

UNIVERSITAT POLITÈCNICA DE CATALUNYA

ESCOLA TÈCNICA SUPERIOR D'ENGINYERS DE TELECOMUNICACIÓ

T E S I D O C T O R A L

" APORTACIÓ AL CONTROL DIGITAL ÓPTIMO DE
SISTEMAS DE ENERGÍA ELÉCTRICA :
APLICACIÓ A LA REGULACIÓ POTENCIA -
FRECUENCIA " .

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Director: JAUME HERRANZ LUIS

BARCELONA, SETEMBRE DE 1985

(2 toms)



U. P. C.

E.T.S.E. TELECOMUNICACIÓ

Biblioteca

APENDICE E :

Resultados de simulación anexos al Capítulo 5.

RESULTADOS DE SIMULACION.

Entrada: Perturbación de 0,01 p.u.MW en el Area 1.

Bloques listados:

- 20 : Generación del Area 1 (p.u.MW).
- 24 : Frecuencia del Area 1 (Hz).
- 27 : Intercambio de potencia del Area 1 al Area 2 (p.u.MW).
- 30 : Frecuencia del Area 2 (Hz).
- 38 : Generación del Area 2 (p.u.MW).
- 46 : Integral del ACE del Area 1, $\int ACE_1(t) dt.$
- 54 : Integral del ACE del Area 2, $\int ACE_2(t) dt.$
- 55 : Integral del error cuadrático de frecuencia del Area 1,
 $\int f_1^2(t) dt.$
- 56 : Integral del error cuadrático del intercambio de potencia
 $\int P_{12}^2(t) dt.$

PROGRAMA DE CONTROL OPTIM/FILTRE DE KALMAN

IDENTIFICACION DEL PROBLEMA :

T. DE MUESTRA
 .01500
 PRECISION
 .05000
 ALFA:
 0.00000

LA MATRIZ A

```

-4.8890E-01 -3.7700E-02 0.0000E 00 -3.7700E-02 0.0000E 00 0.0000E 00
0.0000E 00
-2.6148E 00 -4.7420E-01 0.0000E 00 -2.0170E-01 0.0000E 00 0.0000E 00
0.0000E 00
3.0525E 00 7.5400E-02 -2.0746E 00 7.5400E-02 0.0000E 00 0.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 6.2500E 00 -9.3700E-02 0.0000E 00 -6.2500E 00
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 9.2000E-02 0.0000E 00 1.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 1.5300E 00 0.0000E 00 0.0000E 00
-1.5300E 00
0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 6.2500E 00
-1.2343E 00

