R4_{dist} \\ 30,483 \end{array}$
0 1	$7 \\ R3_{prox} \\ 43,144 \\ 42,899$	$egin{array}{c} 8 \ R3_{mid} \ 53,372 \ 53,642 \end{array}$	$9 \\ R3_{dist} \\ 57,394 \\ 55,727$	$     \begin{array}{r} 10 \\                                   $	$\frac{11}{R4_{mid}} \\ 39{,}580 \\ 39{,}375$	$\begin{array}{c} 12 \\ R4_{dist} \\ 30,483 \\ 31,478 \end{array}$
$\begin{array}{c} 0 \\ 1 \\ 2 \end{array}$	$7 \\ R3_{prox} \\ 43,144 \\ 42,899 \\ 41,218 \\$	$\begin{array}{c} 8 \\ R3_{mid} \\ 53,372 \\ 53,642 \\ 51,608 \end{array}$	$9 \\ R3_{dist} \\ 57,394 \\ 55,727 \\ 55,920$	$\begin{array}{c} 10 \\ R4_{prox} \\ 51,217 \\ 52,152 \\ 49,951 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 39,580 \\ 39,375 \\ 38,988 \end{array}$	$\begin{array}{c} 12 \\ R4_{dist} \\ 30,483 \\ 31,478 \\ 31,485 \end{array}$
$\begin{bmatrix} 0\\ 1\\ 2\\ 3 \end{bmatrix}$	$7 \\ R3_{prox} \\ 43,144 \\ 42,899 \\ 41,218 \\ 40,236$	$egin{array}{c} 8 \\ R3_{mid} \\ 53,372 \\ 53,642 \\ 51,608 \\ 51,268 \end{array}$	$9 \\ R3_{dist} \\ 57,394 \\ 55,727 \\ 55,920 \\ 53,259$	$egin{array}{c} 10 \ R4_{prox} \ 51,217 \ 52,152 \ 49,951 \ 50,559 \ \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 39,580 \\ 39,375 \\ 38,988 \\ 39,686 \end{array}$	$\begin{array}{c} 12 \\ R4_{dist} \\ 30,483 \\ 31,478 \\ 31,485 \\ 31,795 \end{array}$
$\begin{array}{c} 0\\ 1\\ 2\\ 3\\ 4 \end{array}$	$\begin{array}{r} 7 \\ R3_{prox} \\ 43,144 \\ 42,899 \\ 41,218 \\ 40,236 \\ 41,761 \end{array}$	$egin{array}{c} 8 \\ R3_{mid} \\ 53,372 \\ 53,642 \\ 51,608 \\ 51,268 \\ 50,832 \end{array}$	$9 \\ R3_{dist} \\ 57,394 \\ 55,727 \\ 55,920 \\ 53,259 \\ 53,238$	$egin{array}{c} 10 \ R4_{prox} \ 51,217 \ 52,152 \ 49,951 \ 50,559 \ 49,800 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 39,580 \\ 39,375 \\ 38,988 \\ 39,686 \\ 39,684 \end{array}$	$\begin{array}{c} 12 \\ R4_{dist} \\ 30,483 \\ 31,478 \\ 31,485 \\ 31,795 \\ 30,713 \end{array}$
$0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5$	$\begin{array}{c} 7\\ R3_{prox}\\ 43,144\\ 42,899\\ 41,218\\ 40,236\\ 41,761\\ 41,916\\ \end{array}$	$\frac{8}{R3_{mid}}$ $\frac{53,372}{53,642}$ $\frac{51,608}{51,268}$ $\frac{50,832}{47,575}$	$\begin{array}{r} 9\\ R3_{dist}\\ 57,394\\ 55,727\\ 55,920\\ 53,259\\ 53,238\\ 50,981 \end{array}$	$\begin{array}{c} 10 \\ R4_{prox} \\ 51,217 \\ 52,152 \\ 49,951 \\ 50,559 \\ 49,800 \\ 48,122 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 39,580 \\ 39,375 \\ 38,988 \\ 39,686 \\ 39,684 \\ 38,724 \end{array}$	$\begin{array}{c} 12\\ R4_{dist}\\ 30,483\\ 31,478\\ 31,485\\ 31,795\\ 30,713\\ 30,420\\ \end{array}$
$egin{array}{c} 0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{array}$	$\begin{array}{c} 7\\ R3_{prox}\\ 43,144\\ 42,899\\ 41,218\\ 40,236\\ 41,761\\ 41,916\\ 42,316\\ \end{array}$	$\begin{array}{c} 8\\ R3_{mid}\\ 53,372\\ 53,642\\ 51,608\\ 51,268\\ 50,832\\ 47,575\\ 46,225\\ \end{array}$	$\begin{array}{c} 9\\ R3_{dist}\\ 57,394\\ 55,727\\ 55,920\\ 53,259\\ 53,238\\ 50,981\\ 51,082\\ \end{array}$	$\begin{array}{c} 10 \\ R4_{prox} \\ 51,217 \\ 52,152 \\ 49,951 \\ 50,559 \\ 49,800 \\ 48,122 \\ 49,350 \end{array}$	$\begin{array}{c} 11 \\ R4_{mid} \\ 39,580 \\ 39,375 \\ 38,988 \\ 39,686 \\ 39,684 \\ 38,724 \\ 39,843 \\ \end{array}$	$\begin{array}{c} 12\\ R4_{dist}\\ 30,483\\ 31,478\\ 31,485\\ 31,795\\ 30,713\\ 30,713\\ 30,420\\ 30,179\end{array}$

Table 6.10: Distance to the origin (mm).

1	2	3	4	5	6
$R1_{prox}$	$R1_{mid}$	$R1_{dist}$	$R2_{prox}$	$R2_{mid}$	$R2_{dist}$
$^{2,207}$	1,148	0,644	1,084	0,633	0,464
7	8	9	10	11	12
	-	0	10		12
$R3_{prox}$	R3 <sub>mid</sub>	$R3_{dist}$	R4prox	$R4_{mid}$	$R4_{dist}$

Table 6.11: Mean Deviation of the distance to the origin.

Chart 6.2 confirms the hypothesis made about speed, distances traveled and mean distances. Figure 6.3 depicts a frame of the results. The spacial speed (shape deformation) is showed through a colour coding. The coding uses blue, green, red to represent increasing speed in this order (blue means lower speed, red higher). and on the left there are the trajectories of the phanthom projections.



Figure 6.2: Point position, velocity (mm/seg) and traveled path (mm) regarding the rotation axis sorted by the distance to the axis. Points near the axis have less speed and shorter traveled path.

## 6.3 Results using real data

In this example the movement reconstruction and analysis with a real image sequence is presented.



Figure 6.3: Fourth frame spatial speed using a colour coding and the phantom trajetory in both projections.

### 6.3.1 Case using (28.2 RAO, 0 Cranial) and (28.2 RAO, 19.8 Cranial) projection parameters.

These parameters allow for an optimal view of the left coronary arteries. Figure 6.4 shows the model and the selected arteries (red). The sequence under analysis consists



Figure 6.4: Selecting artery segments: LM, C1, C2, C3, C4, OM, M2, L1, L2, L3, L4, D1, D2, S1 i S2.

of six frames acquired at, approximately 4 frames/sec. Then, the model was adapted to the angiographies. As the bifurcation are not detected the detection and tracking is done at branch level. Nevertheless the result is a superposition of every branch (Fig. 6.5).

Figure 6.6 shows the sequence after 3D reconstruction using B-splines.

Figure 6.7 shows the trajectories of the model branches in 2D and 3D.

Table 6.13 summarizes the space increment of every point between any two frames, total and mean traveled space for each frame. Segment C4 shows the highest increment (frame 1, 2).

Figure 6.8 shows the velocity at some points. The cyclic shape described by every point can be explained by the intrinsic beating of the heart, where the arteries are laying.

Table 6.14 shows that the point with highest mean speed is  $C4_{prox}$  and the highest acceleration corresponds to frames 1 and 2. The values in the table are used to show the velocity as a mapping of colors.

Figure 6.9 shows the speed as a function of the time. In red, one can appreciate the highest change between frames 1 and 2. Meanwhile, the lowest change corresponds to frames 4 and 5 (blue). Transition between low and high is represented in green and yelow.



Figure 6.5: Model adapted.



Figure 6.6: 3D Sequence Frames using bsplines and NURBS.

Figure 6.10 shows the dynamic behaviour of the shape of the arteries. The information is obtained, also, from table 6.14. The colour coding is also the same. At the first frames the higher speeds are near the ventricular zone, while during the last frames the high speed is showed near the auricular zone.

Using the right most column of table 6.14 and the same colour convention figure 6.11 shows the mean velocity. The circunflex artery shows the greatest global movement and the speed falls towards the apex.