```

LA MATRIZ B

```

3.7700E-02
2.0170E-01
-7.5400E-02
0.0000E 00
0.0000E 00
0.0000E 00
0.0000E 00

```

LA MATRIZ C

```

0.0000E 00 0.0000E 00 0.0000E 00 1.0000E 00 0.0000E 00 0.0000E 00
0.0000E 00

```

***** OPCION CONTROL *****

LA MATRIZ R

```

1.0000E 00

```

LA MATRIZ Q

```

5.0000E-01 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00
0.0000E 00
0.0000E 00 5.0000E-01 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 5.0000E-01 0.0000E 00 0.0000E 00 0.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 1.0000E 00 0.0000E 00 0.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 5.0000E-01 0.0000E 00
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 5.0000E-01
0.0000E 00
0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00 0.0000E 00
5.0000E-01

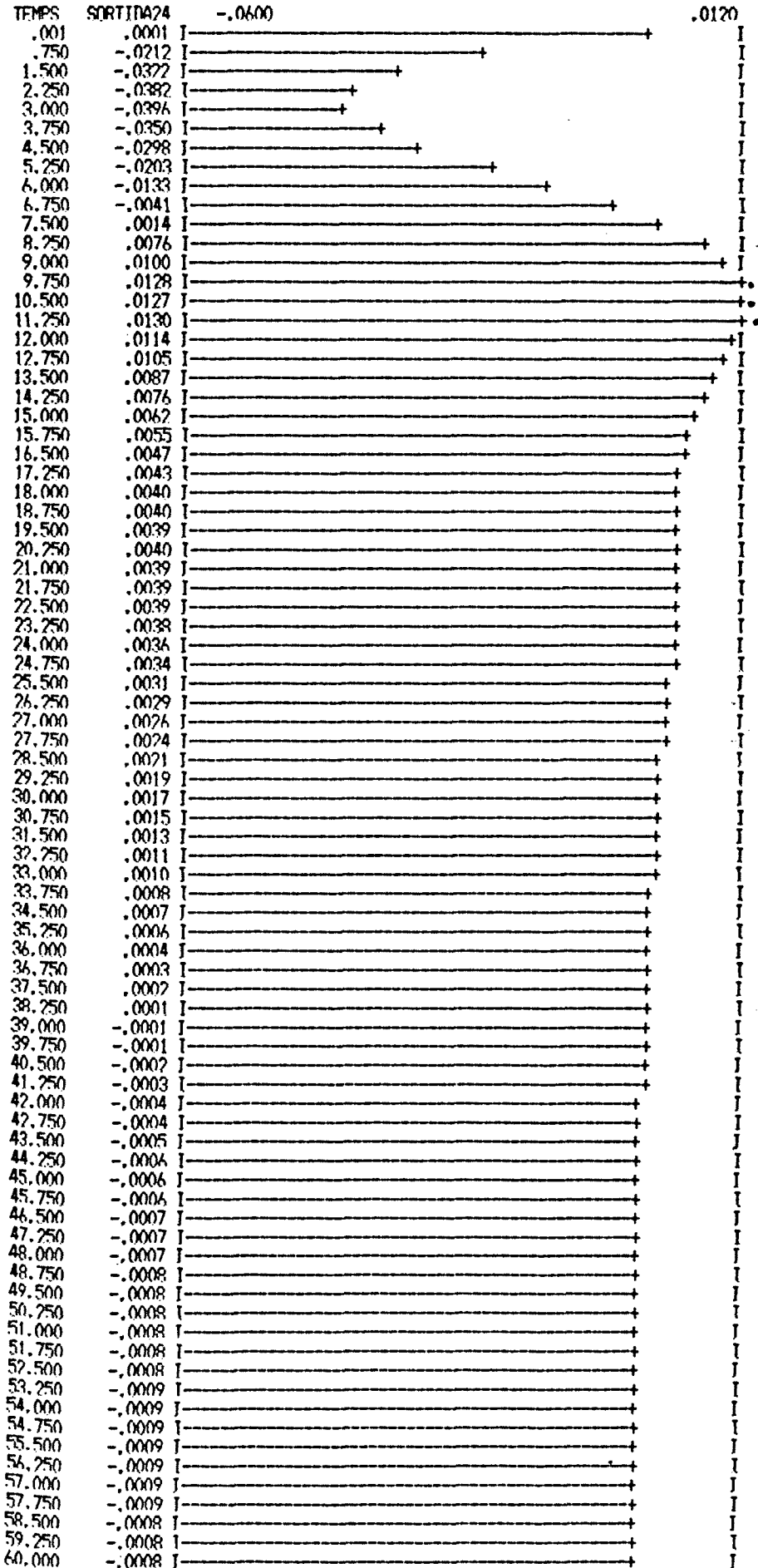
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CONDICIONES INICIALES

Ejemplo de aplicación del programa de cálculo de la matriz de Riccati (matriz P).

BLOC FIX Y (24) MINIM (-.0600) MAXIM (.0120)

S1.1



S1:

Regulación PI convencional en las dos áreas.

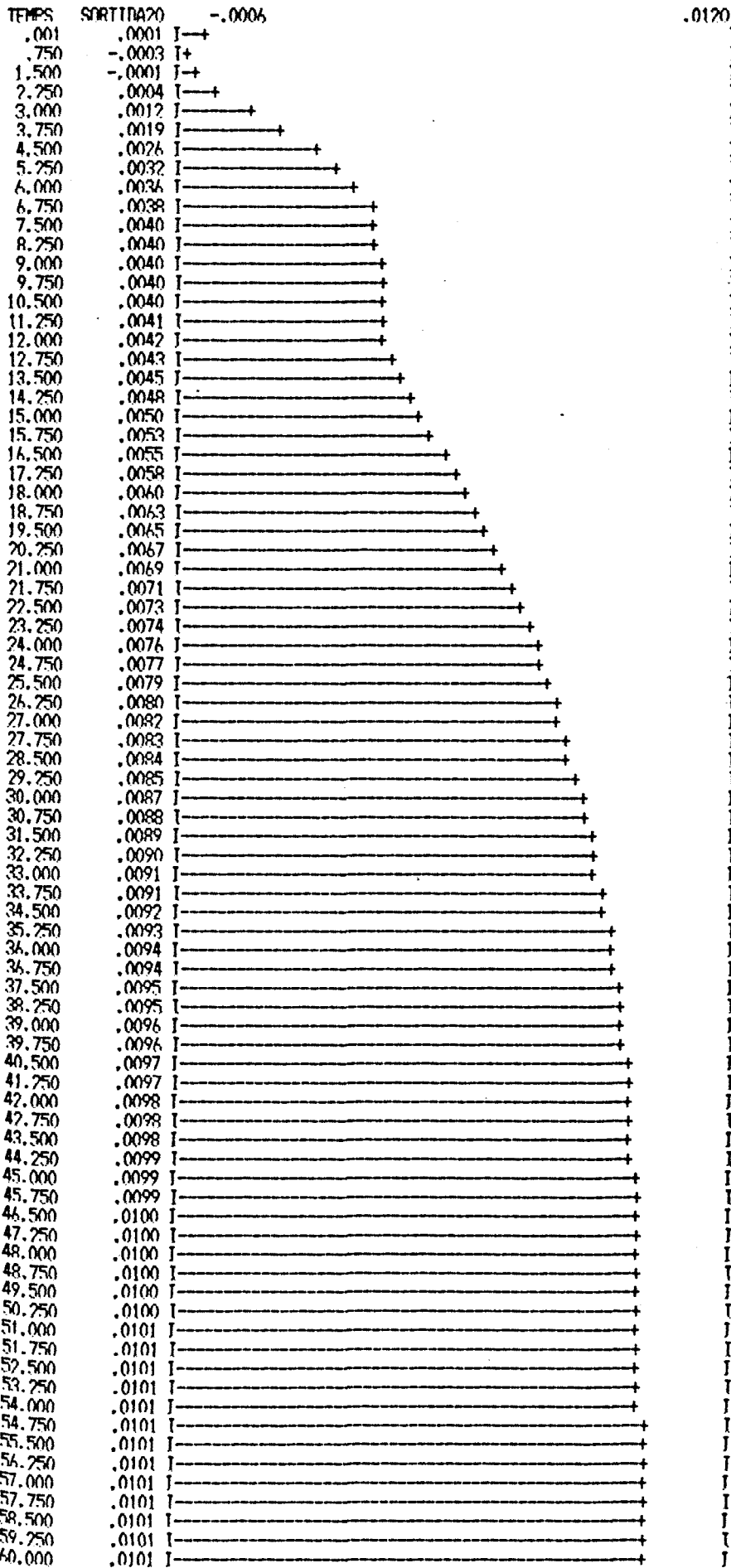
Ganancias de los reguladores:

Area 1 : $K_1 = 0,8$

Area 2 : $K_2 = 0,02$

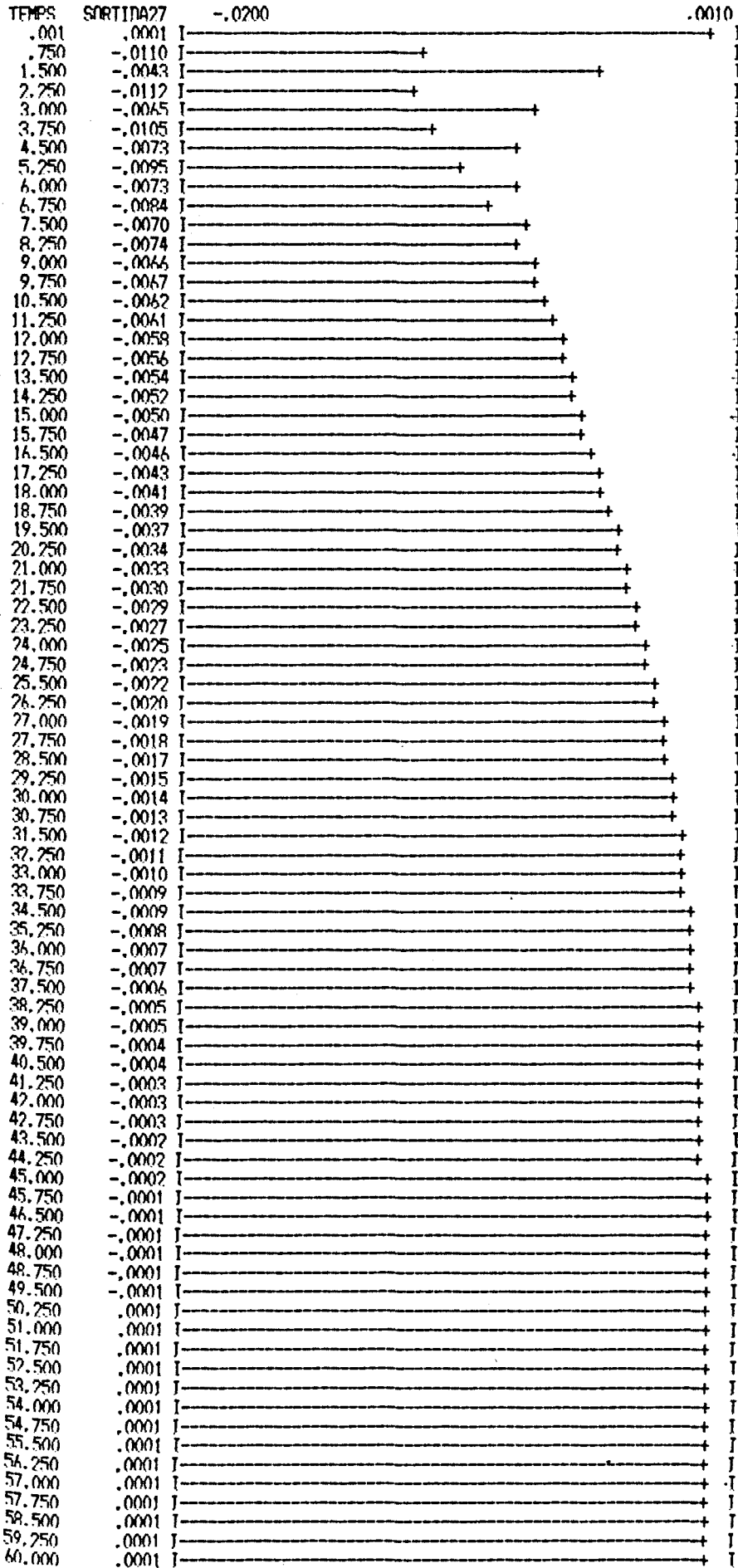
BLOC FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S1.2



BLOC FIX Y (27) MINIM (-.0200) MAXIM (.0010)

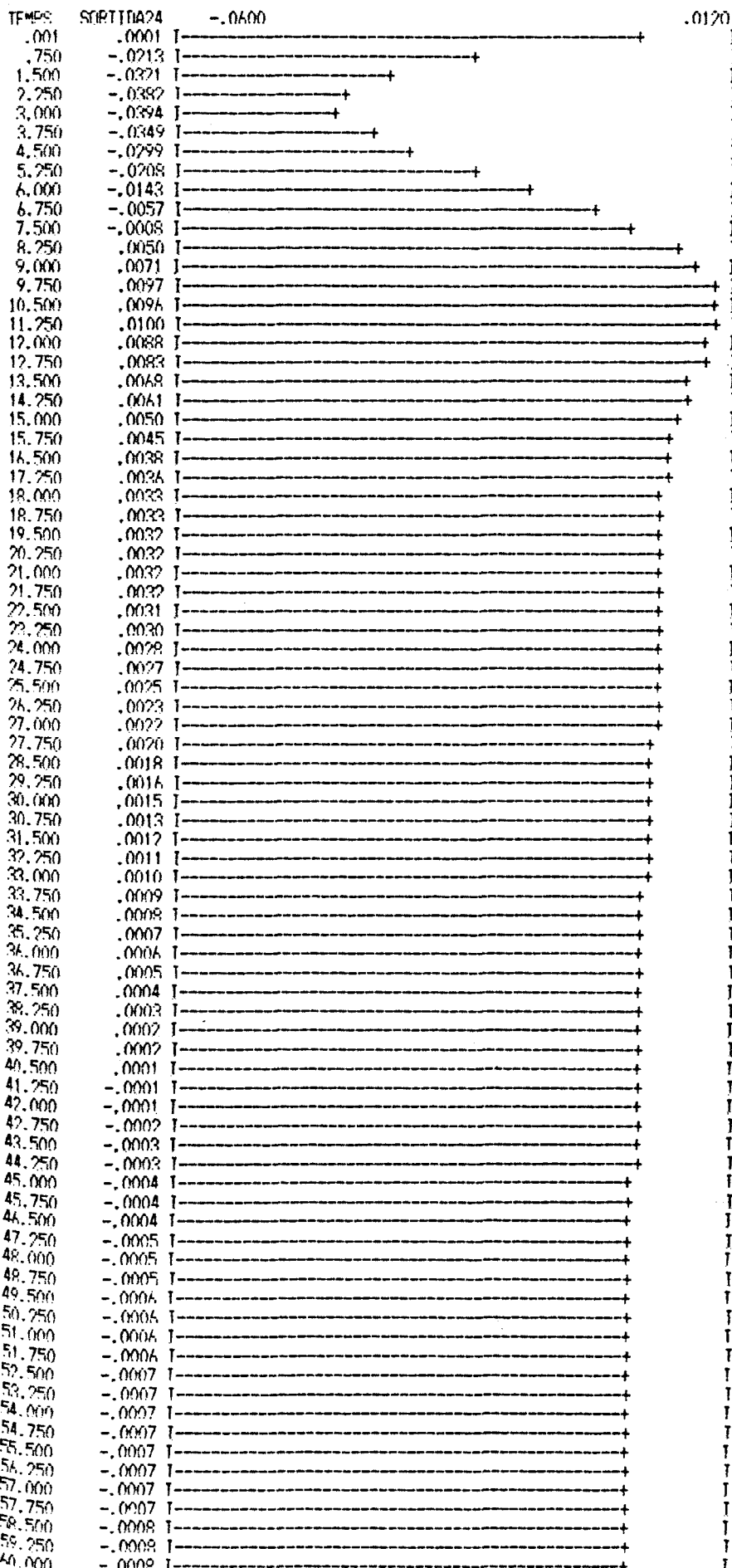
S1.3



TEMPS	SORTIDA46	SORTIDA41	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	.0131	.0014	.0002
4.00	-.0427	.0313	.0043	.0003
6.00	-.0633	.0477	.0054	.0005
8.00	-.0792	.0630	.0055	.0006
10.00	-.0909	.0766	.0057	.0007
12.00	-.1006	.0886	.0060	.0007
14.00	-.1099	.0996	.0062	.0008
16.00	-.1185	.1094	.0063	.0009
18.00	-.1264	.1181	.0064	.0009
20.00	-.1332	.1256	.0064	.0009
22.00	-.1388	.1320	.0064	.0009
24.00	-.1435	.1374	.0064	.0010
26.00	-.1474	.1419	.0065	.0010
28.00	-.1507	.1456	.0065	.0010
30.00	-.1534	.1487	.0065	.0010
32.00	-.1556	.1512	.0065	.0010
34.00	-.1574	.1531	.0065	.0010
36.00	-.1589	.1546	.0065	.0010
38.00	-.1600	.1558	.0065	.0010
40.00	-.1608	.1567	.0065	.0010
42.00	-.1615	.1573	.0065	.0010
44.00	-.1620	.1577	.0065	.0010
46.00	-.1623	.1579	.0065	.0010
48.00	-.1626	.1581	.0065	.0010
50.00	-.1627	.1581	.0065	.0010
52.00	-.1628	.1581	.0065	.0010
54.00	-.1629	.1582	.0065	.0010
56.00	-.1629	.1584	.0065	.0010
58.00	-.1628	.1586	.0065	.0010
60.00	-.1628	.1587	.0065	.0010
62.00	-.1628	.1589	.0065	.0010
64.00	-.1627	.1591	.0065	.0010
66.00	-.1626	.1593	.0065	.0010
68.00	-.1626	.1595	.0065	.0010
70.00	-.1625	.1597	.0065	.0010
72.00	-.1625	.1598	.0065	.0010
74.00	-.1624	.1600	.0065	.0010
76.00	-.1624	.1601	.0065	.0010
78.00	-.1623	.1602	.0065	.0010
80.00	-.1623	.1604	.0065	.0010
82.00	-.1622	.1605	.0065	.0010
84.00	-.1622	.1606	.0065	.0010
86.00	-.1622	.1606	.0065	.0010
88.00	-.1622	.1607	.0065	.0010
90.00	-.1622	.1608	.0065	.0010
92.00	-.1622	.1608	.0065	.0010
94.00	-.1621	.1609	.0065	.0010
96.00	-.1621	.1609	.0065	.0010
98.00	-.1621	.1610	.0065	.0010
100.00	-.1621	.1610	.0065	.0010
102.00	-.1621	.1610	.0065	.0010
104.00	-.1621	.1610	.0065	.0010
106.00	-.1621	.1611	.0065	.0010
108.00	-.1621	.1611	.0065	.0010
110.00	-.1621	.1611	.0065	.0010
112.00	-.1621	.1611	.0065	.0010
114.00	-.1621	.1611	.0065	.0010
116.00	-.1621	.1611	.0065	.0010
118.00	-.1621	.1611	.0065	.0010
120.00	-.1621	.1612	.0065	.0010
122.00	-.1621	.1612	.0065	.0010
124.00	-.1621	.1612	.0065	.0010
126.00	-.1621	.1612	.0065	.0010
128.00	-.1621	.1612	.0065	.0010
130.00	-.1621	.1612	.0065	.0010
132.00	-.1622	.1612	.0065	.0010
134.00	-.1622	.1612	.0065	.0010
136.00	-.1622	.1612	.0065	.0010
138.00	-.1622	.1612	.0065	.0010
140.00	-.1622	.1612	.0065	.0010
142.00	-.1622	.1612	.0065	.0010
144.00	-.1622	.1612	.0065	.0010
146.00	-.1622	.1612	.0065	.0010
148.00	-.1622	.1612	.0065	.0010
150.00	-.1622	.1612	.0065	.0010
152.00	-.1622	.1612	.0065	.0010
154.00	-.1622	.1612	.0065	.0010
156.00	-.1622	.1612	.0065	.0010
158.00	-.1622	.1612	.0065	.0010
160.00	-.1622	.1612	.0065	.0010

RUC FIX Y (24) MINIM (-.0600) MAXIM (.0120)

S2.1



S2.

RLO en Area 1

PI en Area 2

$$\tilde{Q} = \text{diag}(0,5;0,5;0,5;0,5;0,5;0,5)$$

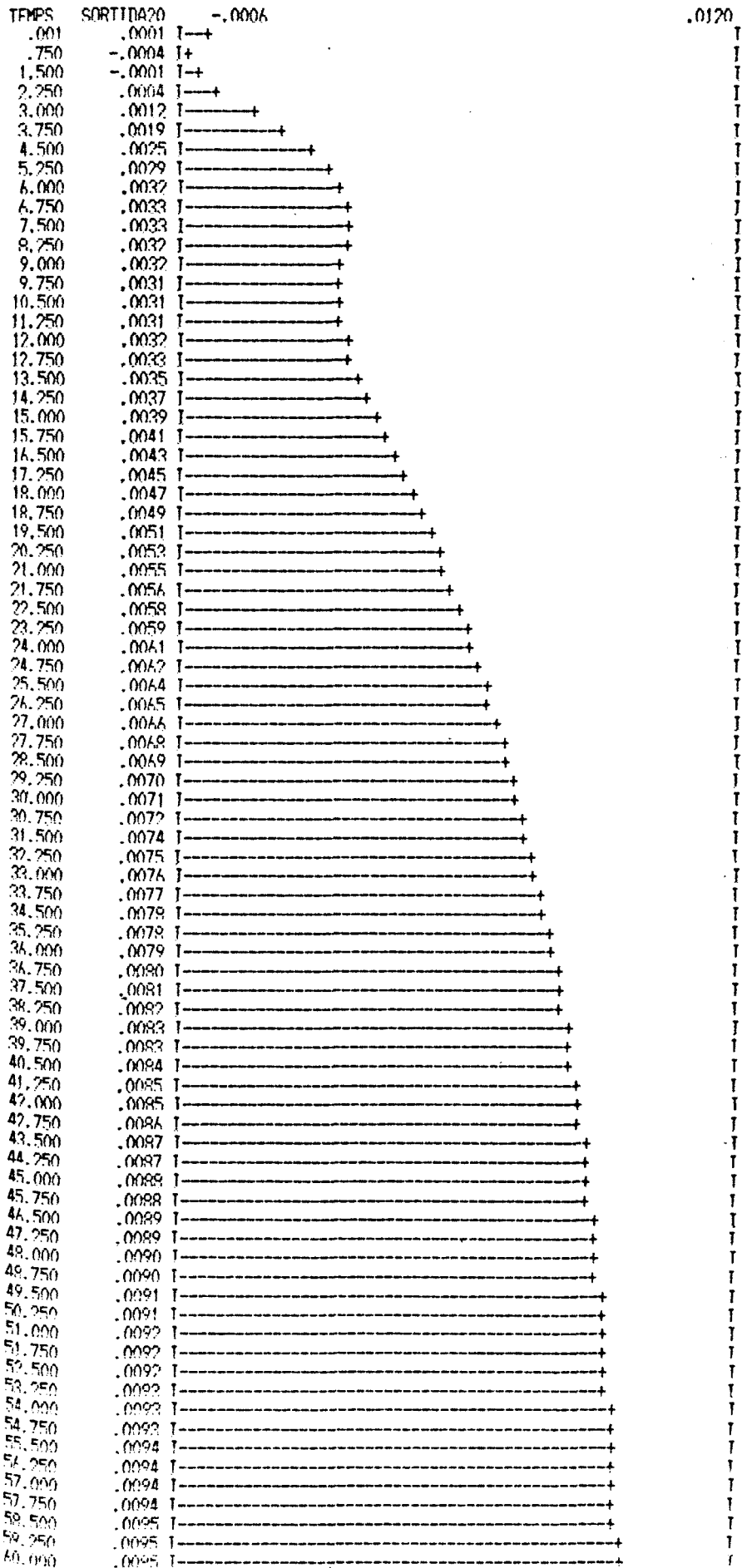
$$\tilde{R} = I$$

$$\tilde{e}_0 = 0$$

Estructura de diseño convencional
(desacoplo del modelo del Area por
la línea de interconexión).

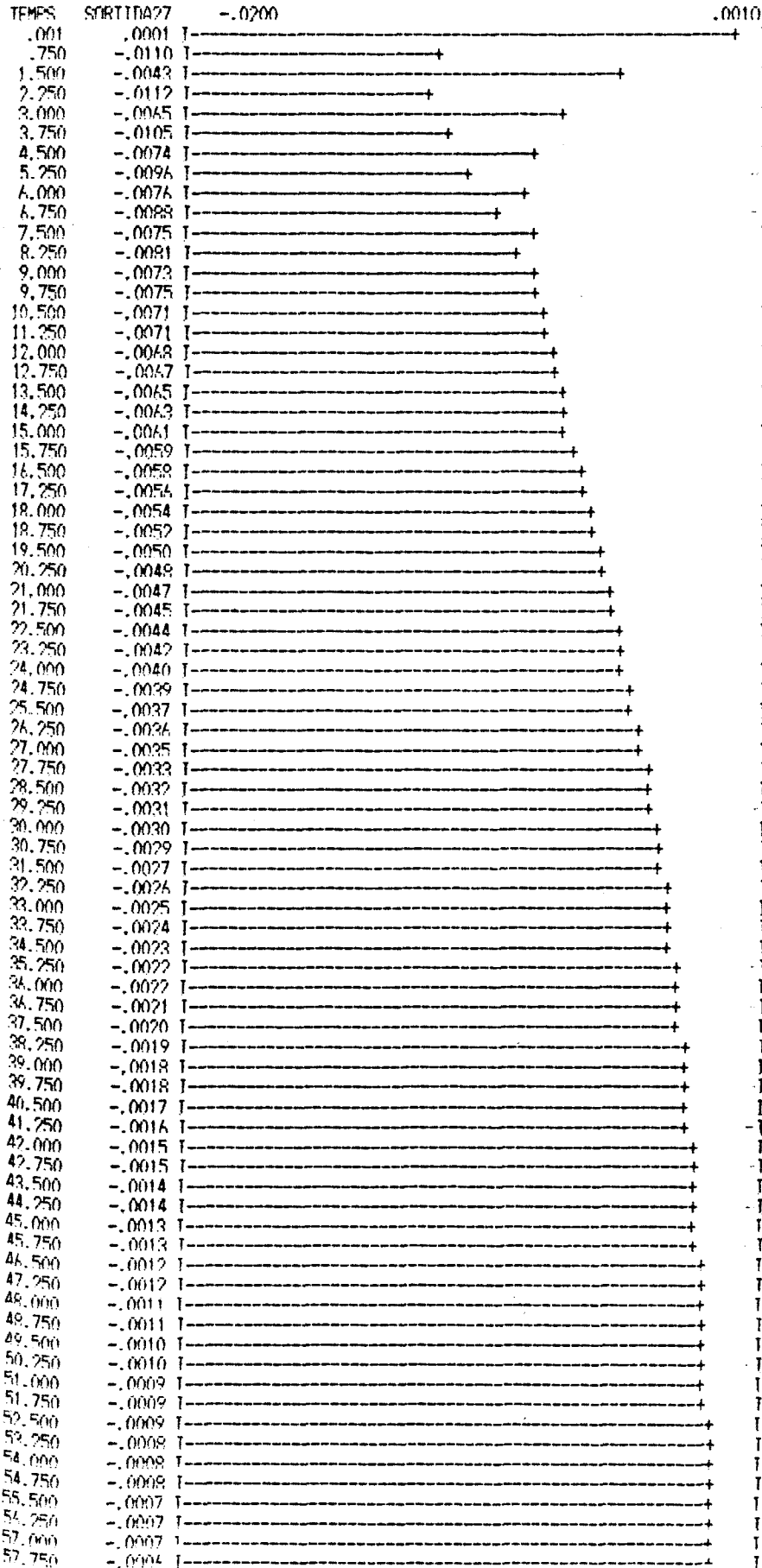
BLDC FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S2.2



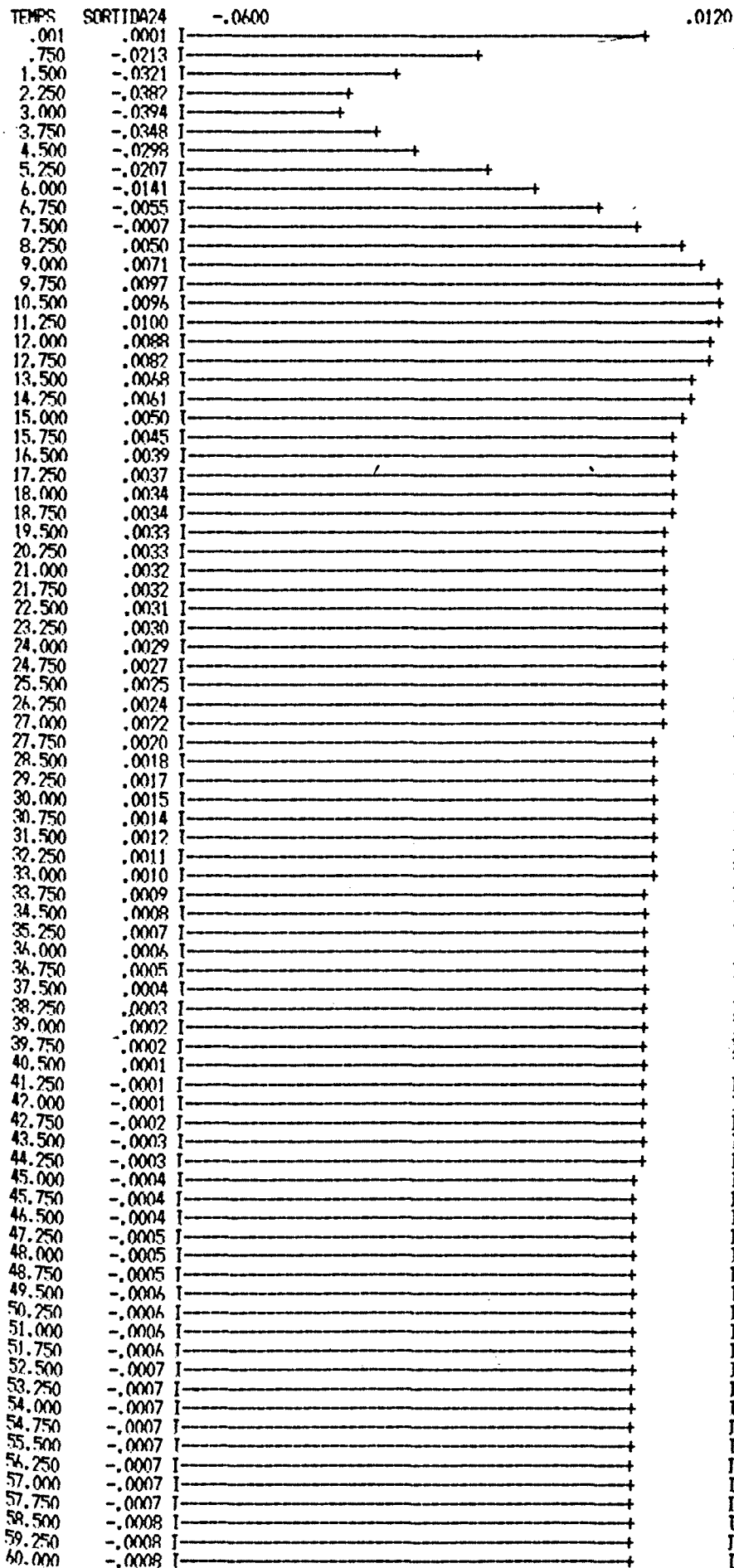
S2.3

RUC FIX Y (27) MINIM (-.0200) MAXIM (.0010)



BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S3.1



S3:

IRLO en Area 1.

IPI en Area 2.

$$\tilde{I}Q = \text{diag}(0,5;0,5;0,5;0,5;0,5;0,5;0,5)$$

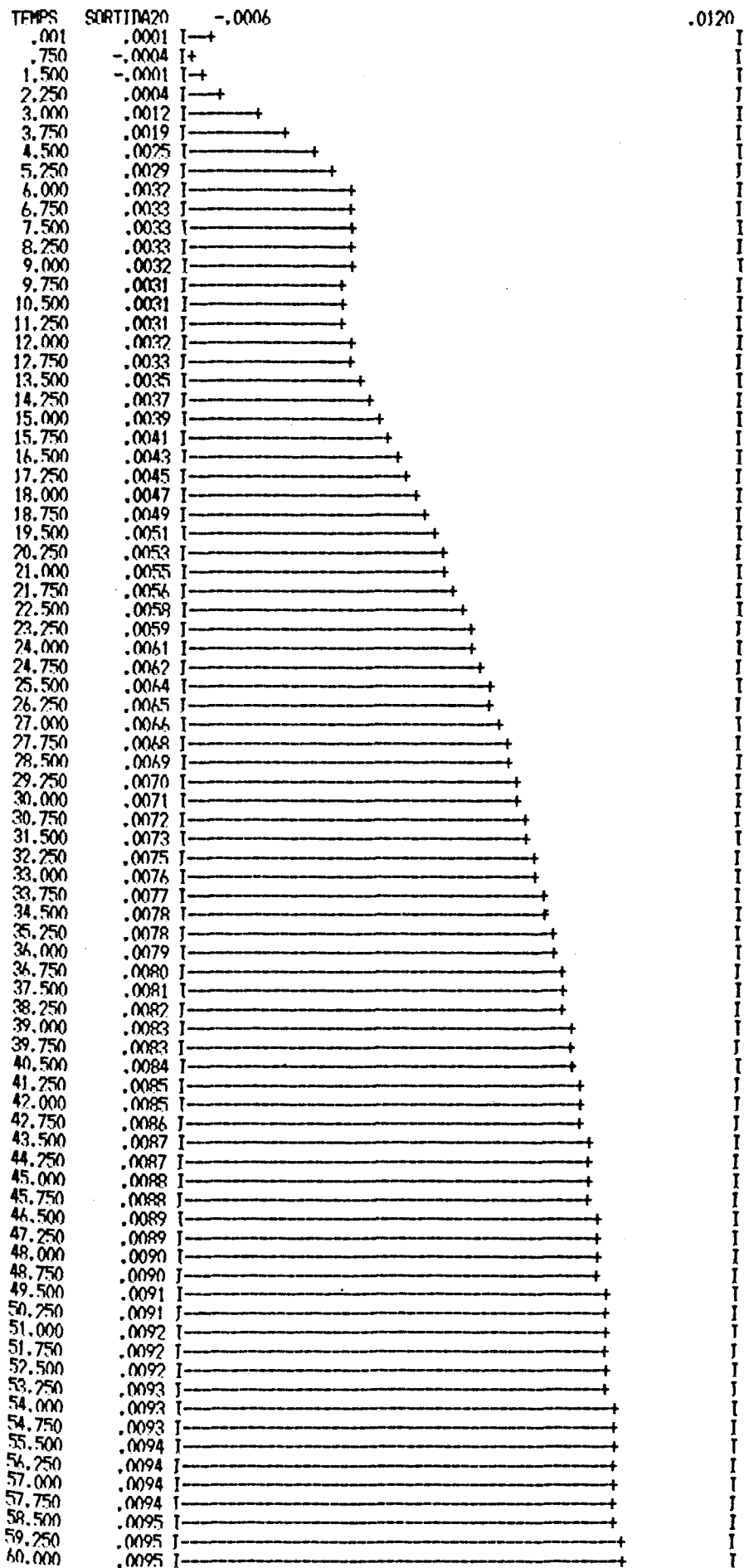
$$\tilde{R} = \tilde{I}$$

$$\alpha_0 = 0$$

Inclusión de la carga externa en el diseño del RLO descentralizado del Area 1.

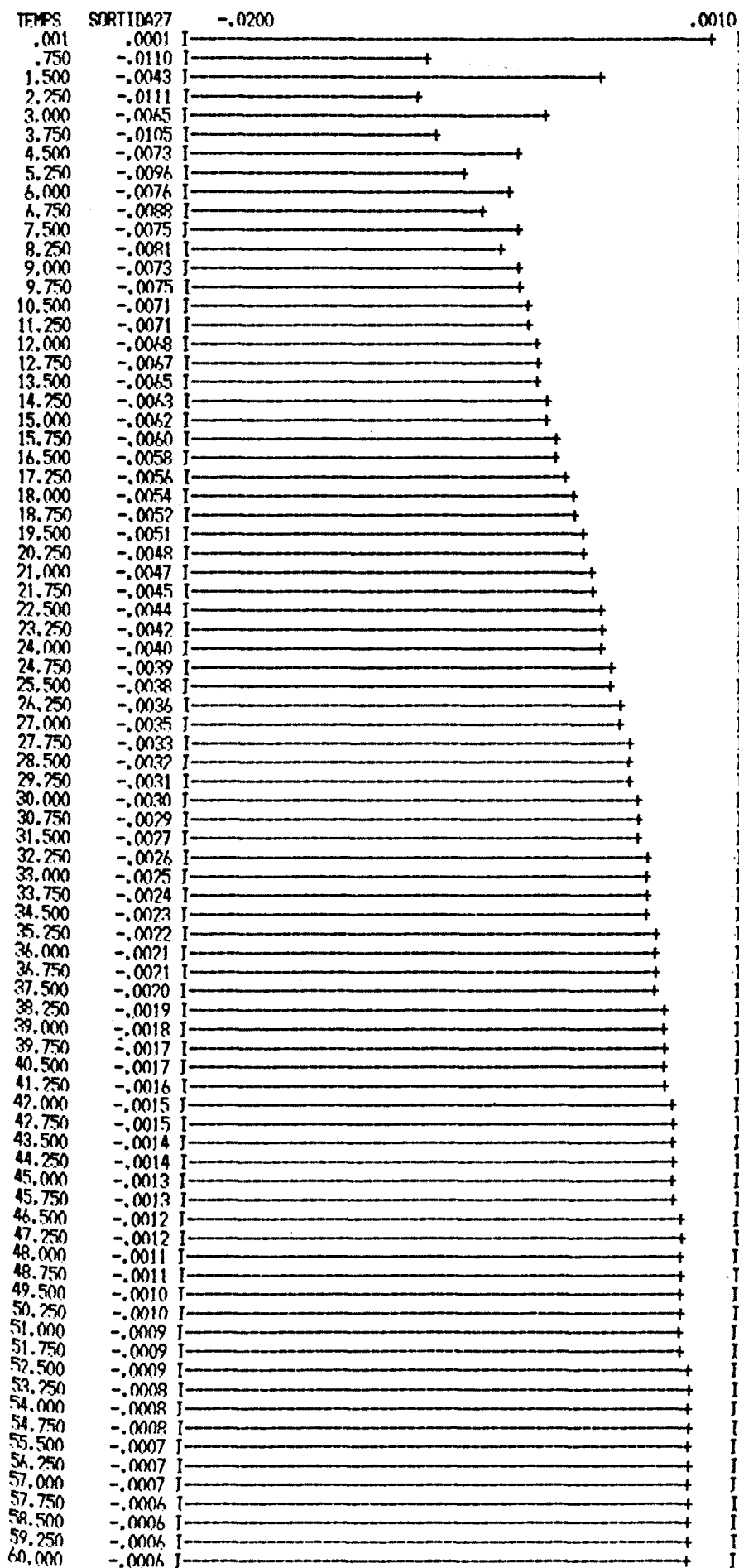
BLOC EIX Y (20) MINIM (-.0006) MAXIM (.0120)

S3.2



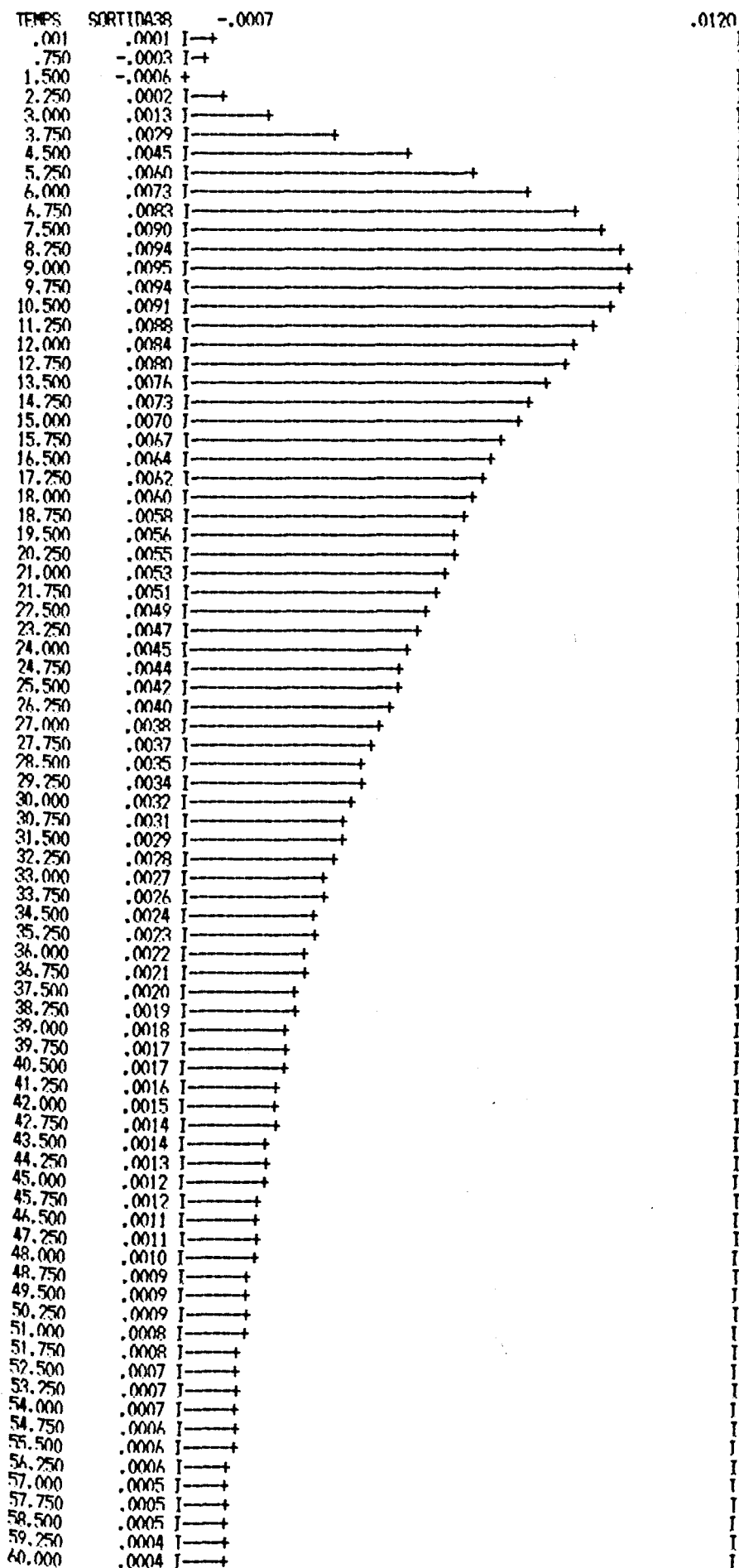
BLOC FIX Y (27) MINIM (-.0200) MAXIM (.0010)

S3.3



BLOC FTX Y (38) MINIM (-.0007) MAXIM (.0120)

S3.4



TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0336	.0014	.0002
4.00	-.0426	-.0359	.0043	.0003
6.00	-.0635	-.0127	.0054	.0005
8.00	-.0805	.0030	.0055	.0006
10.00	-.0942	.0091	.0056	.0007
12.00	-.1064	.0091	.0058	.0008
14.00	-.1182	.0060	.0059	.0009
16.00	-.1294	.0041	.0060	.0010
18.00	-.1399	.0033	.0060	.0010
20.00	-.1496	.0031	.0060	.0011
22.00	-.1582	.0030	.0061	.0011
24.00	-.1661	.0027	.0061	.0012
26.00	-.1732	.0023	.0061	.0012
28.00	-.1796	.0018	.0061	.0012
30.00	-.1855	.0014	.0061	.0012
32.00	-.1908	.0010	.0061	.0012
34.00	-.1954	.0007	.0061	.0013
36.00	-.1999	.0005	.0061	.0013
38.00	-.2038	.0003	.0061	.0013
40.00	-.2073	.0001	.0061	.0013
42.00	-.2105	-.0002	.0061	.0013
44.00	-.2133	-.0003	.0061	.0013
46.00	-.2159	-.0005	.0061	.0013
48.00	-.2187	-.0005	.0061	.0013
50.00	-.2203	-.0006	.0061	.0013
52.00	-.2222	-.0007	.0061	.0013
54.00	-.2239	-.0007	.0061	.0013
56.00	-.2254	-.0008	.0061	.0013
58.00	-.2267	-.0008	.0061	.0013
60.00	-.2280	-.0008	.0061	.0013
62.00	-.2290	-.0008	.0061	.0013
64.00	-.2300	-.0008	.0061	.0013
66.00	-.2309	-.0008	.0061	.0013
68.00	-.2317	-.0008	.0061	.0013
70.00	-.2324	-.0007	.0061	.0013
72.00	-.2331	-.0007	.0061	.0013
74.00	-.2337	-.0007	.0061	.0013
76.00	-.2342	-.0007	.0061	.0013
78.00	-.2346	-.0007	.0061	.0013
80.00	-.2350	-.0006	.0061	.0013
82.00	-.2354	-.0006	.0061	.0013
84.00	-.2358	-.0006	.0061	.0013
86.00	-.2361	-.0005	.0061	.0013
88.00	-.2363	-.0005	.0061	.0013
90.00	-.2366	-.0005	.0061	.0013
92.00	-.2368	-.0005	.0061	.0013
94.00	-.2370	-.0004	.0061	.0013
96.00	-.2372	-.0004	.0061	.0013
98.00	-.2373	-.0004	.0061	.0013
100.00	-.2375	-.0004	.0061	.0013
102.00	-.2376	-.0004	.0061	.0013
104.00	-.2377	-.0003	.0061	.0013
106.00	-.2378	-.0003	.0061	.0013
108.00	-.2379	-.0003	.0061	.0013
110.00	-.2380	-.0003	.0061	.0013
112.00	-.2380	-.0003	.0061	.0013
114.00	-.2381	-.0003	.0061	.0013
116.00	-.2382	-.0002	.0061	.0013
118.00	-.2382	-.0002	.0061	.0013
120.00	-.2383	-.0002	.0061	.0013
122.00	-.2383	-.0002	.0061	.0013
124.00	-.2383	-.0002	.0061	.0013
126.00	-.2384	-.0002	.0061	.0013
128.00	-.2384	-.0002	.0061	.0013
130.00	-.2384	-.0002	.0061	.0013
132.00	-.2385	-.0002	.0061	.0013
134.00	-.2385	-.0002	.0061	.0013
136.00	-.2385	-.0001	.0061	.0013
138.00	-.2385	-.0001	.0061	.0013
140.00	-.2385	-.0001	.0061	.0013
142.00	-.2385	-.0001	.0061	.0013
144.00	-.2386	-.0001	.0061	.0013
146.00	-.2386	-.0001	.0061	.0013
148.00	-.2386	-.0001	.0061	.0013
150.00	-.2386	-.0001	.0061	.0013
152.00	-.2386	-.0001	.0061	.0013
154.00	-.2386	-.0001	.0061	.0013
156.00	-.2386	-.0001	.0061	.0013
158.00	-.2386	-.0001	.0061	.0013

S3.5

TEMPS	20	24	27	30
.00	.0001	.0001	.0001	.0001
.60	-.0004	-.0218	-.0098	-.0130
1.20	-.0002	-.0231	-.0064	-.0321
1.80	.0001	-.0397	-.0072	-.0305
2.40	.0006	-.0364	-.0104	-.0415
3.00	.0012	-.0394	-.0065	-.0376
3.60	.0017	-.0375	-.0105	-.0359
4.20	.0023	-.0300	-.0077	-.0335
4.80	.0027	-.0283	-.0087	-.0247
5.40	.0030	-.0189	-.0089	-.0221
6.00	.0032	-.0151	-.0074	-.0137
6.60	.0033	-.0090	-.0088	-.0094
7.20	.0033	-.0038	-.0072	-.0049
7.80	.0033	-.0014	-.0079	-.0002
8.40	.0033	.0029	-.0075	.0013
9.00	.0032	.0036	-.0070	.0044
9.60	.0032	.0052	-.0074	.0046
10.20	.0032	.0055	-.0067	.0053
10.80	.0033	.0051	-.0070	.0053
11.40	.0033	.0051	-.0066	.0044
12.00	.0034	.0040	-.0065	.0043
12.60	.0035	.0036	-.0065	.0031
13.20	.0037	.0027	-.0062	.0027
13.80	.0038	.0020	-.0063	.0020
14.40	.0040	.0017	-.0060	.0013
15.00	.0041	.0011	-.0059	.0011
15.60	.0043	.0010	-.0058	.0007
16.20	.0045	.0007	-.0055	.0007
16.80	.0047	.0007	-.0055	.0006
17.40	.0048	.0008	-.0053	.0006
18.00	.0050	.0008	-.0052	.0008
18.60	.0051	.0011	-.0050	.0008
19.20	.0053	.0011	-.0049	.0010
19.80	.0054	.0013	-.0048	.0011