Figure 6.12 shows a velocity threshold. One can split the speed in two categories setting a limit as a threshold. Using a colour coding the tree is displayed in two color matching speeds higher and lower than the threshold.

The following tables are the values used above.



Figure 6.7: 2D and 3D Trajectories.



Figure 6.8: Velocity at different artery points.

		Frame 0	Frame 1	Frame 2	Frame 3	Frame 4	Frame 5
1	$LM_{prox}$	65,727	59,400	52,119	$58,\!561$	59,301	$61,\!000$
2	$LM_{mid}$	66,012	59,103	51,228	$58,\!980$	60,455	$60,\!724$
3	$LM_{dist}$	64,967	58,549	50,587	59,268	58,235	$60,\!698$
4	$C1_{prox}$	63, 194	57, 195	49,271	57,744	59,427	$60,\!754$
5	$C1_{mid}$	60,382	54,563	$46,\!682$	$57,\!067$	59,277	$63,\!258$
6	$C1_{dist}$	58,567	57,819	$46,\!648$	$59,\!631$	60,386	$61,\!402$
7	$C2_{prox}$	58,839	54,560	45,231	$50,\!938$	55,198	56,705
8	$C2_{mid}$	54,363	50,081	45,897	$51,\!236$	52,784	$49,\!887$
9	$C2_{dist}$	55,489	55,501	46,266	$54,\!860$	53,917	$52,\!162$
10	$C3_{prox}$	60,502	56,951	56,174	$63,\!656$	64,900	66,988
11	$C3_{mid}$	71,166	67,871	61,178	$73,\!060$	65,544	$71,\!491$
12	$C3_{dist}$	77,672	76,717	60,106	71,412	73,401	70,705
13	$C4_{prox}$	77,324	70,975	59,304	$69,\!140$	$69,\!635$	$66,\!374$
14	$C4_{mid}$	65,342	62, 190	55,030	$59,\!051$	59,323	$58,\!187$
15	$C4_{dist}$	59,320	59,173	49,823	$55,\!427$	57,036	$56,\!213$
16	$M2_{prox}$	70,678	67,252	48,431	$58,\!938$	56,828	$55,\!849$
17	$M2_{mid}$	73,443	70,908	59,087	$66,\!448$	65,755	66,213
18	$M2_{dist}$	66,689	65,938	56,215	$57,\!474$	58,769	59,720
19	$OM_{prox}$	71,922	58,869	42,591	$49,\!105$	49,516	$54,\!185$
20	$OM_{mid}$	66,442	62,379	51,969	$63,\!385$	61,807	$67,\!841$
21	$OM_{dist}$	60,741	60,427	58,292	$59,\!173$	57,933	$63,\!352$
22	$L1_{prox}$	63,963	57,744	52,273	$56,\!879$	59,100	60,788
23	$L1_{mid}$	54,941	47,935	43,959	$46,\!984$	51,037	$52,\!679$
24	$L1_{dist}$	49,612	42,716	37,573	$40,\!809$	$44,\!687$	$47,\!530$
25	$L2_{prox}$	41,162	$37,\!602$	$34,\!540$	$37,\!800$	39,196	$41,\!394$
26	$L2_{mid}$	39,418	39,110	37,429	$38,\!084$	40,395	$40,\!395$
27	$L2_{dist}$	40,112	40,467	38,203	$37,\!728$	39,524	$39,\!524$
28	$L3_{prox}$	42,048	45,124	40,320	$37,\!842$	38,767	$37,\!467$
29	$L3_{mid}$	44,007	46,358	44,425	$38,\!961$	42,715	$42,\!605$
30	$L3_{dist}$	47,706	48,086	49,386	46,729	47,751	$45,\!926$
31	$L4_{prox}$	56,207	55,479	52,386	$50,\!362$	49,825	$48,\!150$
32	$L4_{mid}$	59,143	60,895	62,755	$58,\!906$	57,096	$56,\!482$
33	$L4_{dist}$	59,995	59,968	59,604	$57,\!213$	58,057	$58,\!057$
34	$D1_{prox}$	48,196	42,074	38,817	$46,\!012$	47,737	$50,\!504$
35	$D1_{mid}$	42,001	35,893	34,051	$37,\!967$	39,313	$40,\!472$
36	$D1_{dist}$	43,827	50,493	$47,\!682$	$50,\!353$	$50,\!595$	$50,\!865$
37	$S1_{prox}$	46,839	35,318	30,813	$37,\!476$	39,341	$40,\!815$
38	$S1_{mid}$	$28,\!540$	$25,\!243$	18,042	$22,\!178$	24,427	$24,\!983$
39	$S1_{dist}$	24,156	24,566	$18,\!692$	$14,\!247$	16,841	$15,\!410$

Table 6.12: Distances to the origin of coordinates (mm).