20.40	.0055	.0014	-.0046	.0013
21.00	.0057	.0015	-.0045	.0014
21.60	.0058	.0016	-.0044	.0015
22.20	.0059	.0016	-.0042	.0015
22.80	.0060	.0017	-.0041	.0015
23.40	.0061	.0017	-.0040	.0015
24.00	.0062	.0016	-.0039	.0015
24.60	.0063	.0016	-.0038	.0015
25.20	.0064	.0016	-.0037	.0015
25.80	.0065	.0015	-.0036	.0014
26.40	.0066	.0015	-.0035	.0014
27.00	.0067	.0014	-.0034	.0013
27.60	.0068	.0014	-.0033	.0013
28.20	.0069	.0013	-.0032	.0012
28.80	.0070	.0013	-.0031	.0012
29.40	.0071	.0013	-.0030	.0012
30.00	.0072	.0012	-.0029	.0011
30.60	.0073	.0012	-.0028	.0011
31.20	.0074	.0012	-.0027	.0011
31.80	.0075	.0012	-.0027	.0011
32.40	.0075	.0011	-.0026	.0010
33.00	.0076	.0011	-.0025	.0010
33.60	.0077	.0011	-.0024	.0010
34.20	.0078	.0011	-.0024	.0010
34.80	.0078	.0010	-.0023	.0010
35.40	.0079	.0010	-.0022	.0009
36.00	.0080	.0010	-.0022	.0009
36.60	.0080	.0010	-.0021	.0009
37.20	.0081	.0009	-.0020	.0009
37.80	.0081	.0009	-.0020	.0009
38.40	.0082	.0009	-.0019	.0008
39.00	.0083	.0009	-.0019	.0008
39.60	.0083	.0008	-.0018	.0008
40.20	.0084	.0008	-.0017	.0008
40.80	.0084	.0008	-.0017	.0007
41.40	.0085	.0008	-.0016	.0007
42.00	.0085	.0008	-.0016	.0007
42.60	.0086	.0007	-.0015	.0007
43.20	.0086	.0007	-.0015	.0007
43.80	.0086	.0007	-.0015	.0006
44.40	.0087	.0007	-.0014	.0006
45.00	.0087	.0007	-.0014	.0006
45.60	.0088	.0006	-.0013	.0006
46.20	.0088	.0006	-.0013	.0006
46.80	.0089	.0006	-.0013	.0006
47.40	.0089	.0006	-.0012	.0006
48.00	.0089	.0006	-.0012	.0005

S4.1

S4:

Igual que S3 cuando la generación del Area 2 se limita a la primaria:

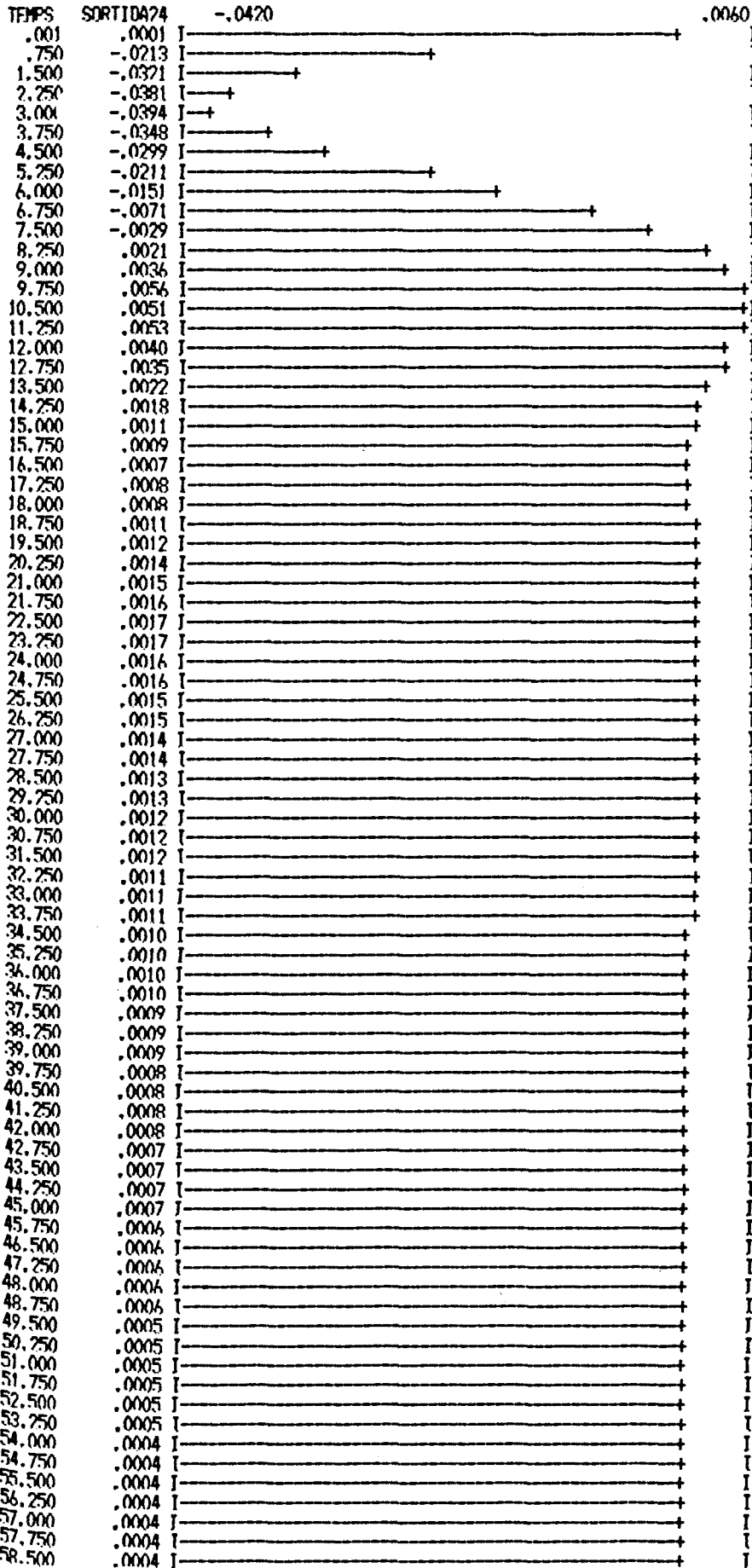
S4.2

48.00	.0089	.0006	-.0012	.0005
48.05	.0089	.0006	-.0012	.0005
48.60	.0090	.0006	-.0011	.0005
49.20	.0090	.0005	-.0011	.0005
49.80	.0090	.0005	-.0011	.0005
50.40	.0091	.0005	-.0010	.0005
51.00	.0091	.0005	-.0010	.0005
51.60	.0091	.0005	-.0010	.0005
52.20	.0091	.0005	-.0010	.0004
52.80	.0092	.0005	-.0009	.0004
53.40	.0092	.0004	-.0009	.0004
54.00	.0092	.0004	-.0009	.0004
54.60	.0093	.0004	-.0008	.0004
55.20	.0093	.0004	-.0008	.0004
55.80	.0093	.0004	-.0008	.0004
56.40	.0093	.0004	-.0008	.0004
57.00	.0093	.0004	-.0008	.0004
57.60	.0094	.0004	-.0007	.0003
58.20	.0094	.0004	-.0007	.0003
58.80	.0094	.0004	-.0007	.0003
59.40	.0094	.0003	-.0007	.0003
60.00	.0095	.0003	-.0007	.0003
60.60	.0095	.0003	-.0006	.0003
61.20	.0095	.0003	-.0006	.0003
61.80	.0095	.0003	-.0006	.0003
62.40	.0095	.0003	-.0006	.0003
63.00	.0095	.0003	-.0006	.0003
63.60	.0096	.0003	-.0005	.0003
64.20	.0096	.0003	-.0005	.0003
64.80	.0096	.0003	-.0005	.0003
65.40	.0096	.0003	-.0005	.0002
66.00	.0096	.0003	-.0005	.0002
66.60	.0096	.0003	-.0005	.0002
67.20	.0096	.0002	-.0005	.0002
67.80	.0097	.0002	-.0004	.0002
68.40	.0097	.0002	-.0004	.0002
69.00	.0097	.0002	-.0004	.0002
69.60	.0097	.0002	-.0004	.0002
70.20	.0097	.0002	-.0004	.0002
70.80	.0097	.0002	-.0004	.0002
71.40	.0097	.0002	-.0004	.0002
72.00	.0097	.0002	-.0004	.0002
72.60	.0097	.0002	-.0004	.0002
73.20	.0098	.0002	-.0004	.0002
73.80	.0098	.0002	-.0003	.0002
74.40	.0098	.0002	-.0003	.0002
75.00	.0098	.0002	-.0003	.0002
75.60	.0098	.0002	-.0003	.0002
76.20	.0098	.0002	-.0003	.0002
76.80	.0098	.0002	-.0003	.0002
77.40	.0098	.0002	-.0003	.0002
78.00	.0098	.0002	-.0003	.0002
78.60	.0098	.0002	-.0003	.0001
79.20	.0098	.0002	-.0003	.0001
79.80	.0098	.0002	-.0003	.0001
80.40	.0098	.0001	-.0003	.0001
81.00	.0099	.0001	-.0002	.0001
81.60	.0099	.0001	-.0002	.0001
82.20	.0099	.0001	-.0002	.0001
82.80	.0099	.0001	-.0002	.0001
83.40	.0099	.0001	-.0002	.0001
84.00	.0099	.0001	-.0002	.0001
84.60	.0099	.0001	-.0002	.0001
85.20	.0099	.0001	-.0002	.0001
85.80	.0099	.0001	-.0002	.0001
86.40	.0099	.0001	-.0002	.0001
87.00	.0099	.0001	-.0002	.0001
87.60	.0099	.0001	-.0002	.0001
88.20	.0099	.0001	-.0002	.0001
88.80	.0099	.0001	-.0002	.0001
89.40	.0099	.0001	-.0002	.0001
90.00	.0099	.0001	-.0002	.0001
90.60	.0099	.0001	-.0002	.0001
91.20	.0099	.0001	-.0002	.0001
91.80	.0099	.0001	-.0002	.0001
92.40	.0099	.0001	-.0002	.0001
93.00	.0099	.0001	-.0002	.0001
93.60	.0099	.0001	-.0002	.0001
94.20	.0100	.0001	-.0001	.0001
94.80	.0100	.0001	-.0001	.0001
95.40	.0100	.0001	-.0001	.0001
96.00	.0100	.0001	-.0001	.0001

59.250	.0094	I	-----+	I
60.000	.0095	I	-----+	I

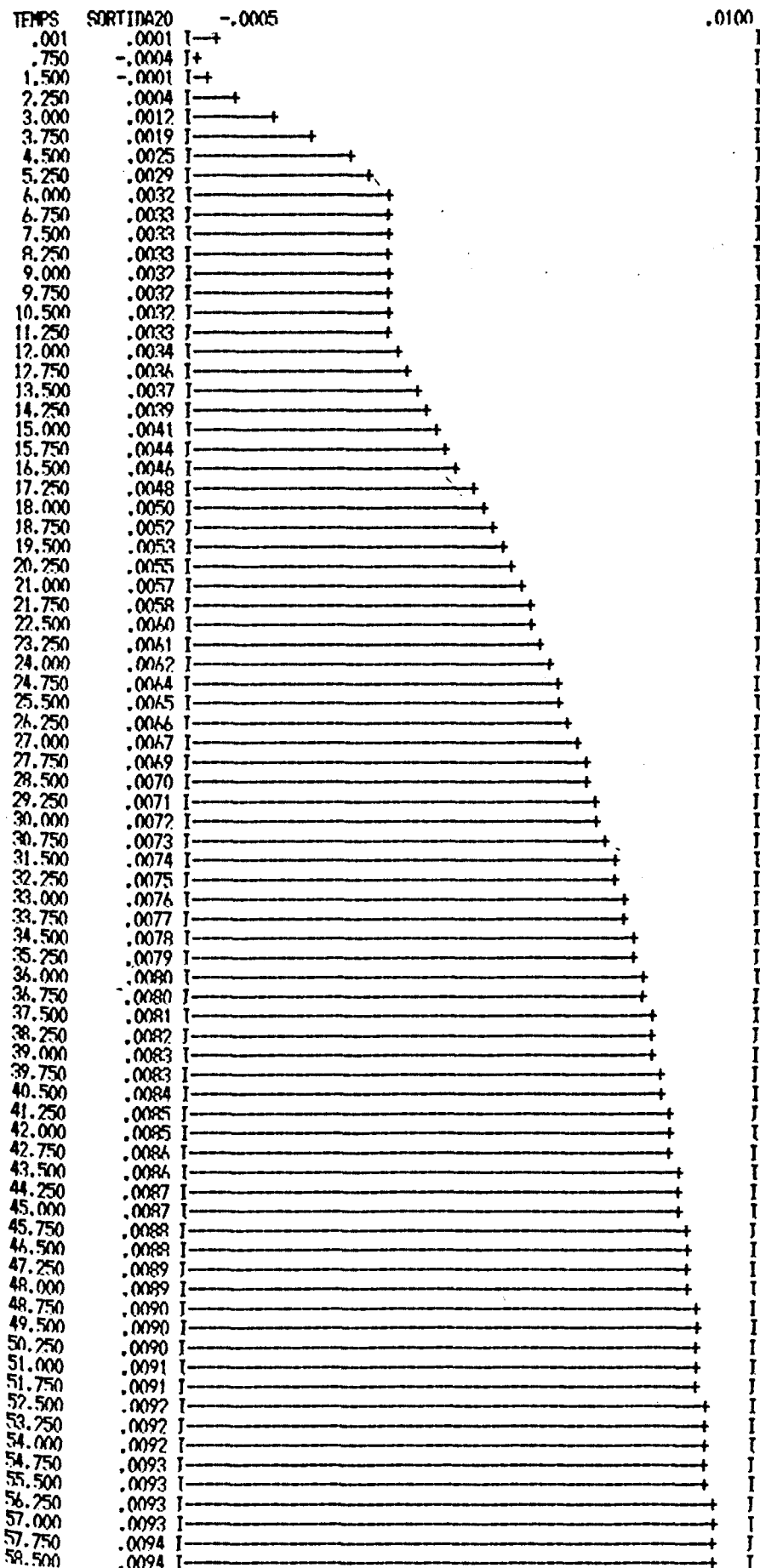
S4.3

BLOC FIX Y (24) MINIM (-.0420) MAXIM (.0060)



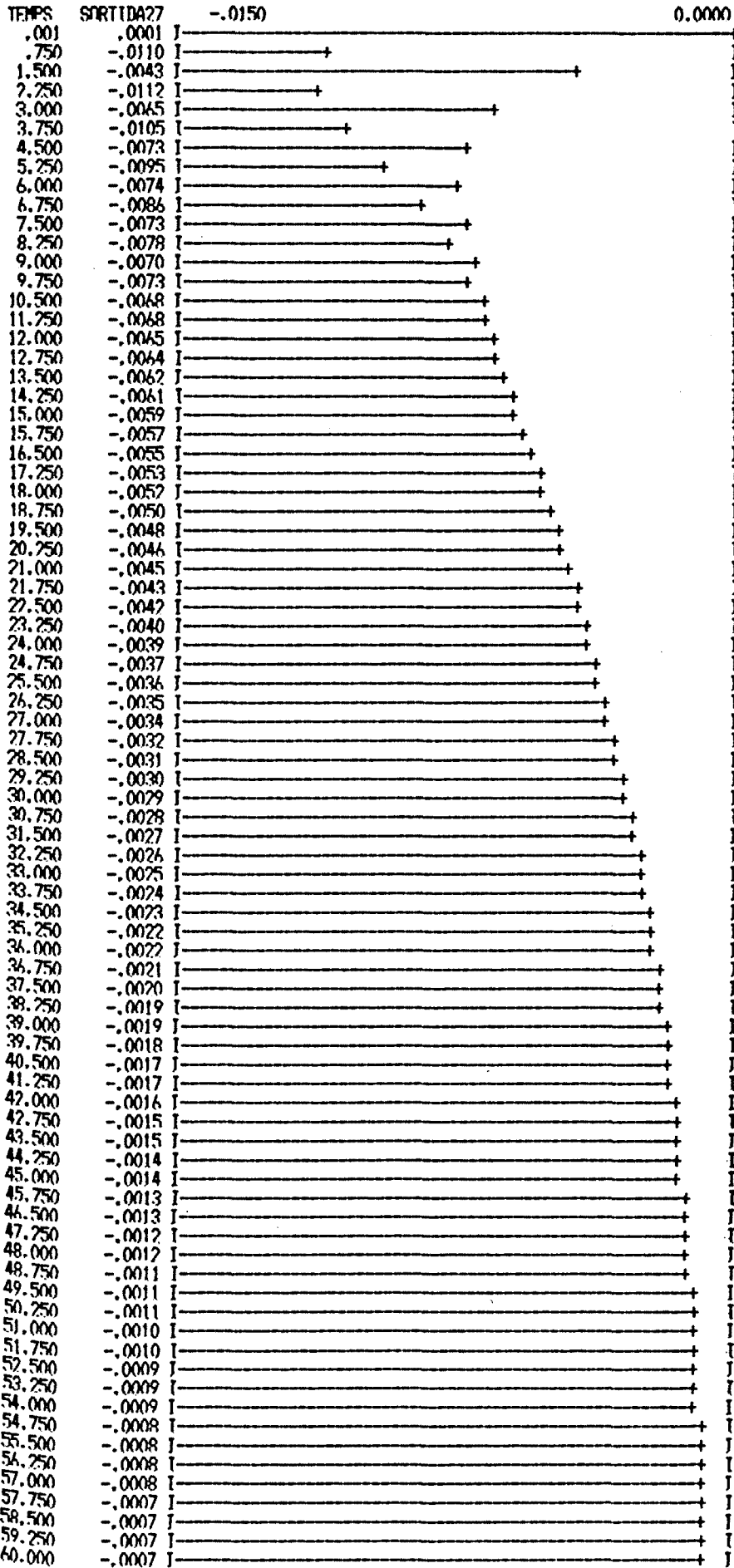
S4.4

BLOC EIX Y (20) MINIM (-.0005) MAXIM (.0100)



BLOC FIX Y (27) MINTH (-.0150) MAXTH (0.0000)

S4.5



59.250 .0003 I
60.000 .0003 I

BLOC FIX Y (30) MINIM (-.0420) MAXIM (.0060)

S4.6

TEMPS	SORTIDA30	-.0420	.0060
.001	.0001		
.750	-.0200		
1.500	-.0307		
2.250	-.0391		
3.000	-.0376		
3.750	-.0366		
4.500	-.0282		
5.250	-.0231		
6.000	-.0137		
6.750	-.0088		
7.500	-.0019		
8.250	.0008		
9.000	.0044		
9.750	.0044		
10.500	.0056		
11.250	.0045		
12.000	.0043		
12.750	.0029		
13.500	.0024		
14.250	.0014		
15.000	.0011		
15.750	.0006		
16.500	.0006		
17.250	.0006		
18.000	.0008		
18.750	.0009		
19.500	.0011		
20.250	.0012		
21.000	.0014		
21.750	.0015		
22.500	.0015		
23.250	.0015		
24.000	.0015		
24.750	.0015		
25.500	.0014		
26.250	.0014		
27.000	.0013		
27.750	.0013		
28.500	.0012		
29.250	.0012		
30.000	.0011		
30.750	.0011		
31.500	.0011		
32.250	.0011		
33.000	.0010		
33.750	.0010		
34.500	.0010		
35.250	.0009		
36.000	.0009		
36.750	.0009		
37.500	.0009		
38.250	.0008		
39.000	.0008		
39.750	.0008		
40.500	.0008		
41.250	.0007		
42.000	.0007		
42.750	.0007		
43.500	.0007		
44.250	.0006		
45.000	.0006		
45.750	.0006		
46.500	.0006		
47.250	.0006		
48.000	.0005		
48.750	.0005		
49.500	.0005		
50.250	.0005		
51.000	.0005		
51.750	.0005		
52.500	.0004		
53.250	.0004		
54.000	.0004		
54.750	.0004		
55.500	.0004		
56.250	.0004		
57.000	.0004		
57.750	.0003		
58.500	.0003		
59.250	.0003		
60.000	.0003		

120.00 -.4526 -.2382 .0001 .0001

ACE1

ACE2

S4.7

TFMPS	SORTIDA46	SORTIDA54	SORTIDA38	SORTIDA20
.00	.0001	.0001	.0001	.0001
1.50	-.0125	-.0473	-.0006	-.0001
3.00	-.0300	-.1371	.0013	.0012
4.50	-.0478	-.2256	.0043	.0025
6.00	-.0634	-.2769	.0069	.0032
7.50	-.0764	-.2884	.0082	.0033
9.00	-.0874	-.2738	.0084	.0032
10.50	-.0973	-.2490	.0079	.0032
12.00	-.1067	-.2252	.0072	.0034
13.50	-.1158	-.2066	.0065	.0037
15.00	-.1246	-.1932	.0060	.0041
16.50	-.1329	-.1827	.0056	.0046
18.00	-.1408	-.1730	.0053	.0050
19.50	-.1481	-.1631	.0051	.0053
21.00	-.1548	-.1527	.0048	.0057
22.50	-.1610	-.1421	.0045	.0060
24.00	-.1667	-.1318	.0042	.0062
25.50	-.1721	-.1221	.0039	.0065
27.00	-.1770	-.1130	.0036	.0067
28.50	-.1817	-.1047	.0033	.0070
30.00	-.1859	-.0970	.0031	.0072
31.50	-.1899	-.0897	.0029	.0074
33.00	-.1936	-.0830	.0027	.0076
34.50	-.1970	-.0767	.0025	.0078
36.00	-.2001	-.0708	.0023	.0080
37.50	-.2030	-.0653	.0022	.0081
39.00	-.2057	-.0602	.0020	.0083
40.50	-.2082	-.0555	.0019	.0084
42.00	-.2105	-.0511	.0017	.0085
43.50	-.2126	-.0470	.0016	.0086
45.00	-.2146	-.0432	.0015	.0087
46.50	-.2164	-.0397	.0014	.0088
48.00	-.2181	-.0365	.0013	.0089
49.50	-.2197	-.0335	.0012	.0090
51.00	-.2211	-.0307	.0011	.0091
52.50	-.2224	-.0281	.0010	.0092
54.00	-.2237	-.0258	.0009	.0092
55.50	-.2248	-.0236	.0009	.0093
57.00	-.2259	-.0215	.0008	.0093
58.50	-.2268	-.0196	.0008	.0094
60.00	-.2277	-.0179	.0007	.0095
61.50	-.2284	-.0163	.0007	.0095
63.00	-.2293	-.0148	.0006	.0095
64.50	-.2300	-.0134	.0006	.0096
66.00	-.2307	-.0122	.0005	.0096
67.50	-.2313	-.0110	.0005	.0096
69.00	-.2318	-.0099	.0005	.0097
70.50	-.2324	-.0089	.0004	.0097
72.00	-.2328	-.0080	.0004	.0097
73.50	-.2333	-.0071	.0004	.0098
75.00	-.2337	-.0063	.0003	.0098
76.50	-.2341	-.0056	.0003	.0098
78.00	-.2344	-.0049	.0003	.0098
79.50	-.2347	-.0043	.0003	.0098
81.00	-.2350	-.0037	.0003	.0099
82.50	-.2353	-.0032	.0002	.0099
84.00	-.2356	-.0027	.0002	.0099
85.50	-.2358	-.0022	.0002	.0099
87.00	-.2360	-.0018	.0002	.0099
88.50	-.2362	-.0014	.0002	.0099
90.00	-.2364	-.0010	.0002	.0099
91.50	-.2366	-.0007	.0002	.0099
93.00	-.2367	-.0004	.0002	.0099
94.50	-.2369	-.0001	.0002	.0100
96.00	-.2370	.0003	.0001	.0100
97.50	-.2371	.0005	.0001	.0100
99.00	-.2373	.0007	.0001	.0100
100.50	-.2374	.0009	.0001	.0100
102.00	-.2375	.0011	.0001	.0100
103.50	-.2375	.0013	.0001	.0100
105.00	-.2376	.0015	.0001	.0100
106.50	-.2377	.0016	.0001	.0100
108.00	-.2378	.0018	.0001	.0100
109.50	-.2378	.0019	.0001	.0100
111.00	-.2379	.0020	.0001	.0100
112.50	-.2380	.0021	.0001	.0100
114.00	-.2380	.0022	.0001	.0100
115.50	-.2381	.0023	.0001	.0100
117.00	-.2381	.0024	.0001	.0100
118.50	-.2381	.0025	.0001	.0100
120.00	-.2382	.0025	.0001	.0100

TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0178	-.0378	.0013	.0002
4.00	-.0416	-.0413	.0043	.0003
6.00	-.0616	-.0332	.0069	.0004
8.00	-.0788	-.0287	.0089	.0005
10.00	-.0933	-.0245	.0102	.0005
12.00	-.1057	-.0207	.0112	.0005
14.00	-.1164	-.0180	.0120	.0006
16.00	-.1256	-.0154	.0125	.0006
18.00	-.1325	-.0132	.0129	.0006
20.00	-.1403	-.0114	.0132	.0006
22.00	-.1461	-.0098	.0134	.0006
24.00	-.1511	-.0084	.0136	.0006
26.00	-.1553	-.0072	.0137	.0006
28.00	-.1590	-.0062	.0138	.0006
30.00	-.1622	-.0053	.0138	.0006
32.00	-.1649	-.0046	.0139	.0006
34.00	-.1672	-.0039	.0139	.0006
36.00	-.1692	-.0034	.0139	.0006
38.00	-.1709	-.0029	.0140	.0006
40.00	-.1723	-.0025	.0140	.0006
42.00	-.1736	-.0022	.0140	.0006
44.00	-.1747	-.0019	.0140	.0006
46.00	-.1756	-.0016	.0140	.0006
48.00	-.1764	-.0014	.0140	.0006
50.00	-.1771	-.0012	.0140	.0006
52.00	-.1776	-.0010	.0140	.0006
54.00	-.1781	-.0009	.0140	.0006
56.00	-.1786	-.0008	.0140	.0006
58.00	-.1789	-.0007	.0140	.0006
60.00	-.1792	-.0006	.0140	.0006
62.00	-.1795	-.0005	.0140	.0006
64.00	-.1797	-.0004	.0140	.0006
66.00	-.1799	-.0004	.0140	.0006
68.00	-.1801	-.0003	.0140	.0006
70.00	-.1803	-.0003	.0140	.0006
72.00	-.1804	-.0003	.0140	.0006
74.00	-.1805	-.0002	.0140	.0006
76.00	-.1806	-.0002	.0140	.0006
78.00	-.1807	-.0002	.0140	.0006
80.00	-.1807	-.0002	.0140	.0006
82.00	-.1808	-.0001	.0140	.0006
84.00	-.1808	-.0001	.0140	.0006
86.00	-.1809	-.0001	.0140	.0006
88.00	-.1809	-.0001	.0140	.0006
90.00	-.1810	-.0001	.0140	.0006
92.00	-.1810	-.0001	.0140	.0006
94.00	-.1810	-.0001	.0140	.0006
96.00	-.1810	-.0001	.0140	.0006
98.00	-.1810	-.0001	.0140	.0006
100.00	-.1811	-.0001	.0140	.0006
102.00	-.1811	-.0001	.0140	.0006
104.00	-.1811	-.0001	.0140	.0006
106.00	-.1811	-.0001	.0140	.0006
108.00	-.1811	-.0001	.0140	.0006
110.00	-.1811	-.0001	.0140	.0006
112.00	-.1811	-.0001	.0140	.0006
114.00	-.1811	-.0001	.0140	.0006
116.00	-.1811	-.0001	.0140	.0006
118.00	-.1811	-.0001	.0140	.0006
120.00	-.1811	-.0001	.0140	.0006
122.00	-.1811	-.0001	.0140	.0006
124.00	-.1811	-.0001	.0140	.0006
126.00	-.1811	-.0001	.0140	.0006
128.00	-.1811	-.0001	.0140	.0006
130.00	-.1811	-.0001	.0140	.0006
132.00	-.1811	-.0001	.0140	.0006
134.00	-.1811	-.0001	.0140	.0006
136.00	-.1811	-.0001	.0140	.0006
138.00	-.1811	-.0001	.0140	.0006
140.00	-.1811	-.0001	.0140	.0006
142.00	-.1811	-.0001	.0140	.0006
144.00	-.1811	-.0001	.0140	.0006
146.00	-.1811	-.0001	.0140	.0006
148.00	-.1811	-.0001	.0140	.0006
150.00	-.1811	-.0001	.0140	.0006
152.00	-.1811	-.0001	.0140	.0006
154.00	-.1811	-.0001	.0140	.0006
156.00	-.1811	-.0001	.0140	.0006
158.00	-.1811	-.0001	.0140	.0006
160.00	-.1811	-.0001	.0140	.0006

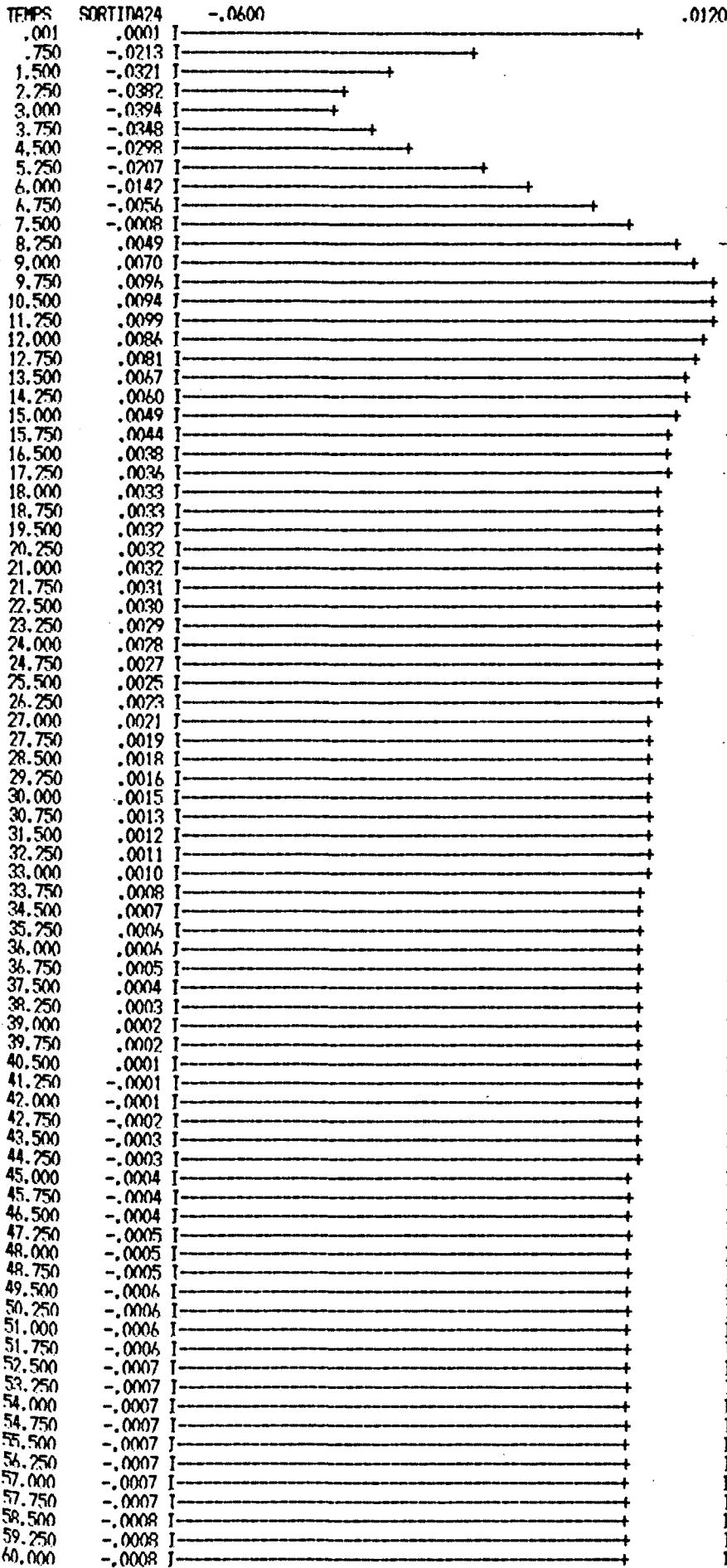
S5.1

S5:

Igual que S3 cuando no se fuerza la generación del Area 2.

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S6.1



S6:

Sobrepenalización de las desviaciones de f_1 .

$Q = \text{diag}(0,5;0,5;0,5;1;0,5;0,5;0,5)$

$R = I$

$\alpha_0 = 0$

TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0336	.0014	.0002
4.00	-.0476	-.0359	.0043	.0003
6.00	-.0635	-.0127	.0054	.0005
8.00	-.0805	.0029	.0055	.0006
10.00	-.0943	.0090	.0056	.0007
12.00	-.1065	.0090	.0058	.0008
14.00	-.1184	.0059	.0059	.0009
16.00	-.1297	.0040	.0060	.0010
18.00	-.1403	.0032	.0060	.0010
20.00	-.1500	.0030	.0060	.0011
22.00	-.1587	.0030	.0060	.0011
24.00	-.1667	.0027	.0061	.0012
26.00	-.1739	.0022	.0061	.0012
28.00	-.1804	.0018	.0061	.0012
30.00	-.1864	.0014	.0061	.0012
32.00	-.1918	.0010	.0061	.0013
34.00	-.1967	.0007	.0061	.0013
36.00	-.2012	.0005	.0061	.0013
38.00	-.2052	.0003	.0061	.0013
40.00	-.2088	.0001	.0061	.0013
42.00	-.2121	-.0002	.0061	.0013
44.00	-.2150	-.0003	.0061	.0013
46.00	-.2177	-.0005	.0061	.0013
48.00	-.2201	-.0005	.0061	.0013
50.00	-.2223	-.0006	.0061	.0013
52.00	-.2242	-.0007	.0061	.0013
54.00	-.2260	-.0007	.0061	.0013
56.00	-.2276	-.0008	.0061	.0013
58.00	-.2290	-.0008	.0061	.0013
60.00	-.2303	-.0008	.0061	.0013
62.00	-.2315	-.0008	.0061	.0013
64.00	-.2326	-.0008	.0061	.0013
66.00	-.2335	-.0008	.0061	.0013
68.00	-.2344	-.0008	.0061	.0013
70.00	-.2351	-.0007	.0061	.0013
72.00	-.2358	-.0007	.0061	.0013
74.00	-.2365	-.0007	.0061	.0013
76.00	-.2370	-.0007	.0061	.0013
78.00	-.2375	-.0007	.0061	.0013
80.00	-.2380	-.0006	.0061	.0013
82.00	-.2384	-.0006	.0061	.0013
84.00	-.2388	-.0006	.0061	.0013
86.00	-.2391	-.0006	.0061	.0013
88.00	-.2394	-.0005	.0061	.0013
90.00	-.2397	-.0005	.0061	.0013
92.00	-.2399	-.0005	.0061	.0013
94.00	-.2401	-.0005	.0061	.0013
96.00	-.2403	-.0004	.0061	.0013
98.00	-.2405	-.0004	.0061	.0013
100.00	-.2406	-.0004	.0061	.0013
102.00	-.2408	-.0004	.0061	.0013
104.00	-.2409	-.0004	.0061	.0013
106.00	-.2410	-.0003	.0061	.0013
108.00	-.2411	-.0003	.0061	.0013
110.00	-.2412	-.0003	.0061	.0013
112.00	-.2413	-.0003	.0061	.0013
114.00	-.2414	-.0003	.0061	.0013
116.00	-.2414	-.0003	.0061	.0013
118.00	-.2415	-.0002	.0061	.0013
120.00	-.2416	-.0002	.0061	.0013
122.00	-.2416	-.0002	.0061	.0013
124.00	-.2416	-.0002	.0061	.0013
126.00	-.2417	-.0002	.0061	.0013
128.00	-.2417	-.0002	.0061	.0013
130.00	-.2418	-.0002	.0061	.0013
132.00	-.2418	-.0002	.0061	.0013
134.00	-.2418	-.0002	.0061	.0013
136.00	-.2418	-.0002	.0061	.0013
138.00	-.2418	-.0001	.0061	.0013
140.00	-.2419	-.0001	.0061	.0013
142.00	-.2419	-.0001	.0061	.0013
144.00	-.2419	-.0001	.0061	.0013
146.00	-.2419	-.0001	.0061	.0013
148.00	-.2419	-.0001	.0061	.0013
150.00	-.2419	-.0001	.0061	.0013
152.00	-.2419	-.0001	.0061	.0013
154.00	-.2419	-.0001	.0061	.0013
156.00	-.2420	-.0001	.0061	.0013
158.00	-.2420	-.0001	.0061	.0013
160.00	-.2420	-.0001	.0061	.0013

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S7.1

TEMPS	SORTIDA24	-.0600	.0120
.001	.0001		
.750	-.0213		
1.500	-.0321		
2.250	-.0382		
3.000	-.0394		
3.750	-.0348		
4.500	-.0298		
5.250	-.0207		
6.000	-.0142		
6.750	-.0056		
7.500	-.0008		
8.250	.0049		
9.000	.0070		
9.750	.0095		
10.500	.0094		
11.250	.0099		
12.000	.0086		
12.750	.0081		
13.500	.0067		
14.250	.0060		
15.000	.0049		
15.750	.0044		
16.500	.0038		
17.250	.0036		
18.000	.0033		
18.750	.0033		
19.500	.0032		
20.250	.0032		
21.000	.0032		
21.750	.0031		
22.500	.0030		
23.250	.0029		
24.000	.0028		
24.750	.0027		
25.500	.0025		
26.250	.0023		
27.000	.0021		
27.750	.0020		
28.500	.0018		
29.250	.0016		
30.000	.0015		
30.750	.0013		
31.500	.0012		
32.250	.0011		
33.000	.0010		
33.750	.0008		
34.500	.0007		
35.250	.0006		
36.000	.0006		
36.750	.0005		
37.500	.0004		
38.250	.0003		
39.000	.0002		
39.750	.0002		
40.500	.0001		
41.250	-.0001		
42.000	-.0001		
42.750	-.0002		
43.500	-.0003		
44.250	-.0003		
45.000	-.0004		
45.750	-.0004		
46.500	-.0004		
47.250	-.0005		
48.000	-.0005		
48.750	-.0005		
49.500	-.0006		
50.250	-.0006		
51.000	-.0006		
51.750	-.0006		
52.500	-.0007		
53.250	-.0007		
54.000	-.0007		
54.750	-.0007		
55.500	-.0007		
56.250	-.0007		
57.000	-.0007		
57.750	-.0007		
58.500	-.0008		
59.250	-.0008		
60.000	-.0008		

S7:

Sobrepenalización de las desviaciones de f_2 .

$$\tilde{Q} = \text{diag}(0,5;0,5;0,5;0,5;0,5;0,5;1)$$

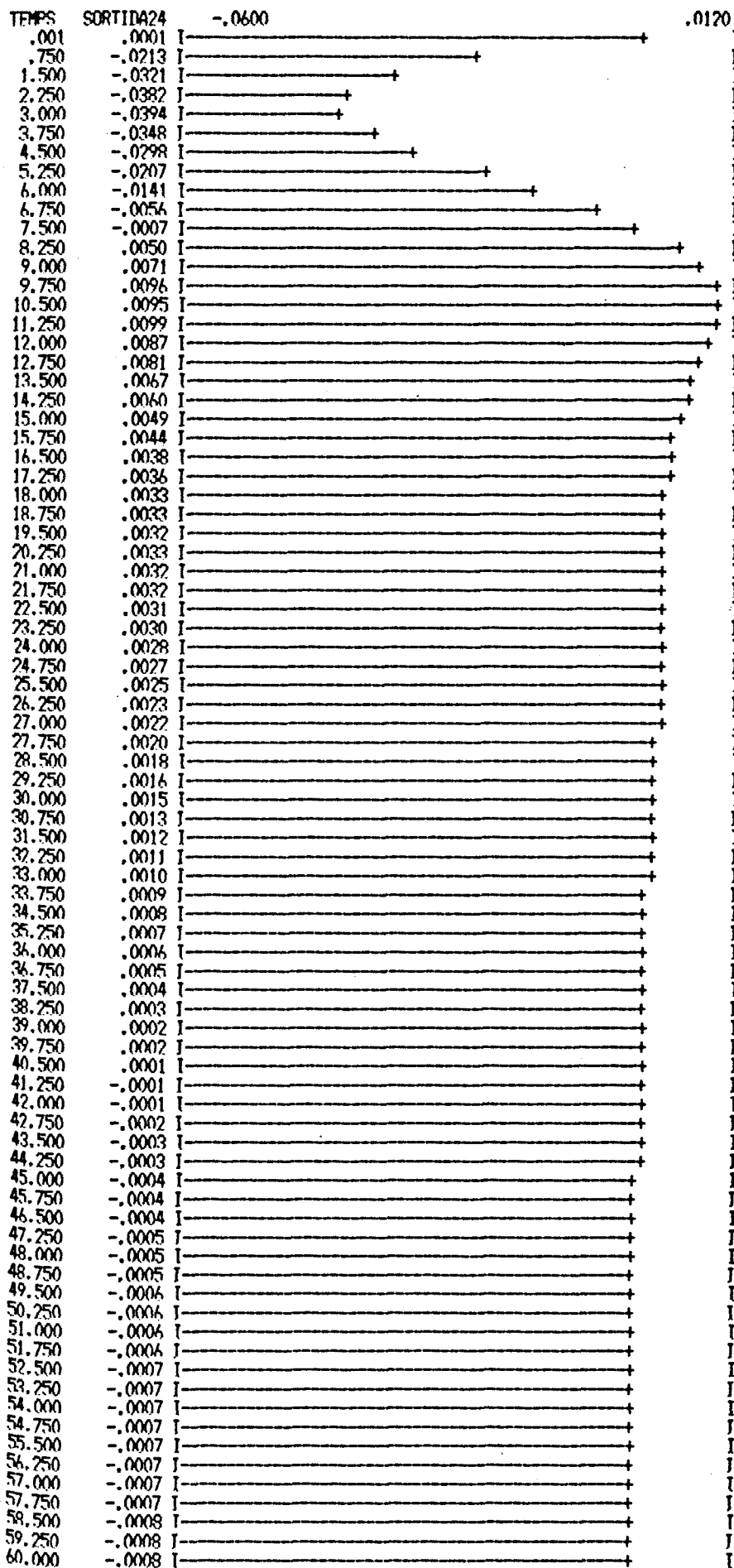
$$\tilde{R} = I$$

$$\tilde{\alpha}_0 = 0$$

TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0336	.0014	.0002
4.00	-.0426	-.0359	.0043	.0003
6.00	-.0635	-.0178	.0054	.0005
8.00	-.0805	.0029	.0055	.0006
10.00	-.0943	.0090	.0056	.0007
12.00	-.1066	.0090	.0058	.0008
14.00	-.1184	.0059	.0059	.0009
16.00	-.1298	.0040	.0060	.0010
18.00	-.1404	.0032	.0060	.0010
20.00	-.1501	.0030	.0060	.0011
22.00	-.1589	.0030	.0061	.0011
24.00	-.1668	.0027	.0061	.0012
26.00	-.1740	.0022	.0061	.0012
28.00	-.1806	.0018	.0061	.0012
30.00	-.1866	.0014	.0061	.0012
32.00	-.1920	.0010	.0061	.0013
34.00	-.1969	.0007	.0061	.0013
36.00	-.2013	.0005	.0061	.0013
38.00	-.2053	.0003	.0061	.0013
40.00	-.2090	.0001	.0061	.0013
42.00	-.2122	-.0002	.0061	.0013
44.00	-.2152	-.0003	.0061	.0013
46.00	-.2179	-.0005	.0061	.0013
48.00	-.2203	-.0005	.0061	.0013
50.00	-.2225	-.0006	.0061	.0013
52.00	-.2244	-.0007	.0061	.0013
54.00	-.2262	-.0007	.0061	.0013
56.00	-.2278	-.0008	.0061	.0013
58.00	-.2292	-.0008	.0061	.0013
60.00	-.2305	-.0008	.0061	.0013
62.00	-.2317	-.0008	.0061	.0013
64.00	-.2327	-.0008	.0061	.0013
66.00	-.2337	-.0008	.0061	.0013
68.00	-.2345	-.0008	.0061	.0013
70.00	-.2353	-.0007	.0061	.0013
72.00	-.2360	-.0007	.0061	.0013
74.00	-.2366	-.0007	.0061	.0013
76.00	-.2372	-.0007	.0061	.0013
78.00	-.2377	-.0007	.0061	.0013
80.00	-.2382	-.0006	.0061	.0013
82.00	-.2386	-.0006	.0061	.0013
84.00	-.2389	-.0006	.0061	.0013
86.00	-.2393	-.0006	.0061	.0013
88.00	-.2396	-.0005	.0061	.0013
90.00	-.2398	-.0005	.0061	.0013
92.00	-.2401	-.0005	.0061	.0013
94.00	-.2403	-.0005	.0061	.0013
96.00	-.2405	-.0004	.0061	.0013
98.00	-.2407	-.0004	.0061	.0013
100.00	-.2408	-.0004	.0061	.0013
102.00	-.2410	-.0004	.0061	.0013
104.00	-.2411	-.0004	.0061	.0013
106.00	-.2412	-.0003	.0061	.0013
108.00	-.2413	-.0003	.0061	.0013
110.00	-.2414	-.0003	.0061	.0013
112.00	-.2415	-.0003	.0061	.0013
114.00	-.2416	-.0003	.0061	.0013
116.00	-.2416	-.0003	.0061	.0013
118.00	-.2417	-.0002	.0061	.0013
120.00	-.2417	-.0002	.0061	.0013