	D a	<b>D</b> 4	<b>D</b>	D a	<b>D</b> (		
	Frame 0	Frame 1	Frame 2	Frame 3	Frame 4	Frame 5	Tot. Space
$LM_{prox}$	5,113	$7,\!194$	6,037	$^{3,223}$	3,379	$^{9,234}$	34,180
$LM_{mid}$	$5,\!890$	6,521	$^{8,505}$	2,242	6,969	$^{6,251}$	36,378
$LM_{dist}$	$5,\!890$	6,521	9,409	$7,\!682$	4,455	6,410	40,368
$C1_{prox}$	5,890	6,521	7,333	2,936	2,984	$7,\!973$	$33,\!636$
$C1_{mid}$	5,890	6,521	9,218	2,000	6,407	15,027	45,062
$C1_{dist}$	10,152	9,440	11,762	3,878	2,756	12,681	50,669
$C2_{prox}$	5,890	$^{8,078}$	5,795	3,538	3,048	7,228	33,576
$C2_{mid}$	5,890	9,512	7,045	3,755	2,674	5,688	34,564
$C2_{dist}$	7,414	12,359	10,702	3,919	2,689	4,589	$41,\!672$
$C3_{prox}$	5,890	12,255	8,907	3,879	1,898	12,940	45,770
$C3_{mid}$	7,262	11,000	13,600	$^{8,342}$	5,459	9,781	55,444
$C3_{dist}$	$^{8,196}$	18,953	12,854	3,749	3,237	6,717	53,707
$C4_{prox}$	8,133	16,387	13,930	2,725	4,706	11,889	57,770
$C4_{mid}$	7,050	11,885	6,553	3,724	2,374	10,472	42,059
$C4_{dist}$	4,574	10,991	8,729	3,594	2,329	9,666	39,882
M2prox	6,953	18,746	11,763	3,885	2,000	13,060	56,409
$M2_{mid}$	6,953	13,742	11,264	1,622	1,204	7,199	41,984
$M2_{dist}$	6,953	13,375	8,413	1,628	1,789	10,021	42,179
$OM_{prox}$	6,810	14,002	6,243	2,409	4,945	12,737	47,145
$O\dot{M_{mid}}$	$^{8,087}$	7,849	9,427	2,409	4,693	4,660	37,124
$OM_{dist}$	10,211	5,612	7,492	1,328	4,945	5,999	35,587
$L1_{prox}$	5,083	6,579	6,387	2,380	2,711	3,935	27,074
$\hat{L1_{mid}}$	8,776	6,579	10,993	3,382	5,863	7,287	42,880
$L1_{dist}$	5,806	5,061	2,737	$^{3,627}$	2,300	6,223	25,755
$L2_{prox}$	4,193	6,591	5,914	4,474	5,461	1,406	28,039
$\hat{L2_{mid}}$	0,747	6,507	7,492	2,045	1,724	3,725	22,240
$L2_{dist}$	2,794	5,597	5,375	1,792	0,669	0,738	16,965
$L3_{prox}$	6,540	6,808	4,738	0,859	3,079	7,491	29,514
$L\hat{3}_{mid}$	4,964	3,856	7,535	4,154	0,937	2,528	23,975
$L3_{dist}$	2,598	2,953	3,976	2,609	1,727	2,836	16,700
$L4_{prox}$	0,747	10,676	4,343	0,646	2,660	12,562	31,634
$L\hat{4}_{mid}$	5,730	2,177	4,947	4,588	1,149	5,538	24,130
$L4_{dist}$	1,116	3,505	4,410	1,876	0,783	6,865	18,556
$D1_{prox}$	7,165	5,061	8,751	4,531	2,260	6,941	34,709
$D1_{mid}$	7,777	5,061	6,980	2,185	1,674	4,490	28,167
$D1_{dist}$	9,510	6,025	3,591	2,185	1,674	9,910	32,895
Slprox	11,447	6,579	6,809	2,185	3,163	6,623	36,806
$S1_{mid}$	$10,\!642$	6,579	8,019	2,185	3,163	4,581	35,168
$S1_{dist}$	7,319	6,579	8,019	2,185	3,163	9,099	36,362
Mean	6,360	8,467	7,846	3,086	3,053	7,512	