122.00	-.2418	-.0002	.0061	.0013
124.00	-.2418	-.0002	.0061	.0013
126.00	-.2419	-.0002	.0061	.0013
128.00	-.2419	-.0002	.0061	.0013
130.00	-.2419	-.0002	.0061	.0013
132.00	-.2420	-.0002	.0061	.0013
134.00	-.2420	-.0002	.0061	.0013
136.00	-.2420	-.0002	.0061	.0013
138.00	-.2420	-.0001	.0061	.0013
140.00	-.2421	-.0001	.0061	.0013
142.00	-.2421	-.0001	.0061	.0013
144.00	-.2421	-.0001	.0061	.0013
146.00	-.2421	-.0001	.0061	.0013
148.00	-.2421	-.0001	.0061	.0013
150.00	-.2421	-.0001	.0061	.0013
152.00	-.2421	-.0001	.0061	.0013
154.00	-.2421	-.0001	.0061	.0013
156.00	-.2421	-.0001	.0061	.0013
158.00	-.2421	-.0001	.0061	.0013
160.00	-.2422	-.0001	.0061	.0013

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S8.1



S8:

Sobrepénalización del intercambio de potencia (P_{12}),

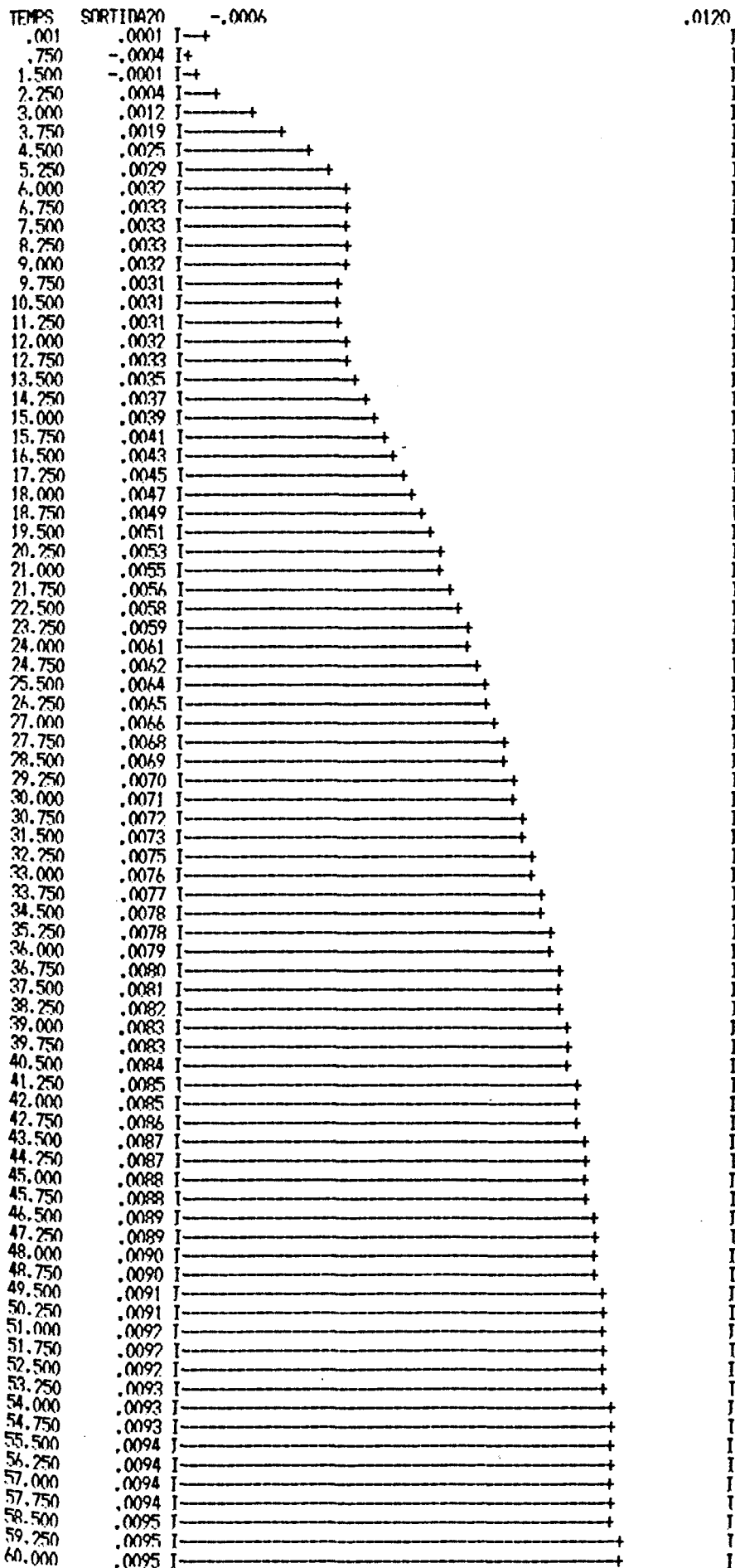
$$Q = \text{diag}(0,5;0,5;0,5;0,5;0,5;1;0,5)$$

$$R = I$$

$$\alpha_0 = 0$$

BLOC FIX Y (20) MINIM (-.0006) MAXIM (.0120)

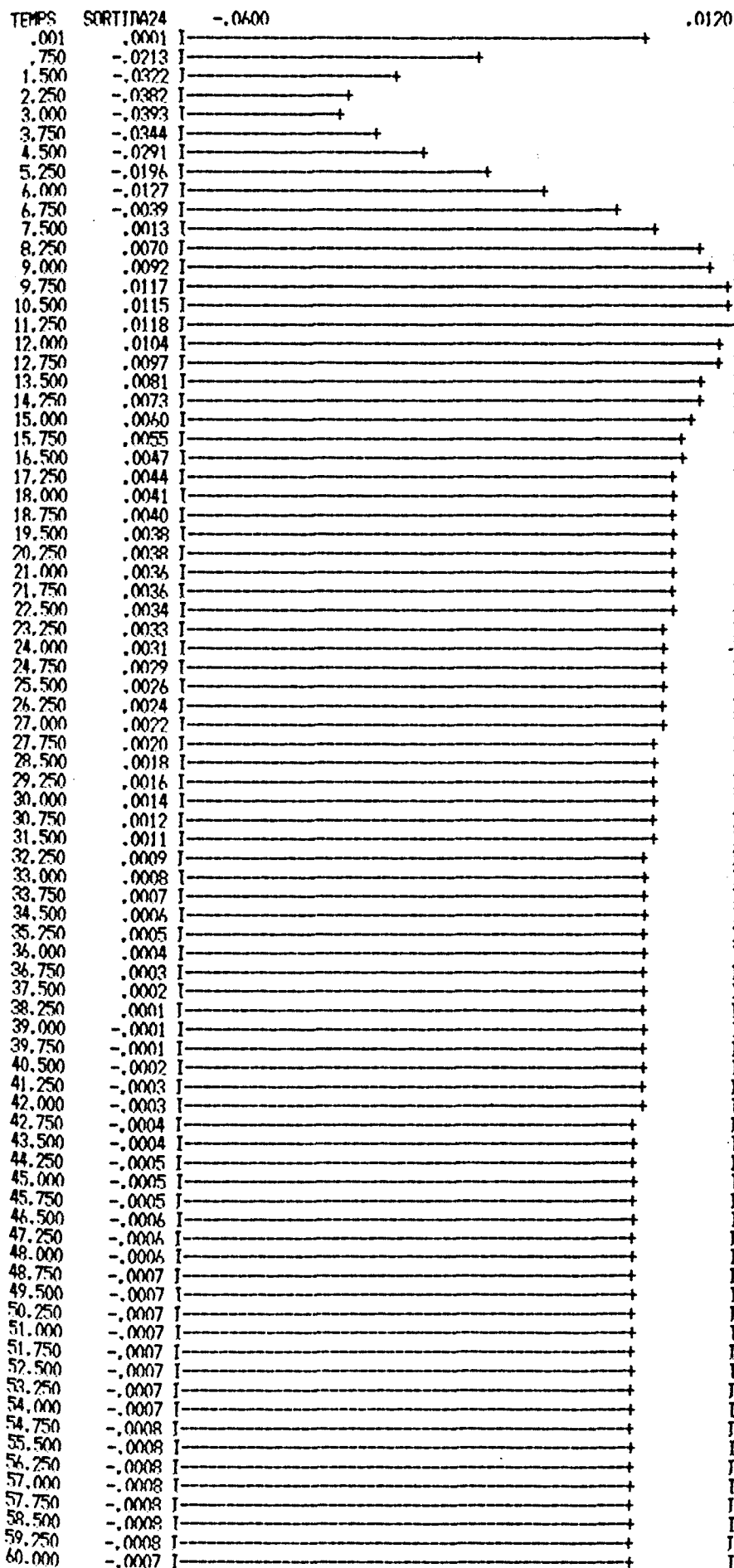
SS.2



TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0336	.0014	.0002
4.00	-.0426	-.0359	.0043	.0003
6.00	-.0635	-.0127	.0054	.0005
8.00	-.0805	.0030	.0055	.0006
10.00	-.0942	.0091	.0056	.0007
12.00	-.1064	.0090	.0058	.0008
14.00	-.1182	.0059	.0059	.0009
16.00	-.1294	.0040	.0060	.0010
18.00	-.1399	.0033	.0060	.0010
20.00	-.1496	.0031	.0060	.0011
22.00	-.1582	.0030	.0061	.0011
24.00	-.1661	.0027	.0061	.0012
26.00	-.1732	.0023	.0061	.0012
28.00	-.1797	.0018	.0061	.0012
30.00	-.1855	.0014	.0061	.0012
32.00	-.1908	.0010	.0061	.0012
34.00	-.1956	.0007	.0061	.0013
36.00	-.1999	.0005	.0061	.0013
38.00	-.2038	.0003	.0061	.0013
40.00	-.2074	.0001	.0061	.0013
42.00	-.2105	-.0002	.0061	.0013
44.00	-.2134	-.0003	.0061	.0013
46.00	-.2160	-.0005	.0061	.0013
48.00	-.2183	-.0005	.0061	.0013
50.00	-.2204	-.0006	.0061	.0013
52.00	-.2222	-.0007	.0061	.0013
54.00	-.2239	-.0007	.0061	.0013
56.00	-.2254	-.0008	.0061	.0013
58.00	-.2268	-.0008	.0061	.0013
60.00	-.2280	-.0008	.0061	.0013
62.00	-.2291	-.0008	.0061	.0013
64.00	-.2301	-.0008	.0061	.0013
66.00	-.2310	-.0008	.0061	.0013
68.00	-.2318	-.0008	.0061	.0013
70.00	-.2325	-.0007	.0061	.0013
72.00	-.2332	-.0007	.0061	.0013
74.00	-.2338	-.0007	.0061	.0013
76.00	-.2343	-.0007	.0061	.0013
78.00	-.2347	-.0007	.0061	.0013
80.00	-.2352	-.0006	.0061	.0013

S8.3

BLOC ETX Y (24) MINIM (-.0400) MAXIM (.0120)

S9.1S9:

Sobrepenalización del ACE

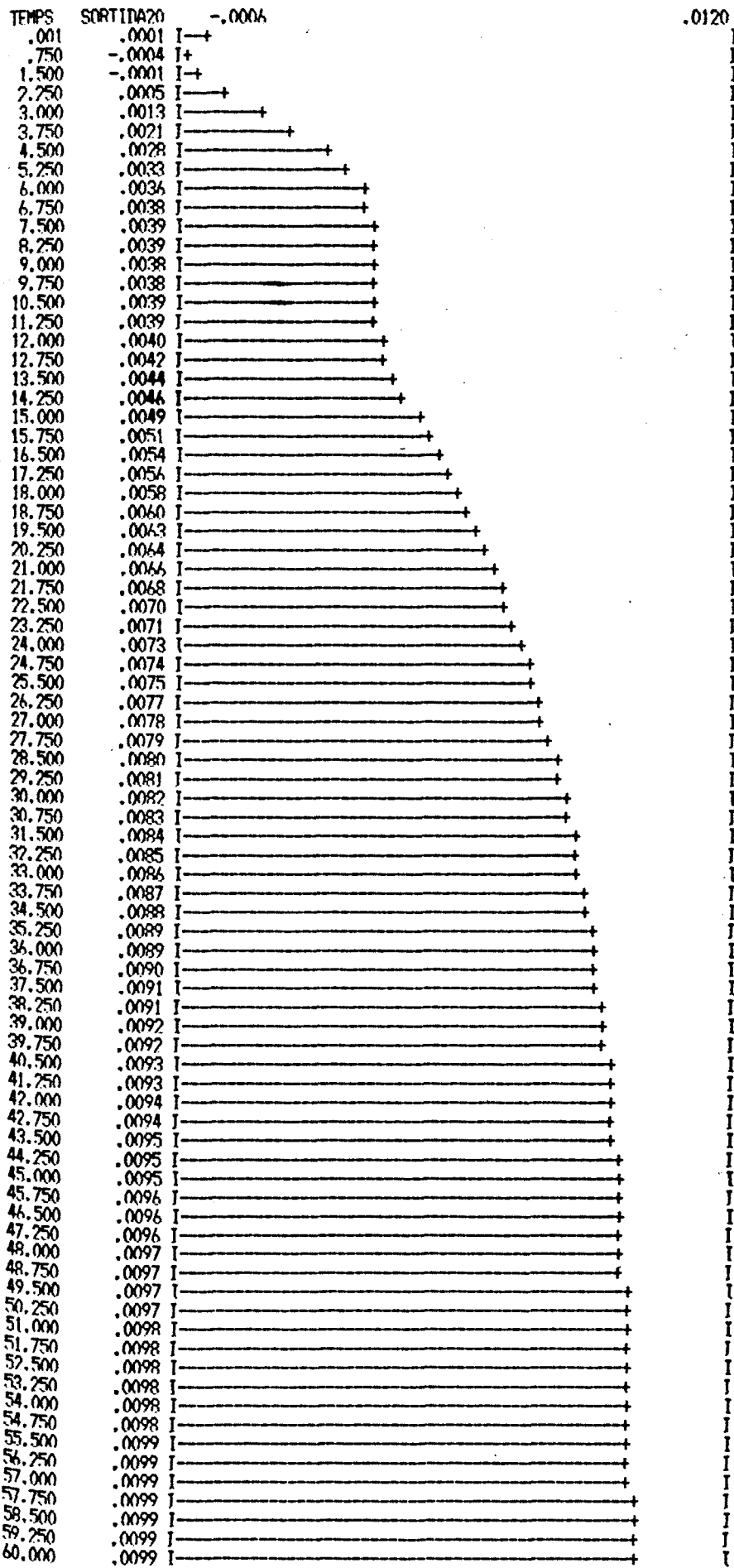
$$\tilde{Q} = \text{diag}(0,5;0,5;0,5;0,5;1;0,5;0,5)$$

$$\tilde{R} = I$$

$$\tilde{\alpha}_0 = 0$$

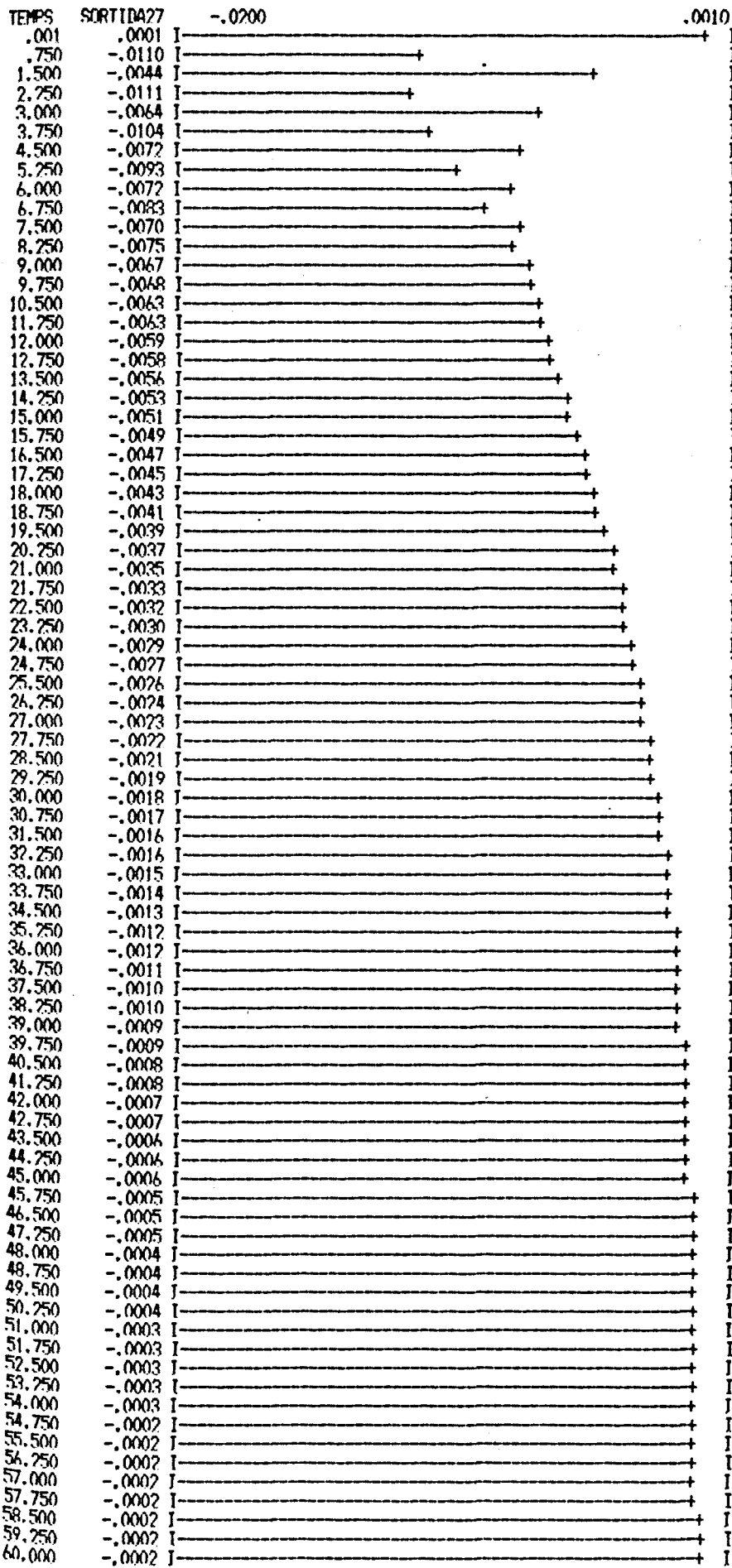
BLOC ETX V (20) MINIM (-.0006) MAXIM (.0120)

S9.2



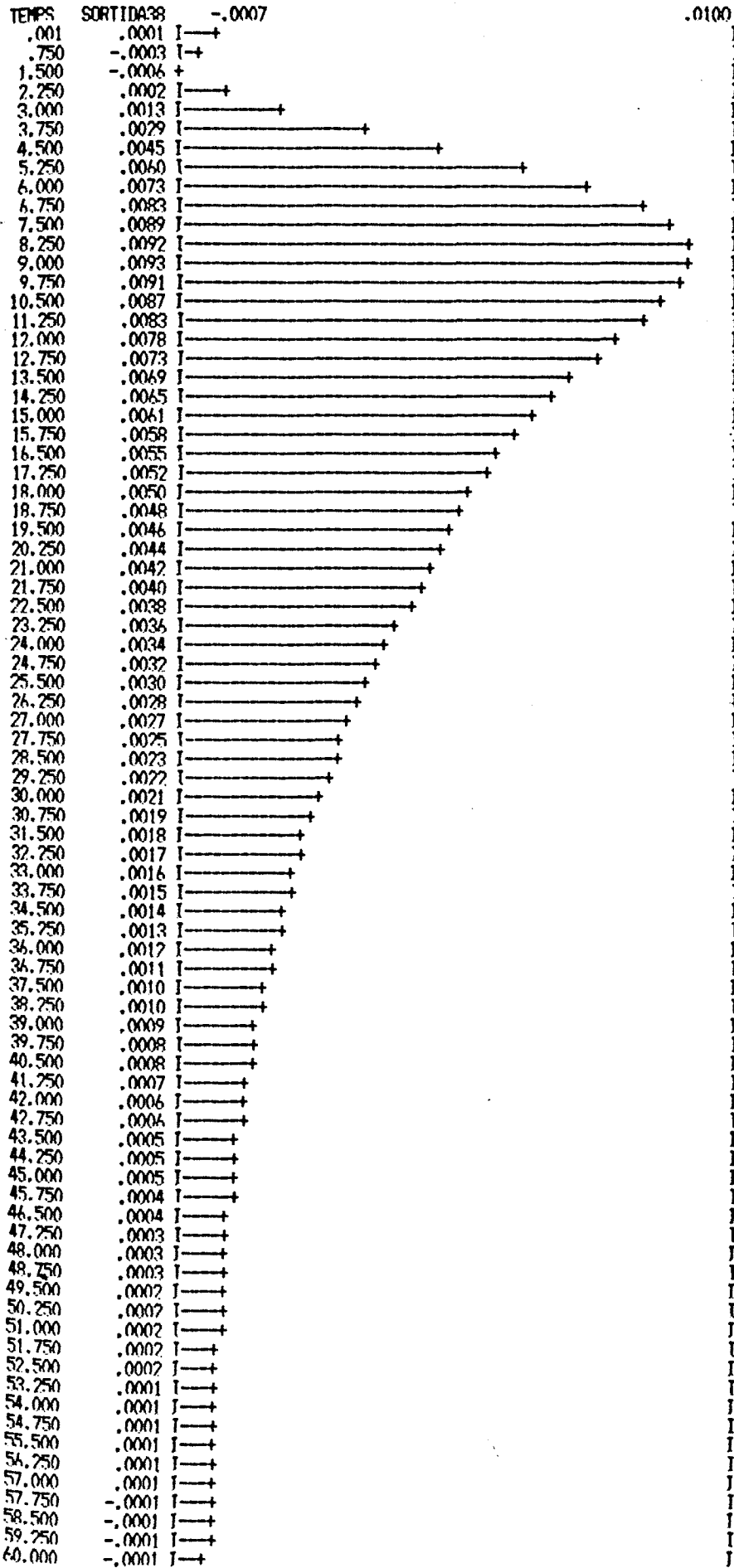
RLOC EIX Y (27) MINIM (-.0200) MAXIM (.0010)

S9.3



PLC FIX Y (38) MINIM (-.0007) MAXIM (.0100)

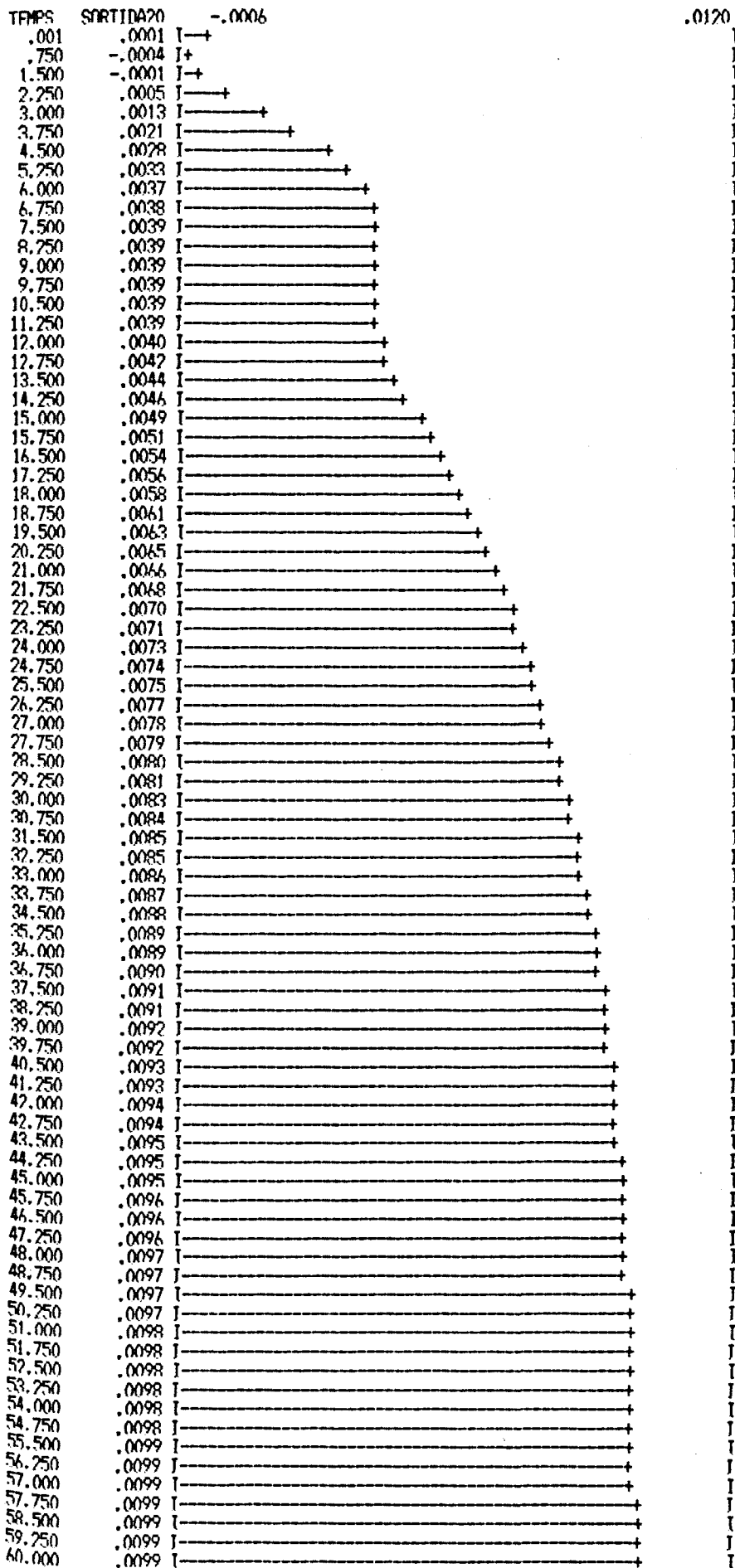
S9.4



TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0174	-.0337	.0014	.0002
4.00	-.0425	-.0355	.0042	.0003
6.00	-.0627	-.0114	.0053	.0005
8.00	-.0785	.0049	.0054	.0006
10.00	-.0906	.0111	.0056	.0007
12.00	-.1008	.0107	.0058	.0007
14.00	-.1105	.0072	.0060	.0008
16.00	-.1196	.0050	.0061	.0009
18.00	-.1278	.0040	.0061	.0009
20.00	-.1350	.0036	.0062	.0009
22.00	-.1413	.0034	.0062	.0010
24.00	-.1467	.0029	.0062	.0010
26.00	-.1514	.0024	.0062	.0010
28.00	-.1555	.0018	.0062	.0010
30.00	-.1591	.0013	.0062	.0010
32.00	-.1622	.0009	.0062	.0010
34.00	-.1649	.0006	.0062	.0010
36.00	-.1672	.0003	.0062	.0010
38.00	-.1692	.0001	.0062	.0010
40.00	-.1710	-.0002	.0062	.0010
42.00	-.1724	-.0004	.0062	.0010
44.00	-.1737	-.0005	.0062	.0010
46.00	-.1748	-.0006	.0062	.0010
48.00	-.1758	-.0007	.0062	.0010
50.00	-.1766	-.0007	.0062	.0010
52.00	-.1773	-.0007	.0062	.0010
54.00	-.1778	-.0008	.0062	.0010
56.00	-.1783	-.0008	.0062	.0010
58.00	-.1788	-.0008	.0062	.0010
60.00	-.1791	-.0008	.0062	.0010
62.00	-.1795	-.0007	.0062	.0010
64.00	-.1797	-.0007	.0062	.0010
66.00	-.1800	-.0007	.0062	.0010
68.00	-.1801	-.0007	.0063	.0010
70.00	-.1803	-.0006	.0063	.0010
72.00	-.1804	-.0006	.0063	.0010
74.00	-.1806	-.0006	.0063	.0010
76.00	-.1807	-.0006	.0063	.0010
78.00	-.1807	-.0005	.0063	.0010
80.00	-.1808	-.0005	.0063	.0010
82.00	-.1809	-.0005	.0063	.0010
84.00	-.1809	-.0004	.0063	.0010
86.00	-.1810	-.0004	.0063	.0010
88.00	-.1810	-.0004	.0063	.0010
90.00	-.1810	-.0004	.0063	.0010
92.00	-.1811	-.0003	.0063	.0010
94.00	-.1811	-.0003	.0063	.0010
96.00	-.1811	-.0003	.0063	.0010
98.00	-.1811	-.0003	.0063	.0010
100.00	-.1811	-.0003	.0063	.0010
102.00	-.1811	-.0003	.0063	.0010
104.00	-.1811	-.0002	.0063	.0010
106.00	-.1811	-.0002	.0063	.0010
108.00	-.1811	-.0002	.0063	.0010
110.00	-.1811	-.0002	.0063	.0010
112.00	-.1811	-.0002	.0063	.0010
114.00	-.1812	-.0002	.0063	.0010
116.00	-.1812	-.0002	.0063	.0010
118.00	-.1812	-.0002	.0063	.0010
120.00	-.1812	-.0001	.0063	.0010
122.00	-.1812	-.0001	.0063	.0010
124.00	-.1812	-.0001	.0063	.0010
126.00	-.1812	-.0001	.0063	.0010
128.00	-.1812	-.0001	.0063	.0010
130.00	-.1812	-.0001	.0063	.0010
132.00	-.1812	-.0001	.0063	.0010
134.00	-.1812	-.0001	.0063	.0010
136.00	-.1812	-.0001	.0063	.0010
138.00	-.1812	-.0001	.0063	.0010
140.00	-.1812	-.0001	.0063	.0010
142.00	-.1812	-.0001	.0063	.0010
144.00	-.1812	-.0001	.0063	.0010
146.00	-.1812	-.0001	.0063	.0010
148.00	-.1812	-.0001	.0063	.0010
150.00	-.1812	-.0001	.0063	.0010
152.00	-.1812	-.0001	.0063	.0010
154.00	-.1812	-.0001	.0063	.0010
156.00	-.1812	-.0001	.0063	.0010
158.00	-.1812	-.0001	.0063	.0010
160.00	-.1812	-.0001	.0063	.0010

BLOC FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S10.1



S10:

Sobrepenalización del ACE y subpenalización de los esfuerzos del lazo de realimentación transitoria de las unidades generadoras.

$$\tilde{Q} = \text{diag}(0,5;0,1;0,5;0,5;1;0,5;0,5)$$

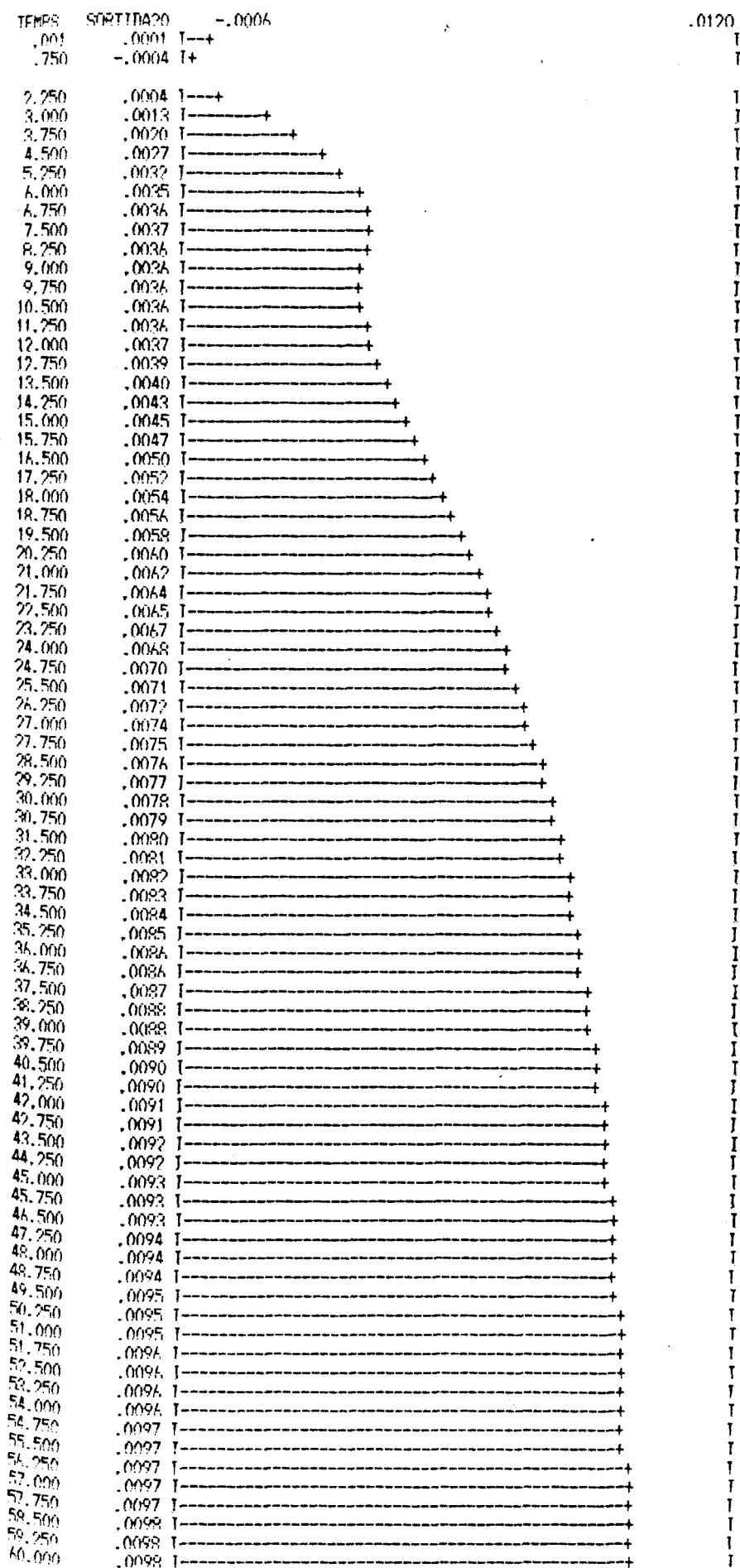
$$R = I$$

$$\alpha_0 = 0$$

TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA54
.00	.0001	.0001	.0001	.0001
2.00	-.0176	-.0337	.0014	.0002
4.00	-.0424	-.0355	.0042	.0003
6.00	-.0627	-.0113	.0053	.0005
8.00	-.0784	.0050	.0054	.0006
10.00	-.0904	.0111	.0056	.0007
12.00	-.1006	.0106	.0058	.0007
14.00	-.1103	.0072	.0060	.0008
16.00	-.1194	.0049	.0061	.0009
18.00	-.1275	.0040	.0061	.0009
20.00	-.1347	.0036	.0061	.0009
22.00	-.1410	.0034	.0062	.0010
24.00	-.1444	.0029	.0062	.0010
26.00	-.1510	.0024	.0062	.0010
28.00	-.1551	.0018	.0062	.0010
30.00	-.1587	.0013	.0062	.0010
32.00	-.1618	.0009	.0062	.0010
34.00	-.1644	.0006	.0062	.0010
36.00	-.1668	.0003	.0062	.0010
38.00	-.1687	.0001	.0062	.0010
40.00	-.1705	-.0002	.0062	.0010
42.00	-.1719	-.0004	.0062	.0010
44.00	-.1732	-.0005	.0062	.0010
46.00	-.1743	-.0006	.0062	.0010
48.00	-.1752	-.0007	.0062	.0010
50.00	-.1760	-.0007	.0062	.0010
52.00	-.1767	-.0007	.0062	.0010
54.00	-.1773	-.0008	.0062	.0010
56.00	-.1778	-.0008	.0062	.0010
58.00	-.1782	-.0008	.0062	.0010
60.00	-.1786	-.0008	.0062	.0010
62.00	-.1789	-.0007	.0062	.0010
64.00	-.1791	-.0007	.0062	.0010
66.00	-.1794	-.0007	.0062	.0010
68.00	-.1796	-.0007	.0062	.0010
70.00	-.1797	-.0006	.0062	.0010
72.00	-.1799	-.0006	.0062	.0010
74.00	-.1800	-.0006	.0062	.0010
76.00	-.1801	-.0006	.0062	.0010
78.00	-.1801	-.0005	.0062	.0010
80.00	-.1802	-.0005	.0062	.0010
82.00	-.1803	-.0005	.0062	.0010
84.00	-.1803	-.0004	.0062	.0010
86.00	-.1804	-.0004	.0062	.0010
88.00	-.1804	-.0004	.0062	.0010
90.00	-.1804	-.0004	.0062	.0010
92.00	-.1805	-.0003	.0062	.0010
94.00	-.1805	-.0003	.0062	.0010
96.00	-.1805	-.0003	.0062	.0010
98.00	-.1805	-.0003	.0062	.0010
100.00	-.1805	-.0003	.0062	.0010
102.00	-.1805	-.0003	.0062	.0010
104.00	-.1805	-.0002	.0062	.0010
106.00	-.1805	-.0002	.0062	.0010
108.00	-.1805	-.0002	.0062	.0010
110.00	-.1806	-.0002	.0062	.0010
112.00	-.1806	-.0002	.0062	.0010
114.00	-.1806	-.0002	.0062	.0010
116.00	-.1806	-.0002	.0062	.0010
118.00	-.1806	-.0002	.0062	.0010
120.00	-.1806	-.0001	.0062	.0010
122.00	-.1806	-.0001	.0062	.0010
124.00	-.1806	-.0001	.0062	.0010
126.00	-.1806	-.0001	.0062	.0010
128.00	-.1806	-.0001	.0062	.0010
130.00	-.1806	-.0001	.0062	.0010
132.00	-.1806	-.0001	.0062	.0010
134.00	-.1806	-.0001	.0062	.0010
136.00	-.1806	-.0001	.0062	.0010
138.00	-.1806	-.0001	.0062	.0010
140.00	-.1806	-.0001	.0062	.0010
142.00	-.1806	-.0001	.0062	.0010
144.00	-.1806	-.0001	.0062	.0010
146.00	-.1806	-.0001	.0062	.0010
148.00	-.1806	-.0001	.0062	.0010
150.00	-.1806	-.0001	.0062	.0010
152.00	-.1806	-.0001	.0062	.0010
154.00	-.1806	-.0001	.0062	.0010
156.00	-.1806	-.0001	.0062	.0010
158.00	-.1806	-.0001	.0062	.0010
160.00	-.1806	-.0001	.0062	.0010

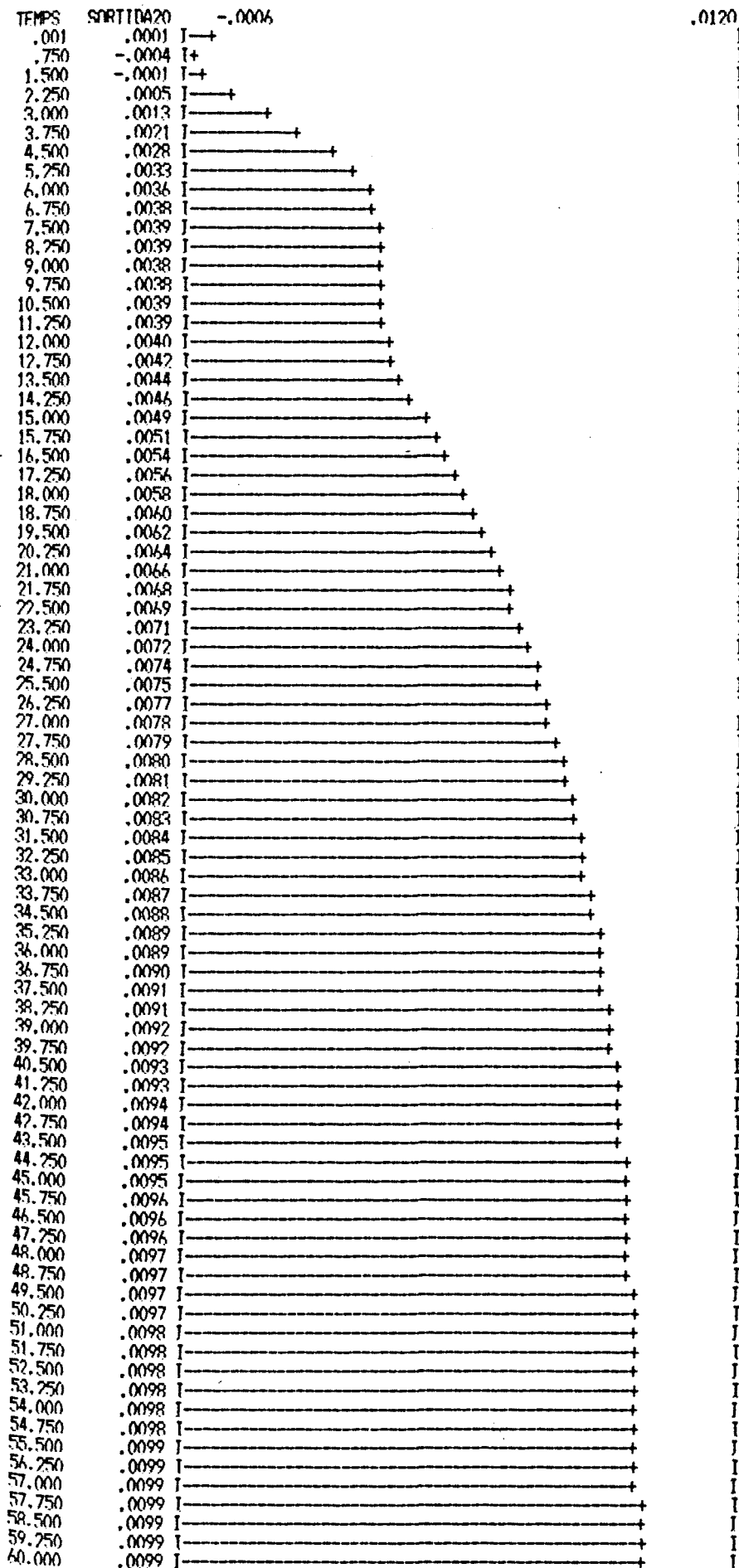
R(0) FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S11.2



BLOC FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S12.1



S12:

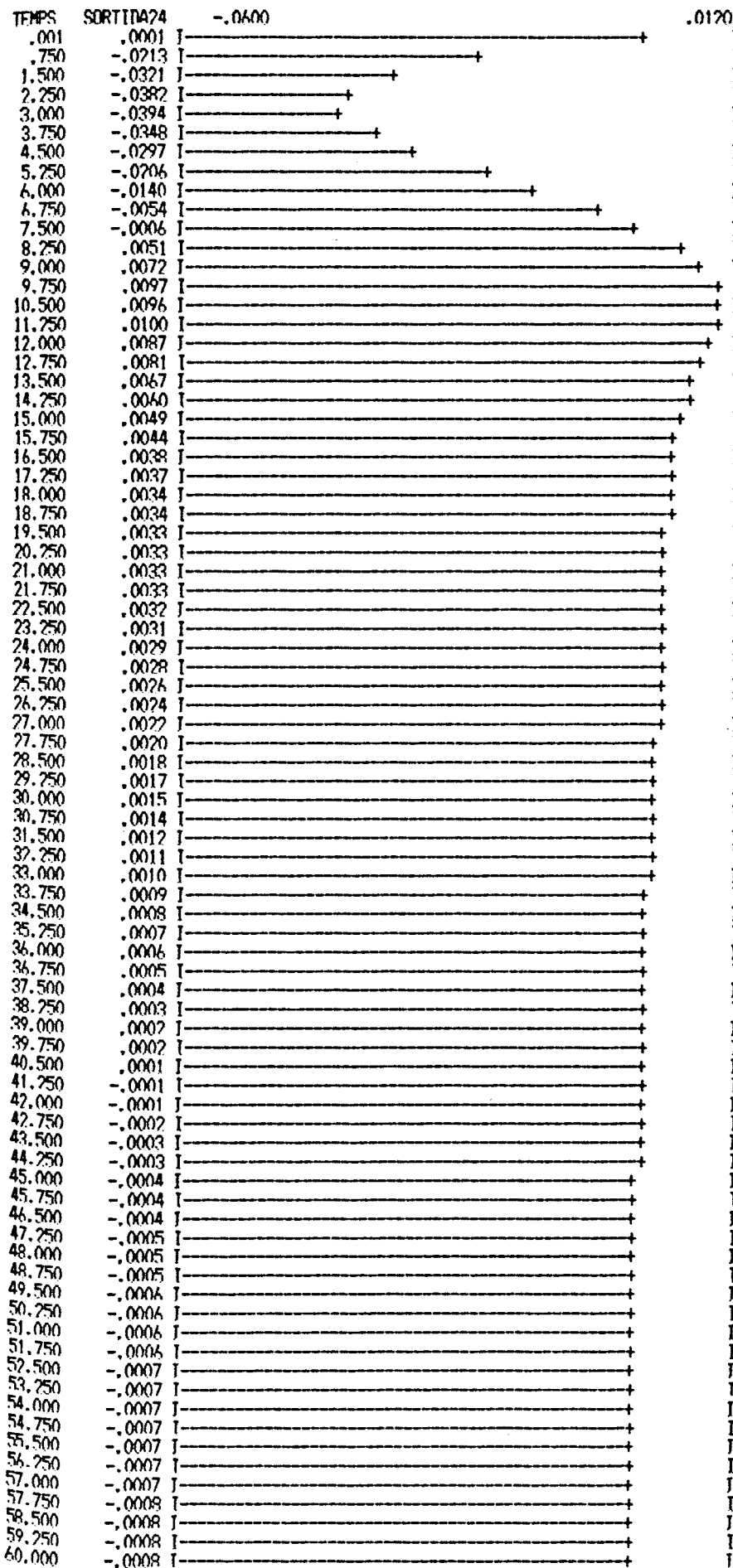
Sobrepenalización del ACE y de la potencia generada en el Area (P_{G1})

$$Q = \text{diag}(0,5;0,5;1;0,5;1;0,5;0,5)$$

$$R = I$$

$$\alpha_0 = 0$$

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)



S13:

Sobrepenalización del ACE y del esfuerzo de control (\tilde{R}).

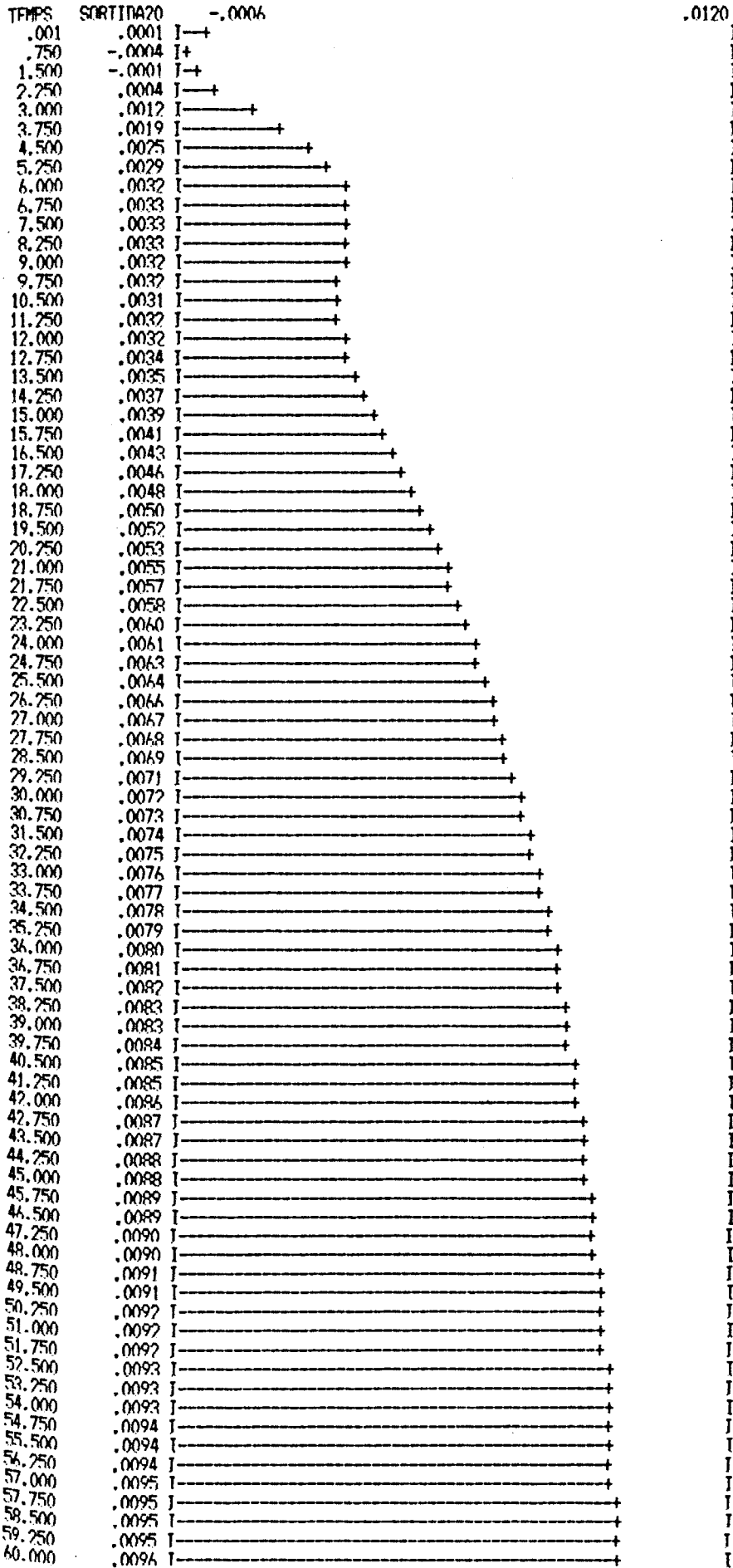
$$\tilde{Q} = \text{diag}(0,5;0,5;0,5;0,5;1;0,5;0,5)$$

$$\tilde{R} = 2I$$

$$\tilde{\rho} = 0$$

BLOC ETX Y (20) MINIM (-.0006) MAXIM (.0120)

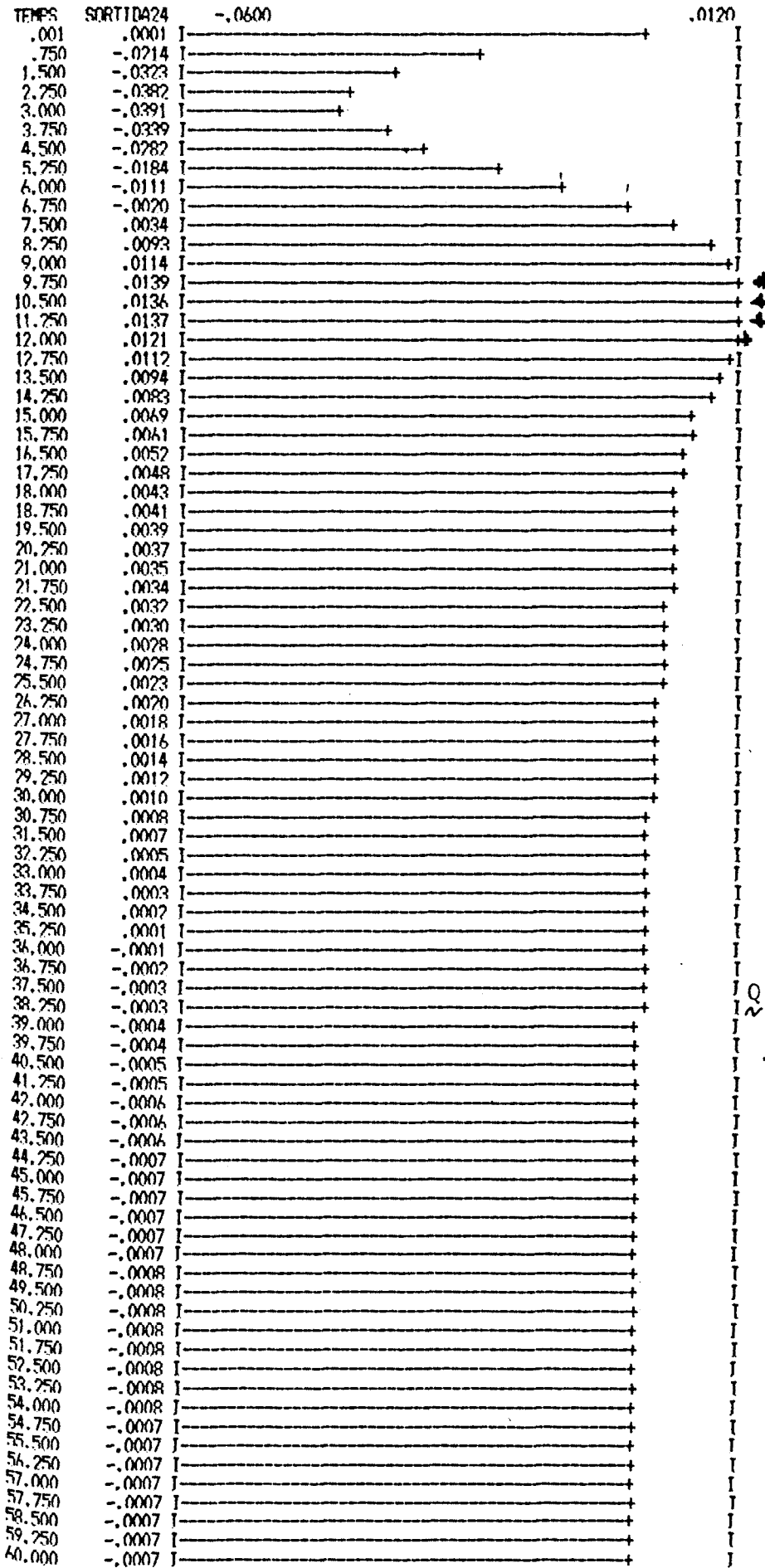
S13.2



TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA5A
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0336	.0014	.0002
4.00	-.0426	-.0359	.0043	.0003
6.00	-.0634	-.0126	.0054	.0005
8.00	-.0803	.0031	.0055	.0006
10.00	-.0940	.0092	.0054	.0007
12.00	-.1061	.0090	.0058	.0008
14.00	-.1178	.0059	.0059	.0009
16.00	-.1290	.0040	.0060	.0010
18.00	-.1394	.0033	.0060	.0010
20.00	-.1489	.0031	.0060	.0011
22.00	-.1575	.0031	.0061	.0011
24.00	-.1652	.0028	.0061	.0011
26.00	-.1722	.0023	.0061	.0012
28.00	-.1785	.0018	.0061	.0012
30.00	-.1842	.0014	.0061	.0012
32.00	-.1894	.0011	.0061	.0012
34.00	-.1940	.0008	.0061	.0012
36.00	-.1982	.0005	.0061	.0013
38.00	-.2019	.0003	.0061	.0013
40.00	-.2053	.0001	.0061	.0013
42.00	-.2083	-.0002	.0061	.0013
44.00	-.2111	-.0003	.0061	.0013
46.00	-.2135	-.0005	.0061	.0013
48.00	-.2157	-.0005	.0061	.0013
50.00	-.2177	-.0006	.0061	.0013
52.00	-.2194	-.0007	.0061	.0013
54.00	-.2210	-.0007	.0061	.0013
56.00	-.2224	-.0008	.0061	.0013
58.00	-.2237	-.0008	.0061	.0013
60.00	-.2248	-.0008	.0061	.0013
62.00	-.2258	-.0008	.0061	.0013
64.00	-.2267	-.0008	.0061	.0013
66.00	-.2275	-.0008	.0061	.0013
68.00	-.2283	-.0008	.0061	.0013
70.00	-.2289	-.0007	.0061	.0013
72.00	-.2295	-.0007	.0061	.0013
74.00	-.2300	-.0007	.0061	.0013
76.00	-.2305	-.0007	.0061	.0013
78.00	-.2309	-.0006	.0061	.0013
80.00	-.2313	-.0006	.0061	.0013
82.00	-.2316	-.0006	.0061	.0013
84.00	-.2319	-.0006	.0061	.0013
86.00	-.2322	-.0005	.0061	.0013
88.00	-.2324	-.0005	.0061	.0013
90.00	-.2326	-.0005	.0061	.0013
92.00	-.2328	-.0005	.0061	.0013
94.00	-.2330	-.0004	.0061	.0013
96.00	-.2331	-.0004	.0061	.0013
98.00	-.2333	-.0004	.0061	.0013
100.00	-.2334	-.0004	.0061	.0013
102.00	-.2335	-.0004	.0061	.0013
104.00	-.2336	-.0003	.0061	.0013
106.00	-.2337	-.0003	.0061	.0013
108.00	-.2338	-.0003	.0061	.0013
110.00	-.2338	-.0003	.0061	.0013
112.00	-.2339	-.0003	.0061	.0013
114.00	-.2340	-.0003	.0061	.0013
116.00	-.2340	-.0002	.0061	.0013
118.00	-.2341	-.0002	.0061	.0013
120.00	-.2341	-.0002	.0061	.0013
122.00	-.2341	-.0002	.0061	.0013
124.00	-.2342	-.0002	.0061	.0013
126.00	-.2342	-.0002	.0061	.0013
128.00	-.2342	-.0002	.0061	.0013
130.00	-.2342	-.0002	.0061	.0013
132.00	-.2343	-.0002	.0061	.0013
134.00	-.2343	-.0001	.0061	.0013
136.00	-.2343	-.0001	.0061	.0013
138.00	-.2343	-.0001	.0061	.0013
140.00	-.2343	-.0001	.0061	.0013
142.00	-.2343	-.0001	.0061	.0013
144.00	-.2343	-.0001	.0061	.0013
146.00	-.2343	-.0001	.0061	.0013
148.00	-.2344	-.0001	.0061	.0013
150.00	-.2344	-.0001	.0061	.0013
152.00	-.2344	-.0001	.0061	.0013
154.00	-.2344	-.0001	.0061	.0013
156.00	-.2344	-.0001	.0061	.0013
158.00	-.2344	-.0001	.0061	.0013
160.00	-.2344	-.0001	.0061	.0013

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S14.1



S14:

Sobrepenalización del ACE y aumento del esfuerzo de control (subpenalización de \tilde{R}).

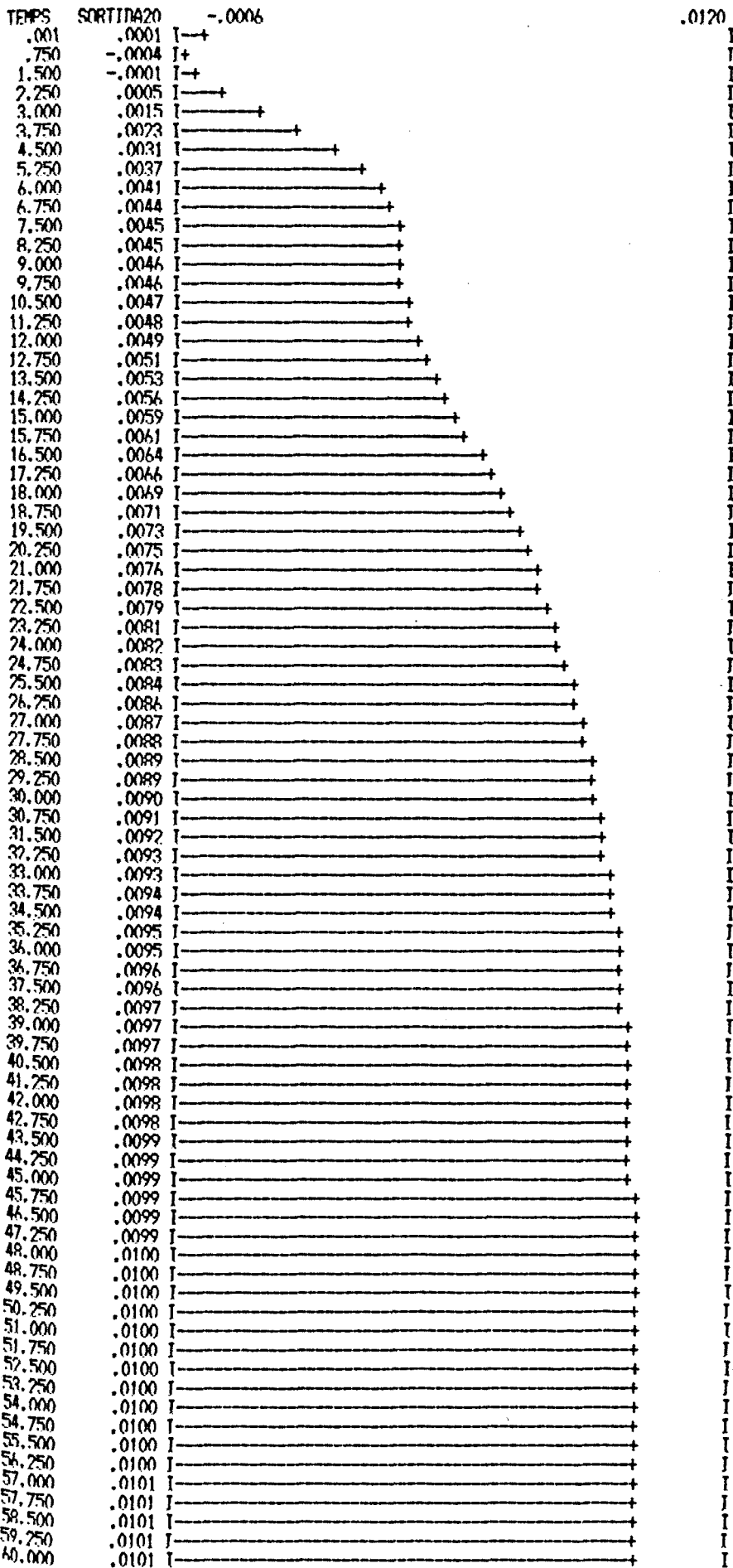
$$\tilde{Q} = \text{diag}(0,5,0,5;0,5;0,5;1;0,5;0,5)$$

$$\tilde{R} = 0,5 \tilde{I}$$

$$\tilde{\rho}_0 = 0$$

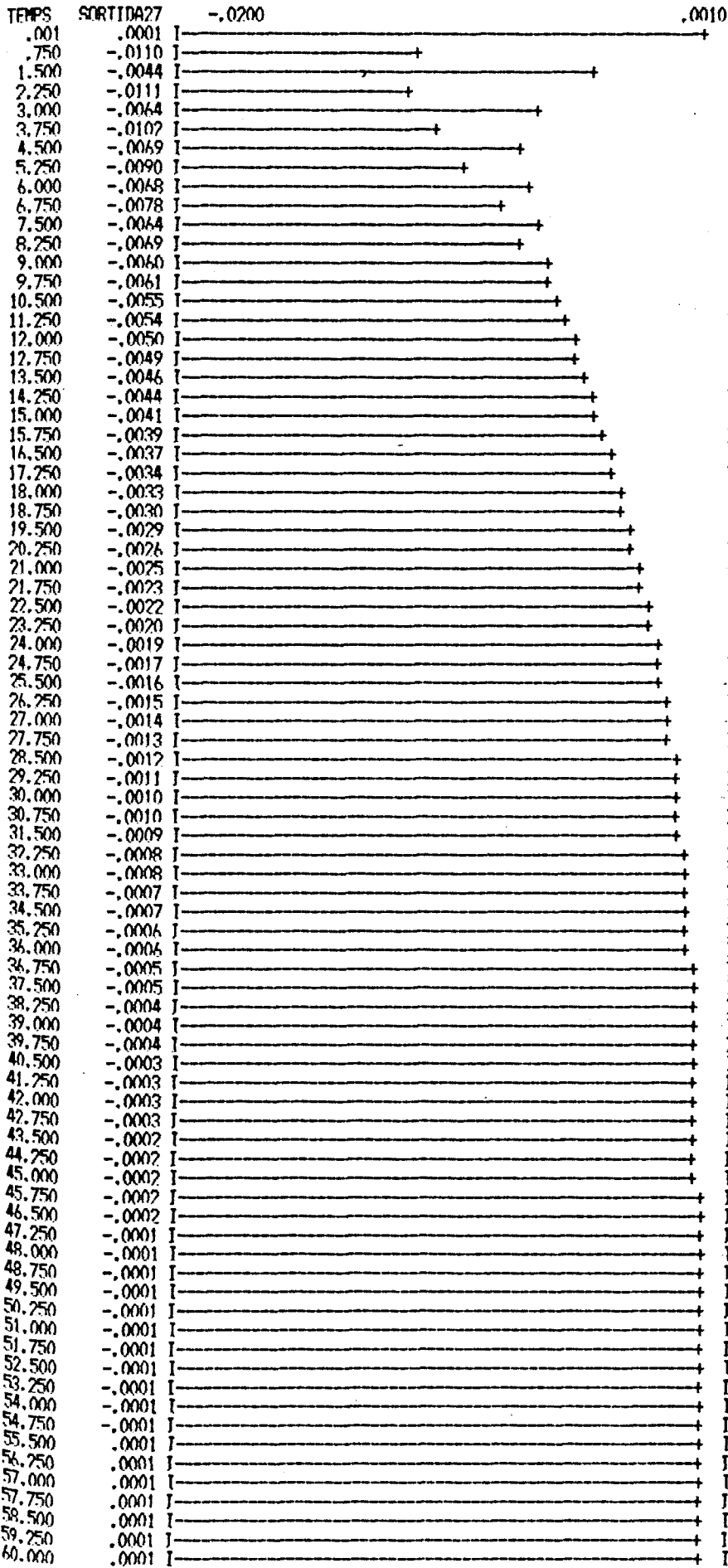
BLOC ETX Y (20) MINTM (-.0006) MAXIM (.0120)

S14.2



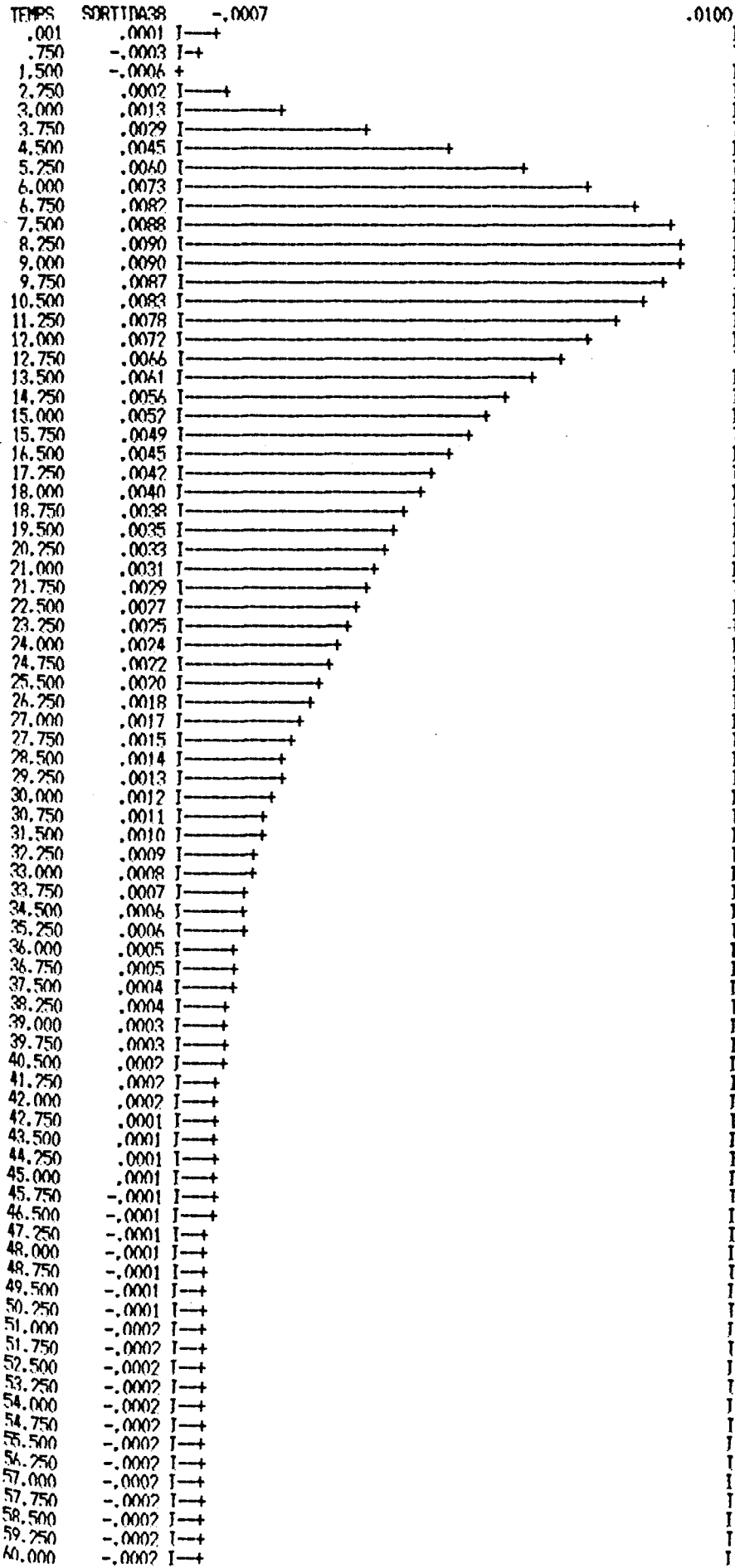
BLOC EIX Y (27) MINIM (-.0200) MAXIM (.0010)

S14.3



RLOC: EIX Y (38) MINIM (-.0007) MAXIM (.0100)

S14.4

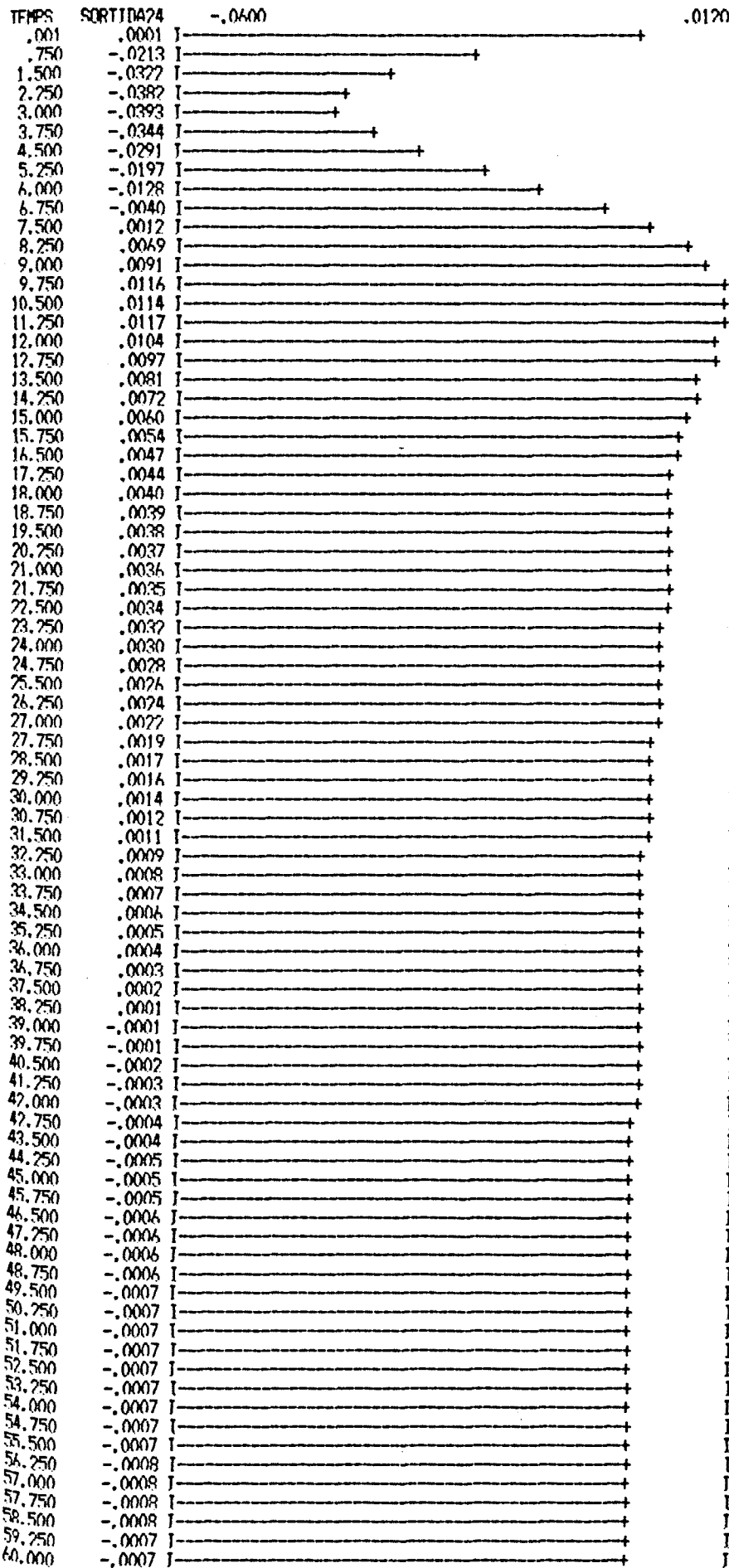


TFMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0176	-.0338	.0014	.0002
4.00	-.0423	-.0349	.0042	.0003
6.00	-.0618	-.0098	.0052	.0004
8.00	-.0762	.0071	.0053	.0005
10.00	-.0865	.0132	.0055	.0006
12.00	-.0947	.0124	.0059	.0007
14.00	-.1022	.0084	.0061	.0007
16.00	-.1090	.0056	.0062	.0008
18.00	-.1151	.0042	.0063	.0008
20.00	-.1202	.0036	.0063	.0008
22.00	-.1244	.0032	.0063	.0008
24.00	-.1279	.0027	.0064	.0008
26.00	-.1308	.0020	.0064	.0008
28.00	-.1332	.0014	.0064	.0008
30.00	-.1352	.0009	.0064	.0008
32.00	-.1368	.0005	.0064	.0008
34.00	-.1382	.0002	.0064	.0008
36.00	-.1393	-.0001	.0064	.0008
38.00	-.1402	-.0003	.0064	.0008
40.00	-.1410	-.0005	.0064	.0008
42.00	-.1416	-.0006	.0064	.0008
44.00	-.1421	-.0007	.0064	.0008
46.00	-.1425	-.0007	.0064	.0008
48.00	-.1428	-.0008	.0064	.0008
50.00	-.1431	-.0008	.0064	.0008
52.00	-.1433	-.0008	.0064	.0008
54.00	-.1434	-.0008	.0064	.0008
56.00	-.1436	-.0007	.0064	.0008
58.00	-.1437	-.0007	.0064	.0008
60.00	-.1437	-.0007	.0064	.0008
62.00	-.1438	-.0007	.0064	.0008
64.00	-.1438	-.0006	.0064	.0008
66.00	-.1439	-.0006	.0064	.0008
68.00	-.1439	-.0006	.0064	.0008
70.00	-.1439	-.0005	.0064	.0008
72.00	-.1439	-.0005	.0064	.0008
74.00	-.1440	-.0005	.0064	.0008
76.00	-.1440	-.0004	.0064	.0008
78.00	-.1440	-.0004	.0064	.0008
80.00	-.1440	-.0004	.0064	.0008
82.00	-.1440	-.0004	.0064	.0008
84.00	-.1440	-.0003	.0064	.0008
86.00	-.1440	-.0003	.0064	.0008
88.00	-.1440	-.0003	.0064	.0008
90.00	-.1440	-.0003	.0064	.0008
92.00	-.1439	-.0003	.0064	.0008
94.00	-.1439	-.0002	.0064	.0008
96.00	-.1439	-.0002	.0064	.0008
98.00	-.1439	-.0002	.0064	.0008
100.00	-.1439	-.0002	.0064	.0008
102.00	-.1439	-.0002	.0064	.0008
104.00	-.1439	-.0002	.0064	.0008
106.00	-.1439	-.0002	.0064	.0008
108.00	-.1439	-.0002	.0064	.0008
110.00	-.1439	-.0001	.0064	.0008
112.00	-.1439	-.0001	.0064	.0008
114.00	-.1439	-.0001	.0064	.0008
116.00	-.1439	-.0001	.0064	.0008
118.00	-.1439	-.0001	.0064	.0008
120.00	-.1439	-.0001	.0064	.0008
122.00	-.1439	-.0001	.0064	.0008
124.00	-.1439	-.0001	.0064	.0008
126.00	-.1439	-.0001	.0064	.0008
128.00	-.1439	-.0001	.0064	.0008
130.00	-.1439	-.0001	.0064	.0008
132.00	-.1439	-.0001	.0064	.0008
134.00	-.1439	-.0001	.0064	.0008
136.00	-.1439	-.0001	.0064	.0008
138.00	-.1439	-.0001	.0064	.0008
140.00	-.1439	-.0001	.0064	.0008
142.00	-.1439	-.0001	.0064	.0008
144.00	-.1439	-.0001	.0064	.0008
146.00	-.1439	-.0001	.0064	.0008
148.00	-.1439	-.0001	.0064	.0008
150.00	-.1439	-.0001	.0064	.0008
152.00	-.1439	-.0001	.0064	.0008
154.00	-.1439	-.0001	.0064	.0008
156.00	-.1439	-.0001	.0064	.0008
158.00	-.1439	-.0001	.0064	.0008
160.00	-.1439	-.0001	.0064	.0008

S14.5

RLOC: ETX Y (24) MINIM (-.0600) MAXIM (.0120)

S15.1



S15:

Distintas penalizaciones.

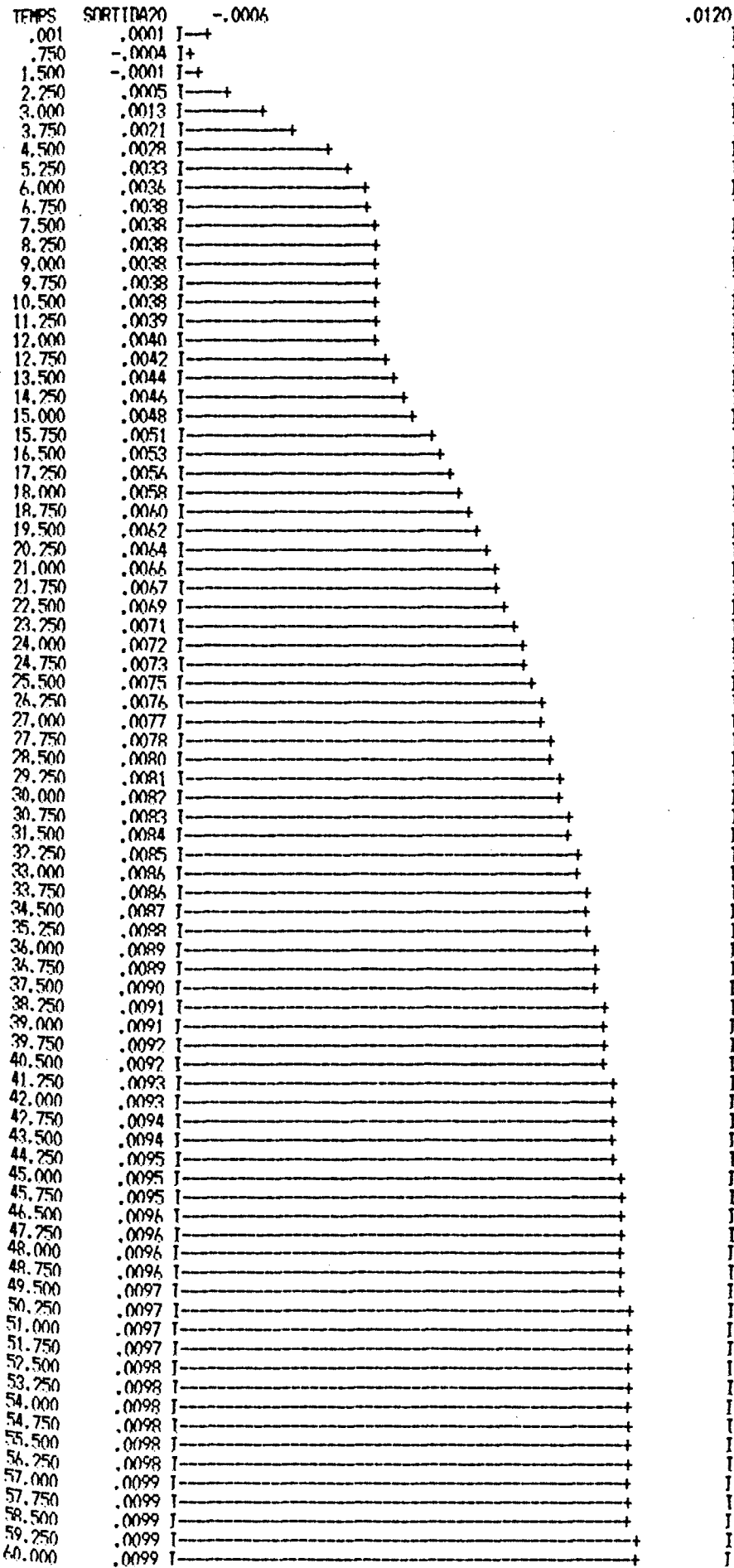
$$Q = \text{diag}(0, 2; 0, 5; 0, 2; 0, 8; 1; 0, 9; 0, 8)$$

$$R = I$$

$$\alpha_0 = 0$$

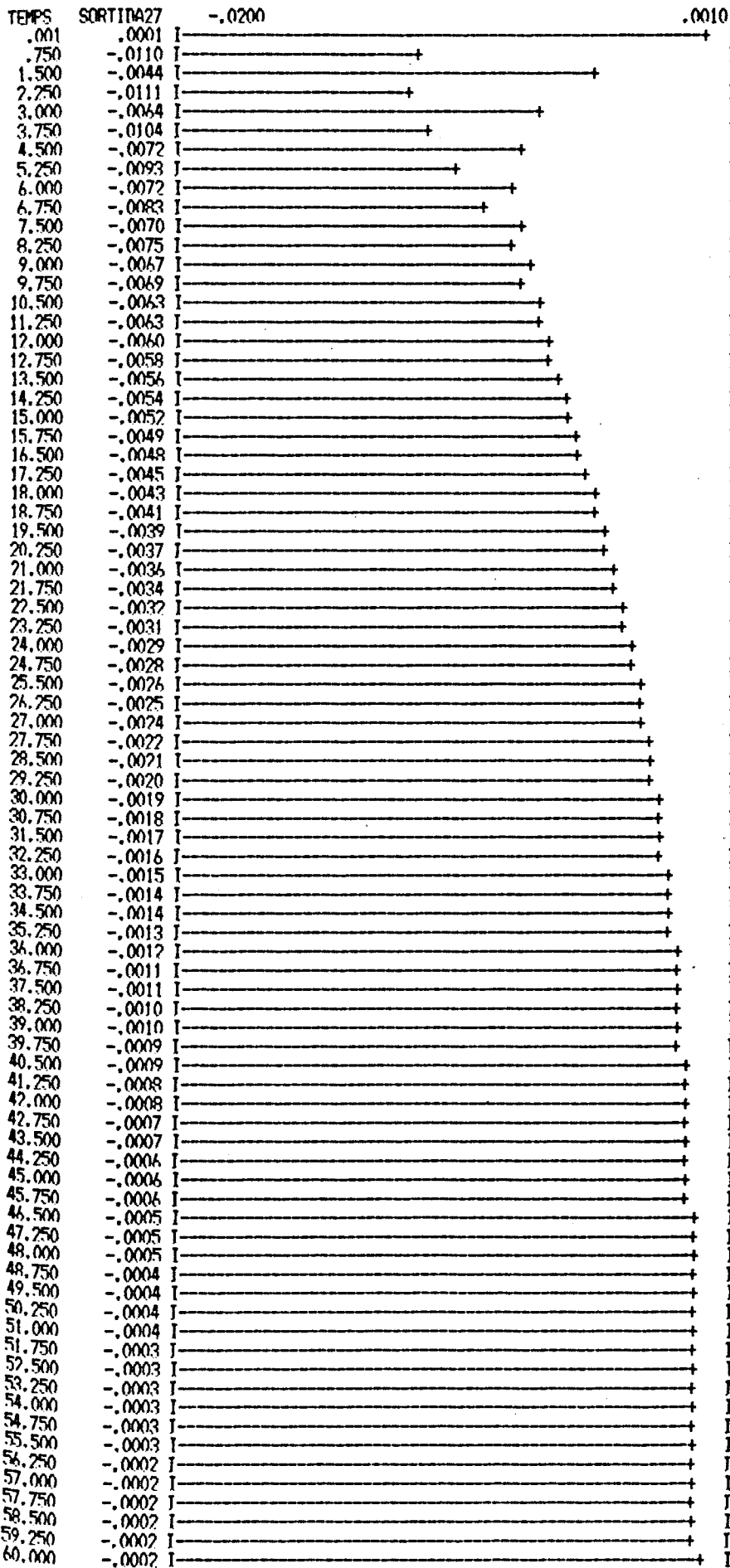
BLOC ETX Y (20) MINJM (-.0006) MAXIM (.0120)

S15.2

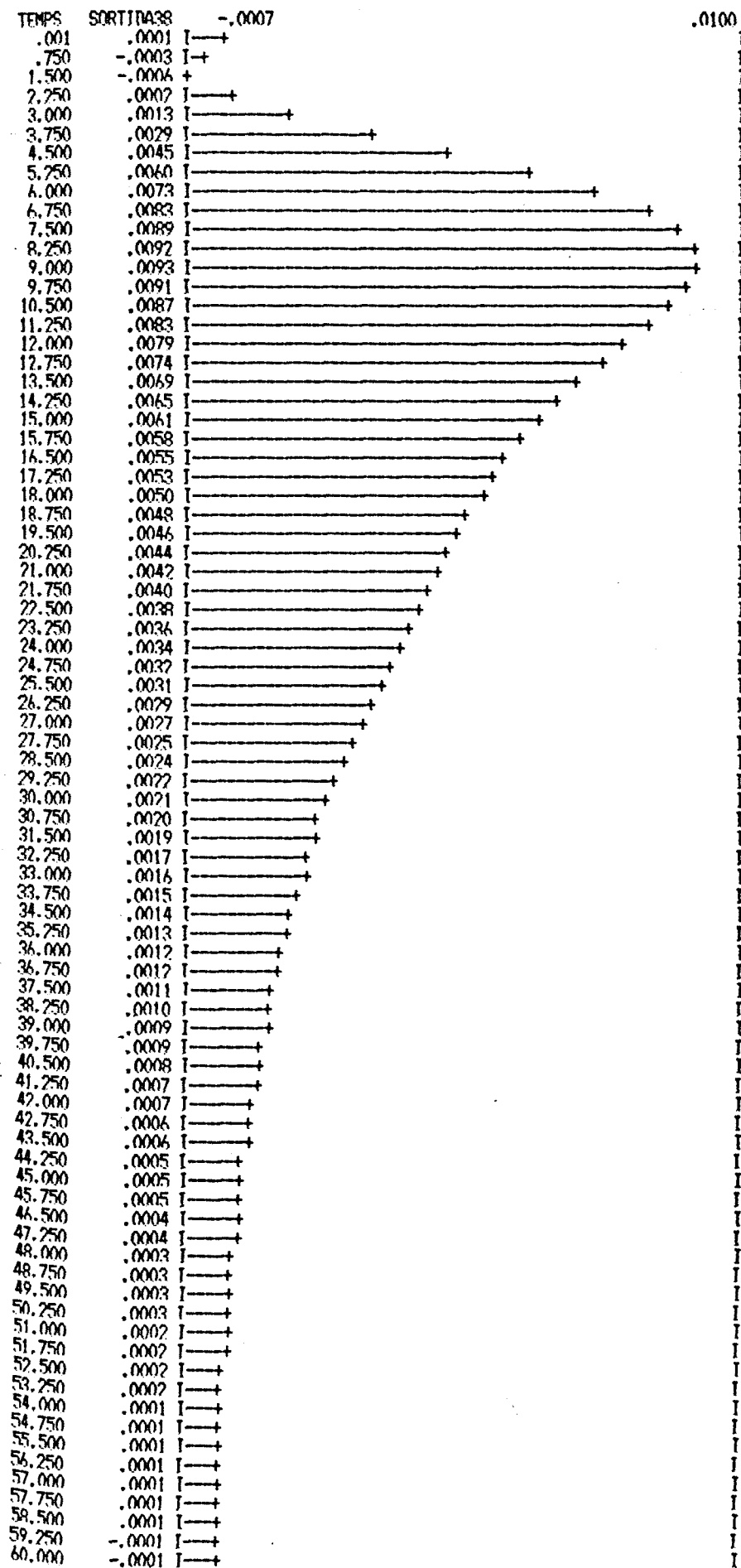


BLOC FIX Y (27) MINIM (-.0200) MAXIM (.0010)

S15.3



BLOC FIX Y (38) MINIM (-.0007) MAXIM (.0100)

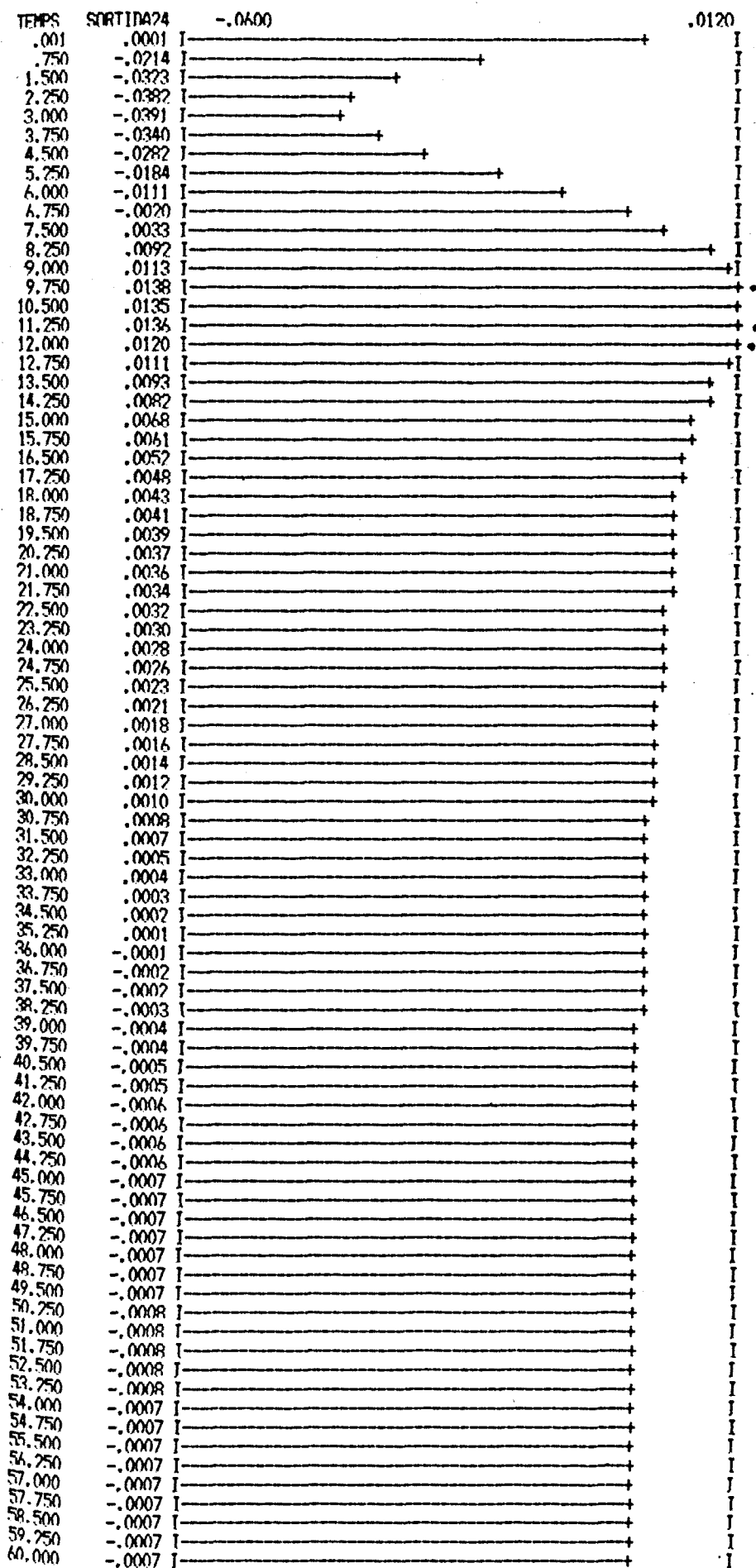
S15.4

TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0176	-.0337	.0014	.0002
4.00	-.0424	-.0355	.0042	.0003
6.00	-.0627	-.0114	.0053	.0005
8.00	-.0786	.0048	.0054	.0006
10.00	-.0907	.0110	.0056	.0007
12.00	-.1011	.0106	.0058	.0007
14.00	-.1108	.0072	.0060	.0008
16.00	-.1199	.0049	.0061	.0009
18.00	-.1282	.0039	.0061	.0009
20.00	-.1355	.0035	.0061	.0009
22.00	-.1419	.0033	.0062	.0010
24.00	-.1475	.0029	.0062	.0010
26.00	-.1523	.0023	.0062	.0010
28.00	-.1565	.0018	.0062	.0010
30.00	-.1602	.0013	.0062	.0010
32.00	-.1634	.0009	.0062	.0010
34.00	-.1662	.0006	.0062	.0010
36.00	-.1687	.0003	.0062	.0010
38.00	-.1708	.0001	.0062	.0010
40.00	-.1726	-.0002	.0062	.0010
42.00	-.1742	-.0004	.0062	.0010
44.00	-.1756	-.0005	.0062	.0010
46.00	-.1767	-.0006	.0062	.0010
48.00	-.1777	-.0006	.0062	.0010
50.00	-.1784	-.0007	.0062	.0010
52.00	-.1794	-.0007	.0062	.0010
54.00	-.1800	-.0008	.0062	.0010
56.00	-.1806	-.0008	.0062	.0010
58.00	-.1811	-.0008	.0062	.0010
60.00	-.1815	-.0008	.0062	.0010
62.00	-.1818	-.0007	.0062	.0010
64.00	-.1821	-.0007	.0062	.0010
66.00	-.1824	-.0007	.0062	.0010
68.00	-.1826	-.0007	.0062	.0010
70.00	-.1828	-.0006	.0062	.0010
72.00	-.1830	-.0006	.0062	.0010
74.00	-.1831	-.0006	.0062	.0010
76.00	-.1832	-.0006	.0062	.0010
78.00	-.1833	-.0005	.0062	.0010
80.00	-.1834	-.0005	.0062	.0010
82.00	-.1835	-.0005	.0062	.0010
84.00	-.1835	-.0004	.0062	.0010
86.00	-.1836	-.0004	.0062	.0010
88.00	-.1836	-.0004	.0062	.0010
90.00	-.1837	-.0004	.0062	.0010
92.00	-.1837	-.0004	.0062	.0010
94.00	-.1837	-.0003	.0062	.0010
96.00	-.1837	-.0003	.0062	.0010
98.00	-.1838	-.0003	.0062	.0010
100.00	-.1838	-.0003	.0062	.0010
102.00	-.1838	-.0003	.0062	.0010
104.00	-.1838	-.0002	.0062	.0010
106.00	-.1838	-.0002	.0062	.0010
108.00	-.1838	-.0002	.0062	.0010
110.00	-.1838	-.0002	.0062	.0010
112.00	-.1838	-.0002	.0062	.0010
114.00	-.1838	-.0002	.0062	.0010
116.00	-.1838	-.0002	.0062	.0010
118.00	-.1838	-.0002	.0062	.0010