 ${\bf Table \ 6.13:}\ {\bf Increment,\ mean\ and\ total\ space\ (mm).}$ 

	Frame 0	Frame 1	Frame 2	Frame 3	Frame 4	Frame 5	Mean/Point
LMprox	15,978	22,481	18,865	10,072	10,561	28,855	17,802
$L\dot{M_{mid}}$	18,405	20,379	26,577	7,007	21,778	19,534	18,947
$LM_{dist}$	18,405	20,379	29,404	24,007	13,923	20,032	21,025
$C1_{prox}$	18,405	20,379	22,914	9,176	9,324	24,915	17,519
$C1_{mid}$	18,405	20,379	28,805	6,250	20,021	46,960	23,470
$C1_{dist}$	31,726	29,499	36,756	12,117	8,613	39,629	26,390
$C2_{prox}$	18,405	25,243	18,109	11,057	9,524	22,586	17,487
$C2_{mid}$	18,405	29,726	22,017	11,734	8,356	17,775	18,002
$C2_{dist}$	23,169	38,623	33,442	12,246	8,403	14,341	21,704
$C3_{prox}$	18,405	38,298	27,834	12,123	5,932	40,439	23,838
$C3_{mid}$	22,694	34,375	42,499	26,069	17,060	30,566	28,877
$C3_{dist}$	25,612	59,228	40,169	11,717	10, 117	20,991	27,973
$C4_{prox}$	25,415	51,209	43,532	8,516	14,706	$37,\!153$	30,088
$C\dot{4}_{mid}$	22,032	37,140	20,477	11,638	7,420	32,726	21,906
$C4_{dist}$	14,293	34,345	27,277	11,232	7,278	30,205	20,772
$M 2_{prox}$	21,729	58,582	36,760	12,142	6,251	40,813	29,379
$M2_{mid}$	21,729	42,944	35,200	5,070	3,762	22,495	21,867
$M 2_{dist}$	21,729	41,796	26,291	5,086	5,592	31,315	21,968
$OM_{prox}$	21,280	43,756	19,511	7,527	15,453	39,802	24,555
$O\dot{M_{mid}}$	25,273	24,527	29,459	7,527	14,665	14,563	19,336
$OM_{dist}$	31,909	17,538	23,412	4,149	15,453	18,747	18,535
$L1_{prox}$	15,884	20,558	19,961	7,436	8,470	12,296	14,101
$L1_{mid}$	27,424	20,558	34,354	10,570	18,321	22,772	22,333
$L1_{dist}$	18,143	15,816	$^{8,554}$	11,334	7,188	19,448	13,414
$L2_{prox}$	13,103	20,596	18,483	13,982	17,065	4,393	14,604
$L2_{mid}$	2,336	20,334	23,412	6,392	5,386	$11,\!640$	11,583
$L2_{dist}$	$^{8,732}$	17,491	16,797	5,601	2,089	2,305	8,836
$L3_{prox}$	20,437	21,275	14,806	2,683	9,621	23,409	15,372
$L3_{mid}$	15,513	12,051	23,546	12,982	2,930	7,901	12,487
$L3_{dist}$	$^{8,120}$	9,227	12,426	$^{8,154}$	5,397	8,863	8,698
$L4_{prox}$	2,336	33,363	13,571	2,019	$^{8,312}$	39,255	16,476
$L4_{mid}$	17,907	6,802	15,460	14,338	3,591	17,307	12,568
$L4_{dist}$	3,489	10,954	13,782	5,861	2,448	21,452	9,664
$D1_{prox}$	22,390	15,816	27,347	14,159	7,064	$21,\!691$	18,078
$D1_{mid}$	24,303	15,816	21,814	$^{6,827}$	5,233	14,031	$14,\!670$
$D1_{dist}$	29,718	18,827	11,223	$^{6,827}$	5,233	30,969	17,133
$S 1_{prox}$	35,773	20,558	$21,\!279$	$^{6,827}$	9,884	$20,\!698$	$19,\!170$
$S1_{mid}$	33,255	20,558	25,058	$^{6,827}$	9,884	14,316	18,316
$S1_{dist}$	22,872	20,558	25,058	$^{6,827}$	9,884	28,433	18,939
Mean/Frame	19,875	26,461	24,519	9,644	9,543	$23,\!478$	

Table 6.14: Velocity and mean for each point and frame (mm/seg).