120.00	-.1838	-.0002	.0062	.0010
122.00	-.1838	-.0001	.0062	.0010
124.00	-.1838	-.0001	.0062	.0010
126.00	-.1838	-.0001	.0062	.0010
128.00	-.1838	-.0001	.0062	.0010
130.00	-.1838	-.0001	.0062	.0010
132.00	-.1838	-.0001	.0062	.0010
134.00	-.1838	-.0001	.0062	.0010
136.00	-.1838	-.0001	.0062	.0010
138.00	-.1838	-.0001	.0062	.0010
140.00	-.1838	-.0001	.0062	.0010
142.00	-.1838	-.0001	.0062	.0010
144.00	-.1838	-.0001	.0062	.0010
146.00	-.1838	-.0001	.0062	.0010
148.00	-.1838	-.0001	.0062	.0010
150.00	-.1838	-.0001	.0062	.0010
152.00	-.1838	-.0001	.0062	.0010
154.00	-.1838	-.0001	.0062	.0010
156.00	-.1838	-.0001	.0062	.0010
158.00	-.1838	-.0001	.0062	.0010
160.00	-.1838	-.0001	.0062	.0010

S15.5

BLOC EIX Y (24) MINIM (-.0600) MAXIM (.0120)

S16.1



S16:

Igual que S15, con:

$$\alpha_o = 0,02$$

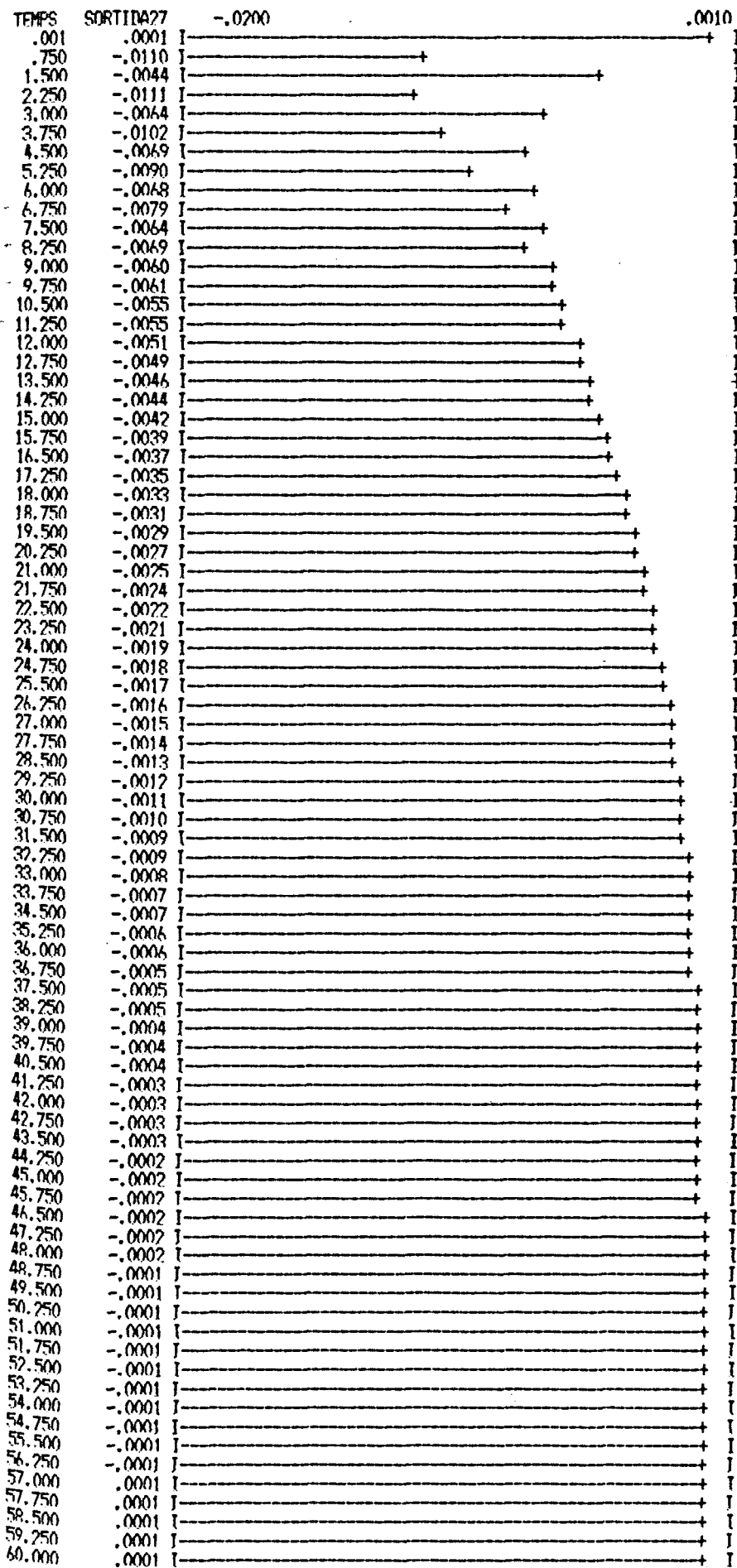
NO. FIX Y (20) MINIM (-.0006) MAXIM (.0120)

S16.2

TEMPS	SOITDA20	-.0006	.0120
.001	.0001	I--+	I
.750	-.0004	I+	I
1.500	-.0001	I+	I
2.250	.0005	I--+	I
3.000	.0015	I--+	I
3.750	.0023	I--+	I
4.500	.0031	I--+	I
5.250	.0037	I--+	I
6.000	.0041	I--+	I
6.750	.0043	I--+	I
7.500	.0045	I--+	I
8.250	.0045	I--+	I
9.000	.0045	I--+	I
9.750	.0046	I--+	I
10.500	.0046	I--+	I
11.250	.0047	I--+	I
12.000	.0049	I--+	I
12.750	.0051	I--+	I
13.500	.0053	I--+	I
14.250	.0055	I--+	I
15.000	.0058	I--+	I
15.750	.0061	I--+	I
16.500	.0063	I--+	I
17.250	.0066	I--+	I
18.000	.0068	I--+	I
18.750	.0070	I--+	I
19.500	.0072	I--+	I
20.250	.0074	I--+	I
21.000	.0076	I--+	I
21.750	.0077	I--+	I
22.500	.0079	I--+	I
23.250	.0080	I--+	I
24.000	.0082	I--+	I
24.750	.0083	I--+	I
25.500	.0084	I--+	I
26.250	.0085	I--+	I
27.000	.0086	I--+	I
27.750	.0087	I--+	I
28.500	.0088	I--+	I
29.250	.0089	I--+	I
30.000	.0090	I--+	I
30.750	.0091	I--+	I
31.500	.0091	I--+	I
32.250	.0092	I--+	I
33.000	.0093	I--+	I
33.750	.0093	I--+	I
34.500	.0094	I--+	I
35.250	.0094	I--+	I
36.000	.0095	I--+	I
36.750	.0095	I--+	I
37.500	.0096	I--+	I
38.250	.0096	I--+	I
39.000	.0097	I--+	I
39.750	.0097	I--+	I
40.500	.0097	I--+	I
41.250	.0098	I--+	I
42.000	.0098	I--+	I
42.750	.0098	I--+	I
43.500	.0098	I--+	I
44.250	.0099	I--+	I
45.000	.0099	I--+	I
45.750	.0099	I--+	I
46.500	.0099	I--+	I
47.250	.0099	I--+	I
48.000	.0099	I--+	I
48.750	.0100	I--+	I
49.500	.0100	I--+	I
50.250	.0100	I--+	I
51.000	.0100	I--+	I
51.750	.0100	I--+	I
52.500	.0100	I--+	I
53.250	.0100	I--+	I
54.000	.0100	I--+	I
54.750	.0100	I--+	I
55.500	.0100	I--+	I
56.250	.0100	I--+	I
57.000	.0100	I--+	I
57.750	.0100	I--+	I
58.500	.0101	I--+	I
59.250	.0101	I--+	I
60.000	.0101	I--+	I

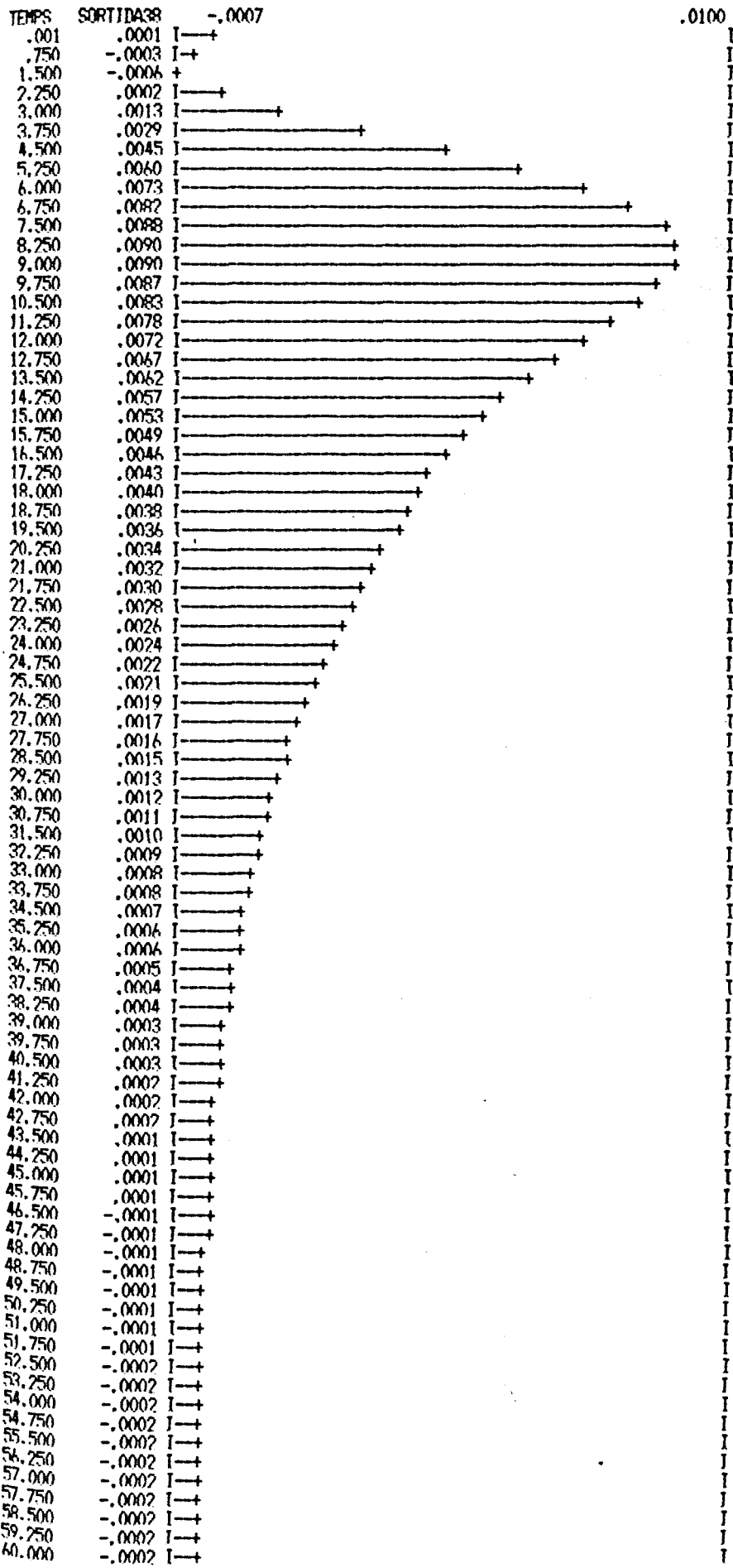
BLOC EIX Y (27) MINIM (-.0200) MAXIM (.0010)

S16.3



BLOC EIX Y (38) MINIM (-.0007) MAXIM (.0100)

S16.4



TEMPS	SORTIDA46	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0176	-.0338	.0014	.0002
4.00	-.0473	-.0350	.0042	.0003
6.00	-.0618	-.0099	.0057	.0004
8.00	-.0762	.0070	.0053	.0005
10.00	-.0866	.0131	.0055	.0006
12.00	-.0949	.0123	.0059	.0007
14.00	-.1026	.0082	.0061	.0007
16.00	-.1095	.0055	.0062	.0008
18.00	-.1157	.0042	.0063	.0008
20.00	-.1209	.0036	.0063	.0008
22.00	-.1252	.0032	.0063	.0008
24.00	-.1288	.0027	.0063	.0008
26.00	-.1318	.0020	.0063	.0008
28.00	-.1343	.0014	.0064	.0008
30.00	-.1364	.0009	.0064	.0008
32.00	-.1381	.0005	.0064	.0008
34.00	-.1396	.0002	.0064	.0008
36.00	-.1408	-.0001	.0064	.0008
38.00	-.1418	-.0003	.0064	.0008
40.00	-.1426	-.0005	.0064	.0008
42.00	-.1432	-.0006	.0064	.0008
44.00	-.1438	-.0007	.0064	.0008
46.00	-.1442	-.0007	.0064	.0008
48.00	-.1446	-.0007	.0064	.0008
50.00	-.1449	-.0008	.0064	.0008
52.00	-.1451	-.0008	.0064	.0008
54.00	-.1453	-.0008	.0064	.0008
56.00	-.1455	-.0007	.0064	.0008
58.00	-.1456	-.0007	.0064	.0008
60.00	-.1457	-.0007	.0064	.0008
62.00	-.1458	-.0007	.0064	.0008
64.00	-.1458	-.0006	.0064	.0008
66.00	-.1459	-.0006	.0064	.0008
68.00	-.1459	-.0006	.0064	.0008
70.00	-.1459	-.0005	.0064	.0008
72.00	-.1460	-.0005	.0064	.0008
74.00	-.1460	-.0005	.0064	.0008
76.00	-.1460	-.0004	.0064	.0008
78.00	-.1460	-.0004	.0064	.0008
80.00	-.1460	-.0004	.0064	.0008
82.00	-.1460	-.0004	.0064	.0008
84.00	-.1460	-.0003	.0064	.0008
86.00	-.1460	-.0003	.0064	.0008
88.00	-.1460	-.0003	.0064	.0008
90.00	-.1460	-.0003	.0064	.0008
92.00	-.1460	-.0003	.0064	.0008
94.00	-.1460	-.0002	.0064	.0008
96.00	-.1460	-.0002	.0064	.0008
98.00	-.1460	-.0002	.0064	.0008
100.00	-.1460	-.0002	.0064	.0008
102.00	-.1460	-.0002	.0064	.0008
104.00	-.1460	-.0002	.0064	.0008
106.00	-.1460	-.0002	.0064	.0008
108.00	-.1460	-.0002	.0064	.0008
110.00	-.1460	-.0001	.0064	.0008
112.00	-.1460	-.0001	.0064	.0008
114.00	-.1460	-.0001	.0064	.0008
116.00	-.1460	-.0001	.0064	.0008
118.00	-.1460	-.0001	.0064	.0008
120.00	-.1460	-.0001	.0064	.0008
122.00	-.1460	-.0001	.0064	.0008
124.00	-.1460	-.0001	.0064	.0008
126.00	-.1460	-.0001	.0064	.0008
128.00	-.1460	-.0001	.0064	.0008
130.00	-.1459	-.0001	.0064	.0008
132.00	-.1459	-.0001	.0064	.0008
134.00	-.1459	-.0001	.0064	.0008
136.00	-.1459	-.0001	.0064	.0008
138.00	-.1459	-.0001	.0064	.0008
140.00	-.1459	-.0001	.0064	.0008
142.00	-.1459	-.0001	.0064	.0008
144.00	-.1459	-.0001	.0064	.0008
146.00	-.1459	-.0001	.0064	.0008
148.00	-.1459	-.0001	.0064	.0008
150.00	-.1459	-.0001	.0064	.0008
152.00	-.1459	-.0001	.0064	.0008
154.00	-.1459	-.0001	.0064	.0008
156.00	-.1459	-.0001	.0064	.0008
158.00	-.1459	-.0001	.0064	.0008
160.00	-.1459	-.0001	.0064	.0008

APENDICE F:

Programas desarrollados para el diseño del RLO discreto.

Los diferentes programas que se exponen en este Apéndice se han desarrollado para obtener la ley de control óptima para el caso del RLO discreto, tanto cuando la acción de control era simple y sin retardos como cuando había retardos o era múltiple. En concreto, los programas efectúan los siguientes cálculos:

Datos	Programa (s)	Resultados
\tilde{A}	TRAD	$\tilde{\Phi}(T)$
$\tilde{\Phi}(t)$	TRANS	$\tilde{\Phi}(T)$
$\tilde{\Phi}(t) + \tilde{B}$	FITA	$\tilde{\Theta}(T)$
$\tilde{\Phi}(T) + \tilde{\Theta}(T)$ $+ \tilde{Q} + \tilde{R}$	MATQ SIMP MATPES	$\hat{Q}(T), \hat{R}(T),$ $\tilde{V}(T), \tilde{M}_i(T)$
$\tilde{\Phi}(T) + \tilde{\Theta}(T)$ $+ \hat{Q}(T) + \hat{R}(T)$	RTRT RTR2	Solución de las ecuaciones de Riccati [62.16] y [62.18]
$\tilde{\Phi}(T) + \tilde{\Theta}(T)$ $+ \hat{Q}(T) + \hat{R}(T) +$ $\tilde{M}_i(T) + \tilde{V}(T)$	MULTC MULTR	Solución de la ecuación de Riccati [63.28]

A diferencia del programa "BASMAT" de la ref. [126], usado para el cálculo de la ecuación de Riccati asociada al modelo continuo del Capítulo 5, y que se había programado en Fortran, los programas de este Apéndice lo han sido en Basic, dado que el tiempo de cálculo del RLO discreto es, para una misma planta, sensiblemente menor que el del RLO continuo.

Puesto que los resultados de unos programas constituyen los datos de entrada de otros, lo ideal sería usar un único programa estructurado. Pero, dadas las limitaciones del TI990 sobre el que se han implementado (19 KB de memoria disponibles para el usuario), se ha recurrido a un programa independiente para cada cálculo, creándose unos ficheros para el intercambio de datos. En todo caso, su adaptación a un ordenador de mayor capacidad solo requerirá una sencilla depuración de las subrutinas de entrada y salida de datos.

TRAD : Calcula la matriz de planta discreta ($\tilde{\Phi}(T)$) a partir de la continua (A) mediante el desarrollo en serie de Taylor de $\tilde{\Phi}(T)$.

$$\tilde{\Phi}(T) = e^{AT} = \tilde{I} + \tilde{A}T + \frac{\tilde{A}^2 T^2}{2!} + \frac{\tilde{A}^3 T^3}{3!} + \dots$$

Orden de la planta ≤ 7 .

Número de términos del desarrollo seleccionable.

TRANS : Efectua el mismo cálculo que "TRAD" a partir del desarrollo de Sylvester [120], para lo cual deben obtenerse con el programa "BASMAT" [126] los autovalores λ_i y las matrices F_i de

$$\tilde{\Phi}(t) = F_1 e^{\lambda_1 t} + F_2 e^{\lambda_2 t} + \dots + F_N e^{\lambda_N t},$$

encargándose el programa "TRANS" de particularizar para $t = T$. La precisión obtenida es la misma (hasta el 12º decimal) que en "TRAD" cuando en éste se seleccionan más de 5 términos del desarrollo.

FITA : Calcula (para $B = \text{cte}$),

$$\begin{aligned} \tilde{\Theta}(T) &= \int_0^T \tilde{\Phi}(\tau) \tilde{B} d\tau = \\ &= \int_0^T (F_1 e^{\lambda_1 \tau} + \dots + F_N e^{\lambda_N \tau}) \tilde{B} d\tau. \end{aligned}$$

debiéndose entrar la integral indefinida de la matriz de transición de estado $\tilde{\Phi}(t)$, obtenida con el programa "BASMAT".

MATQ
SIMP
MATPES

Calculan las matrices de ponderación de los criterios integrales adecuados al caso discreto a partir de las matrices Q y R del clásico criterio integral cuadrático continuo.

RTRT
RTR2

Resolución de la ecuación de Riccati para muestreo simple.

MULTC
MULTR

Resolución de la ecuación de Riccati para muestreo doble.

P.1