Figure 6.9: Temporal dynamic analysis.



Figure 6.10: Shape dynamics analysis.



Figure 6.11: Mean speed.



Figure 6.12: Setting a threshold to visualize areas of different speeds. In blue areas with speeds lower than 33 mm/seg otherwise in red.

### 6.4. Summary

The results obtained can be interpreted as follows: the heart beats in a cyclic way. To each dilation follows a contraction. In the case study, the first three frames correspond to the contraction period (systole) and the last ones to dilation (diastole). There is a qualitative coincidence (visual) between the 3D trajectories obtained and the systole/diastole cycle. The movement, in general, is greater during diastole.

Moreover, a quantitative analysis done using the data in the tables shows the same coincidence. For example, sorting the artery segments by mean velocity, greater to less: C3, M2, C4, C1, OM, LM, C2, S1, D1, L1, L4, L3, L2. However, it has to be clear that further clinical assessment and validation is necessary to use the model in a clinical daily work.

## 6.4 Summary

The chapter presents some experimental results obtained with the model. The data obtained agree with the expected data taking into account the qualitative dynamic behaviour of a heart (normal).

### RESULTS

# Chapter 7

## Conclusion and future work

### 7.0.1 Main contributions

### A deformable coronary tree model

Using snakes as a global technique and a graph structure to hold the information, a 3D model of the coronary arteries is developed. The model takes into account the intrinsic vessel deformation and the vessel movements. It is ready to incorporate more knowledge, like vessel diameter, acceleration, etc..

In order to build the model, there are two approaches to data collection: do it manually or automatically. In this thesis the data collection is done automatically. The global technique used is known as snakes and at this point are three main contributions: two of them are resumed in incorporating elements of probability and statistics and the third is related to 3D reconstruction.

#### Statistical snakes

A new minimizing schema for snakes is developed. At this point a statistical vessel learning is used together with a mahalanobis distance measure to obtain a new minimizing schema for the snake named by us as eigensnakes. The other contribution has consisted in replacing the deterministic potential map by a probabilistic one after a learning process of vessel gray profiles.

The value of the statistic basis for linear structure detection and tracking has been established by demonstrating two methods:

- 1. the mechanism of PCA and Mahalanobis distances embedde into the minimization eschema of the snakes.
- 2. the mechanism of the PPCA embedded into the snake framework.

In order to manage complex objects and the variability of appearance of image structures, our techniques are supported by a learning approach to extract and detect only these "crease-like" features determined by the training set. Learned models are used in a probabilistic framework in order to build significant energy potential, resulting in less false responses of the image feature detector and more robust snakebased object tracking.

A new approach to potential computation using a likelihood map is formulated and applied to the tracking of specific structure on angiographies. The snake is less dependent on its initialisation and once placed on the hybrid potential map it converges to image features with high probability to represent learned object profiles. The obtained results and the self-training capability of the snake encourage utilizing it in different applications.

The experiments carried out showed that there are no significative differences between the use of PCA or PPCA regarding the results (vessel detection). The PCA are faster to compute, meanwhile PPCA offers a probabilistic framework open to incorporate higher levels of reasoning.

#### **3D** Vessel reconstruction using snakes

Finally, a new approach for 3D reconstruction under uncertainty conditions using snakes is formulated. The aim is to take profit of the "global property" of the snakes at a curve level instead of using the usual point to point reconstruction strategy. A snake model was applied to segment and reconstruct the coronary vessels. The advantages of this approach are that no exact user-provided point correspondence is necessary. The snake evolves in the space to adjust to the image data; as a result the model provides such a correspondence between the image points. The results showed that the technique is optimal from the point of view of the minimal reconstruction error defined as the distance between the projection rays. Furthermore, the reconstruction is improved when isocenter co-ordinates are iteratively updated.

### 7.0.2 Results

A cardiac imaging workstation was developed. From an existing radiological imaging workstation, the evolution process was explained. The goal was on the conformance to the international standard formulated for digital imaging in medicine. A deformable coronary tree model. A model to enable a high degree of automation in computer vessel analysis from angiographic imaging.

#### 7.0.3 Future work

Clinical research about coronary arteries dynamics. Full integration of the model into the cardiac image analysis software. Complete the model with statistically relevant data. Here an increment of samples are needed. Research to define new attributes to include in the graph. Image registration. To fuse spatial information from biplane angiograms with structural information provided by intra-vascular ultrasound images.

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