```

10 DIM R(7,7),Z(7,7),A(7,7),B(7,7),D(7,7),Y(7,7)
20 PRINT FRASE ALL
30 PRINT "ORDRE DE LA PLANTA"
40 INPUT H
50 PRINT FRASE ALL
60 PRINT "MATRILIA"
70 CALL MINT(A(,),H,H)
80 PRINT FRASE ALL
90 PRINT "T DE MOSTREIG"
100 INPUT T
110 PRINT "NOMBRE D'ITERATIONS"
120 INPUT N
130 K=0
140 CALL MIND(R(,),H)
150 CALL MIND(Z(,),H)
160 C=T/(K+1)
170 CALL MPRC(C,A(,),R(,),H,H)
180 CALL MPRD(R(,),B(,),D(,),H,H,H)
190 FOR U=1 TO H
200 FOR J=1 TO H
210 R(U,J)=D(U,J)
220 NEXT J::NEXT U
230 CALL MADD(R(,),"+",Z(,),Y(,),H,H)
240 FOR U=1 TO H
250 FOR J=1 TO H
260 Z(U,J)=Y(U,J)
270 NEXT J::NEXT U
275 PRINT FRASE ALL
280 CALL MOUT(Z(,),H,H)
290 K=K+1
300 PRINT K
310 IF K<N THEN GOTO 160
315 OPEN #8:"DISC2:TRAB"
320 CALL MDD(Z(,),H,H,8)
325 CLOSE #8
330 END
6130 SUB MOUT(X(,),F,C)
6140 TA=INT(80/C)
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6170 PRINT AT (I+2,(J-1)*TA) USING A180:X(I,J)
6180 IMAGE ##.###^
6190 NEXT J::NEXT I
6200 SUBEND
6210 SUB MINT(X(,),F,C)
6220 REM PRINT FRASE ALL
6230 TA=INT(80/C)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT AT (I+2,(J-1)*TA):X(I,J)
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(I,J)=0
6330 FOR K=1 TO XY
6340 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
6350 NEXT K::NEXT J::N

```

} $\tilde{A}(t)$

} T

→ $\phi(T)$

TRAD

$$\tilde{\Phi}(T) = e^{\tilde{A}T} = \tilde{I} + \tilde{A}T + \frac{\tilde{A}^2 T^2}{2!} + \frac{\tilde{A}^3 T^3}{3!} + \dots$$


```

80 DIM A9(7,7),R9(7,7),C9(7,7),D9(7,7),E9(7,7),F9(7,7),G9(7,7) } ORDEN 7
81 DIM D9(7,7),P9(7,7),Q9(7,7),R9(7,7),S9(7,7),T9(7,7)
82 DIM V(7,7)
90 PRINT FRASE ALL
95 PP=0
97 TT=0
99 OPEN #1:"DISC2:MOD1"
100 OPEN #2:"DISC2:MOD2"
101 OPEN #3:"DISC2:MOD3"
102 OPEN #4:"DISC2:MOD4"
105 H9=(EXP(-5.7934E-01*TT))*COS(.43693*TT)
110 I9=(EXP(-5.7934E-01*TT))*SIN(.43693*TT)
115 J9=EXP(-2.0528E-01*TT)
120 K9=EXP(-2.3794*TT)
130 L9=(EXP(-3.1117E-01*TT))*COS(4.301*TT)
140 M9=(EXP(-3.1117E-01*TT))*SIN(4.301*TT)
150 PRINT "MAT 1"
160 CALL MINT(A9(,),7,7,1)
170 PRINT "MAT 2"
175 CALL MINT(R9(,),7,7,2)
180 PRINT "MAT 3"
185 CALL MINT(C9(,),7,7,3)
186 CLOSE #1
187 CLOSE #2
188 CLOSE #3
190 PRINT "MAT 4"
200 CALL MINT(D9(,),7,7,4)
202 CLOSE #4
210 PRINT "MAT 5"
212 OPEN #5:"DISC2:MOD5"
213 OPEN #6:"DISC2:MOD6"
214 OPEN #7:"DISC2:MOD7"
220 CALL MINT(E9(,),7,7,5)
230 PRINT "MAT 6"
240 CALL MINT(F9(,),7,7,6)
250 PRINT "MAT 7"
260 CALL MINT(G9(,),7,7,7)
266 CLOSE #5
267 CLOSE #6
268 CLOSE #7
280 CALL MPRC(I9,A9(,),D9(,),7,7)
290 CALL MPRC(H9,R9(,),P9(,),7,7)
300 CALL MPRC(L9,C9(,),Q9(,),7,7)
310 CALL MPRC(K9,D9(,),R9(,),7,7)
320 CALL MPRC(J9,E9(,),S9(,),7,7)
330 CALL MPRC(M9,F9(,),T9(,),7,7)
340 CALL MADD(D9(,),"+",P9(,),A9(,),7,7)
350 CALL MADD(Q9(,),"+",R9(,),R9(,),7,7)
360 CALL MADD(S9(,),"+",T9(,),C9(,),7,7)
370 CALL MADD(A9(,),"+",R9(,),D9(,),7,7)
380 CALL MADD(C9(,),"+",G9(,),S9(,),7,7)
381 CALL MADD(D9(,),"+",S9(,),F9(,),7,7)
382 IF PP=1 THEN GOTO 4387
383 FOR I=1 TO 7
384 FOR J=1 TO 7

```

$\tilde{F}_1, \tilde{F}_2, \tilde{F}_3, \tilde{F}_4$

105-140:
COEFICIENTES λ_i (AUTOVALORES)
(SALIDA DE "BASMAT")

Modificación del orden:

- 1/ 80-82: DIM ... (N,N).
- 2/ ADAPTAR 105-140 A LOS VALORES DE SALIDA DEL "BASMAT"
- 3/ ELIMINAR LA ENTRADA DE LOS \tilde{F}_i SOBREVANTES.
- 4/ ADECUAR LA DIMENSION DE LAS MATRICES RESULTADO

$\tilde{F}_5, \tilde{F}_6, \tilde{F}_7$



$$\begin{aligned}
 \Phi(T) &= e^{\tilde{A}T} \\
 &= \tilde{F}_1 e^{\lambda_1 T} + \tilde{F}_2 e^{\lambda_2 T} + \dots + \tilde{F}_N e^{\lambda_N T} \\
 &\quad (N \leq 7)
 \end{aligned}$$

```

385 V(I,J)=F9(I,J)
386 NEXT J:=NEXT J
388 PP=1
389 PRINT FRASE ALL
390 PRINT "T DE MOSTREIG"
391 INPUT TT
392 GOTO 99
4387 CALL MADD(F9(,),"-",V(,),F9(,),7,7) (*)
4388 FOR I=1 TO 7
4390 F9(I,I)=F9(I,I)+1
4391 NEXT I
5389 OPEN #8:"DSC:TRR1"
5390 PRINT FRASE ALL
5391 CALL MOUT(F9(,),7,7,8) → Φ(T)
5392 CLOSE #8
5395 END
6130 SUB MOUT(X(,),F,C,LT)
6140 TA=INT(80/C)
6150 FOR J=1 TO F
6160 FOR I=1 TO C
6170 PRINT AT (I+2,(J-1)*TA) USING 6175:X(I,J)
6175 IMAGE ##.###^
6180 PRINT #1 T:X(J,I)
6190 NEXT I:=NEXT I
6200 SUBEND
6210 SUB MINT(X(,),F,C,IL)
6230 TA=INT(80/C)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT #1 I:X(J,I)
6270 NEXT J:=NEXT J
6325 SUBEND
6430 SUB MADD(X(,),X$,V(,),7(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN 7(I,J)=X(I,J)+V(I,J)
6470 IF X$="-" THEN 7(I,J)=X(I,J)-V(I,J)
6480 NEXT J:=NEXT J
6490 SUBEND
6630 SUB MPRC(A,X(,),7(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 7(I,J)=A*X(I,J)
6670 NEXT J:=NEXT J
6680 SUBEND

```

(*) : Si no hubiera errores de truncamiento y redondeo,

$$\tilde{V} = \tilde{\Phi}(0) = \tilde{I}.$$

Dado que, en realidad, $\tilde{V} \approx \tilde{I}$, por imprecisiones de "BASHAT", en 4387 y 4390 se compensan estos errores:

$$\text{BASHAT} \rightarrow \tilde{T}_1, \tilde{T}_2, \dots, \tilde{T}_N$$

$$\tilde{V} = f_1(\tilde{T}_1, \tilde{T}_2, \dots, \tilde{T}_N) = \tilde{I} + \psi$$

$$\tilde{\Phi}_c(T) = f_2(\tilde{T}_1, \tilde{T}_2, \dots, \tilde{T}_N) = \tilde{\Phi}(T) + \psi$$

$$\tilde{\Phi}(T) = \tilde{\Phi}_c(T) - \tilde{V} + \tilde{I}$$

INTEGRAL DE SALIDA DEL "BASMAT",
LOS TERMINOS DE

```

1 REM ****A "620" ES POT CANVIAR EL FITXER DE SORTIDA DE DADRES"
10 DIM A9(7,7),B9(7,7),C9(7,7),D9(7,7),F9(7,7),F9(7,7),G9(7,7)
11 DIM O9(7,7)
12 DIM H(7,7)
13 DIM S(7,7)
14 DIM P(7,7)
20 PRINT FRASE ALI
35 PP=0
40 PRINT "TEMPS DE MOSTREIG"
45 INPUT TT
50 OPEN #1:"DSC2:MOD1",INPUT
51 OPEN #2:"DSC2:MOD2"
52 OPEN #3:"DSC2:MOD3"
105 H9=EXP(-5.7934E-01*TT)*(-.57934*COS(.43693*TT)+.43693*SIN(.43693*TT))
106 H9=H9/((.57934^2)+(.43693^2))
110 I9=EXP(-5.7934E-01*TT)*(-.57934*SIN(.43693*TT)-.43693*COS(.43693*TT))
111 I9=I9/((.57934^2)+(.43693^2))
115 J9=EXP(-2.0528E-01*TT)/(-.20528)
120 K9=EXP(-2.3794*TT)/(-2.3794)
130 L9=EXP(-3.1117E-01*TT)*(-.31117*COS(4.301*TT)+4.301*SIN(4.301*TT))
131 O5=(.31117^2)+(4.301^2)
132 I9=I9/O5
140 M9=EXP(-3.1117E-01*TT)*(-.31117*SIN(4.301*TT)-4.301*COS(4.301*TT))
141 M9=M9/O5
150 PRINT "MAT 1"
160 CALL MINT(A9(,),7,7,1)
170 PRINT "MAT 2"
175 CALL MINT(B9(,),7,7,2)
180 PRINT "MAT 3"
185 CALL MINT(C9(,),7,7,3)
186 CLOSE #1
187 CLOSE #2
188 CLOSE #3
190 PRINT "MAT 4"
195 OPEN #4:"DSC2:MOD4"
200 CALL MINT(D9(,),7,7,4)
202 CLOSE #4
210 PRINT "MAT 5"
212 OPEN #5:"DSC2:MOD5"
213 OPEN #6:"DSC2:MOD6"
214 OPEN #7:"DSC2:MOD7"
220 CALL MINT(F9(,),7,7,5)
230 PRINT "MAT 6"
240 CALL MINT(F9(,),7,7,6)
250 PRINT "MAT 7"
260 CALL MINT(G9(,),7,7,7)
266 CLOSE #5
267 CLOSE #6
268 CLOSE #7
280 CALL MPRC(I9,A9(,),O9(,),7,7)
290 CALL MPRC(H9,B9(,),A9(,),7,7)
300 CALL MPRC(I9,C9(,),B9(,),7,7)
310 CALL MPRC(K9,D9(,),C9(,),7,7)
320 CALL MPRC(L9,F9(,),D9(,),7,7)
330 CALL MPRC(M9,F9(,),F9(,),7,7)
    
```

F_1, F_2, F_3

F_4

F_5, F_6, F_7

Modificación del orden:

- 1/ 10-40: DIM....(N,N)
- 2/ 105-141: INTEGRAL DE LOS NUEVOS VALORES DE $e^{\lambda t}$ ("BASMAT")
- 3/ ELIMINAR LA ENTRADA DE LOS F_i SOBREVANTES.
- 4/ ADECUAR LA DIMENSION DE LAS MATRICES RESULTADO.

FITA

$$\begin{aligned}
 \tilde{\Theta}(T) &= \int_0^T \tilde{\Phi}(t) \tilde{B} dt = \\
 &= \int_0^T (\tilde{F}_1 e^{\lambda_1 t} + \tilde{F}_2 e^{\lambda_2 t} + \dots + \tilde{F}_N e^{\lambda_N t}) \tilde{B} dt
 \end{aligned}$$

```

331 CALL MPRD(TT,G9(,),F9(,),7,7)
340 CALL MADD(O9(,),"+",A9(,),P9(,),7,7)
350 CALL MADD(R9(,),"+",C9(,),A9(,),7,7)
360 CALL MADD(O9(,),"+",F9(,),R9(,),7,7)
370 CALL MADD(P9(,),"+",A9(,),C9(,),7,7)
380 CALL MADD(F9(,),"+",R9(,),G9(,),7,7)
381 CALL MADD(C9(,),"+",G9(,),O9(,),7,7)
382 IF PP=1 THEN GOTO 388
383 FOR J=1 TO 7
384 FOR I=1 TO 7
385 H(I,,I)=O9(I,,I)
386 NEXT I::NEXT I
387 GOTO 394
388 CALL MADD(H(,),"-",O9(,),B9(,),7,7)
394 GOTO 500
396 TT=0
397 PP=1
400 GOTO 50
500 PRINT FRASE ALL
505 TA=80
510 FOR I=1 TO 7
520 INPUT AT (I+2,0):S(I,,I)
530 NEXT I
540 CALL MPRD(R9(,),S(,),A9(,),7,7,1)
550 OPEN #8:"DSC2:TRAS"
560 CALL MOUT(A9(,),7,1,8)
570 CLOSE #8
580 FND
6130 SUB MOUT(X(,),F,C,I,T)
6140 TA=INT(80/C)
6150 FOR J=1 TO F
6160 FOR I=1 TO C
6170 PRINT AT (I+2,(J-1)*TA) USING 6175:X(I,,I)
6175 IMAGE ##.###^
6180 PRINT #I T:X(I,,I)
6190 NEXT I::NEXT I
6200 SUBFND
6210 SUB MINT(X(,),F,C,I,I)
6220 TA=INT(80/C)
6240 FOR J=1 TO F
6250 FOR I=1 TO C
6260 INPUT #I I:X(I,,I)
6270 NEXT I::NEXT I
6280 SUBFND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR I=1 TO CY
6310 FOR J=1 TO FX
6320 Z(I,,I)=0
6330 FOR K=1 TO XY
6340 Z(I,,I)=Z(I,,I)+X(I,,K)*Y(K,,I)
6350 NEXT K::NEXT I::NEXT I
6360 SUBFND
6430 SUB MADD(X(,),X$,Y(,),Z(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C

```

↑ B
~

```
6460 IF X$="+" THEN Z(I,,J)=X(I,J)+Y(I,,J)
6470 IF X$="-" THEN Z(I,,J)=X(I,,J)-Y(I,,J)
6480 NEXT J, I::NEXT I
6490 SUBEND
6530 SUB MPROC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,,J)=A*(INT(X(I,J)*100)/100)
6670 NEXT J, I::NEXT J
6680 SUBEND
```

```

10 DIM A(7,7),B(7,7),C(7,7),D(7,7),E(7,7)
11 DIM F(7,7)
20 CALL MINT(D(.,.),7) | DEFINICION DE Q
30 R(5,5)=1
40 CALL M7FR(A(.,.),7,7)
50 OPEN #1:"DSC:T1"
60 OPEN #2:"DSC:T2"
70 OPEN #3:"DSC:T3"
80 OPEN #4:"DSC:T4"
90 HH=1
100 CALL MINT(R(.,.),7,7,HH)
120 CALL MTRA(R(.,.),D(.,.),7,7)
130 CALL MPRD(R(.,.),R(.,.),C(.,.),7,7,7)
140 CALL MPRD(D(.,.),D(.,.),R(.,.),7,7,7)
150 CALL MATD(A(.,.),"+",R(.,.),E(.,.),7,7)
160 FOR I=1 TO 7
165 FOR J=1 TO 7
170 A(I.,J)=E(I.,J)
180 NEXT J.:NEXT I
188 HH=HH+1
195 IF HH=5 THEN GOTO 300
198 IF HH=9 THEN GOTO 500
200 GOTO 100
300 CLOSE #1
310 CLOSE #2
320 CLOSE #3
330 CLOSE #4
340 OPEN #5:"DSC:T5"
350 OPEN #6:"DSC:T6"
360 OPEN #7:"DSC:T7"
370 OPEN #8:"DSC:T8"
399 GOTO 100
500 CLOSE #5
510 CLOSE #6
520 CLOSE #7
530 CLOSE #8
600 OPEN #9:"DSC:TE"
610 CALL MOUT(E(.,.),7,7)
650 CLOSE #9
700 END
6130 SUB MOUT(X(.,.),F,C)
6140 TA=INT(RO/C)
6150 FOR J=1 TO F
6160 FOR I=1 TO C
6170 PRINT #9:X(I.,J)
6175 PRINT AT(I+1,(J-1)*TA) USING 6180:X(I.,J)
6180 IMAGE ##.###^
6190 NEXT J.:NEXT I
6200 SUBEND
6210 SUB MINT(X(.,.),F,C,I)
6220 PRINT ERASE ALL
6230 TA=INT(RO/C)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT #I:X(I.,J)

```

PARA ORDEN 7.

Ecuaciones 62.12 y 63.6

CASO $w(T) = \hat{Q}(T)$
 $T_i = \Phi(1)$

CASO $w(T) = \hat{R}(T)$
 $T_i = \Phi(1) \Theta(i)$

CASO $w(T) = V(T)$
 $T_i = \Theta(i)$

(T = 8 seg)

$$E = T_1^T Q T_1 + T_2^T Q T_2 + \dots + T_F^T Q T_F = \hat{Q}(8)$$

MATQ

INTEGRACION POR LA REGLA DE SIMPSON.

Calculo de las matrices de ponderacion de [62.12] y de [63.6] a partir de la expresion general:

$$w(T) = \int_0^T [\underbrace{\varphi(t-\tau)}_{\sim} \underbrace{y(t-k\tau+\tau)}_{\sim} \underbrace{Q}_{\sim} \underbrace{F(t-k\tau+\tau)}_{\sim} \underbrace{\Omega(t-\tau)}_{\sim}] dz$$

```
6261 PRINT AT(T+1,(J-1)*TA) USING A264:X(T,,J)
6264 IMAGE ##.###^
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(T,,J)=0
6330 FOR K=1 TO XY
6340 Z(T,,J)=Z(T,,J)+X(T,K)*Y(K,,J)
6350 NEXT K::NEXT I::NEXT J
6360 SUBEND
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(T,,J)=X(J,,I)
6410 NEXT J::NEXT I
6420 SUBEND
6430 SUB MADN(X(,),X$,Y(,),Z(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(T,,J)=X(T,,J)+Y(T,,J)
6470 IF X$="-" THEN Z(T,,J)=X(T,,J)-Y(T,,J)
6480 NEXT J::NEXT I
6490 SUBEND
6500 SUB M7FR(X(,),F,C)
6510 FOR I=1 TO F
6520 FOR J=1 TO C
6530 X(T,,J)=0.0
6540 NEXT J::NEXT I
6550 SUBEND
6560 SUB MTND(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(T,,J)=0.0
6600 IF I=J THEN X(T,,J)=0.5
6610 NEXT J::NEXT I
6620 SUBEND
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(T,,J)=A*X(T,,J)
6670 NEXT J::NEXT I
6680 SUBEND
```

```

10 DIM A(7,1),B(7,7),C(7,7),D(7,7),E(7,7) | PARA ORDEN 7
11 DIM F(7,1),F(7,7)
20 CALL MINT(D(.,),7) | DEFINICION DE Q.
30 D(5,5)=1
40 CALL MZER(A(.,),7,1)
50 OPEN #1:"DISC:T1"
60 OPEN #2:"DISC:T2"
70 OPEN #3:"DISC:T11"
80 OPEN #4:"DISC:T12"
90 HH=1
95 MM=3
100 CALL MINT(B(.,),7,7,HH)
110 CALL MINT(F(.,),7,1,MM)
120 CALL MTRA(B(.,),D(.,),7,7)
130 CALL MPRD(C(.,),B(.,),C(.,),7,7,7)
140 CALL MPRD(D(.,),C(.,),B(.,),7,7,7)
145 CALL MPRD(E(.,),B(.,),C(.,),7,7,7)
148 CALL MPRD(C(.,),F(.,),B(.,),7,7,1)
150 CALL MADD(A(.,),"+",B(.,),F(.,),7,1)
160 FOR I=1 TO 7
170 A(I,1)=F(I,1)
180 NEXT I
188 HH=HH+1
190 MM=MM+1
191 PRINT HH,MM
195 IF HH=3 THEN GOTO 300
198 IF HH=7 THEN GOTO 500
200 GOTO 100
300 CLOSE #1
310 CLOSE #2
320 CLOSE #3
330 CLOSE #4
340 OPEN #5:"DISC:T3"
350 OPEN #6:"DISC:T4"
360 OPEN #7:"DISC:T13"
370 OPEN #8:"DISC:T14"
390 HH=5
395 MM=7
399 GOTO 100
500 CLOSE #5
510 CLOSE #6
520 CLOSE #7
530 CLOSE #8
600 OPEN #9:"DISC:TE"
610 CALL MINT(E(.,),7,1)
650 CLOSE #9
700 END
6130 SUB MINT(X(.,),F,C)
6140 TA=INT(RO/6)
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6170 PRINT #9:X(I,J)
6175 PRINT AT (I+1,(J-1)*TA) USING #9:X(I,J)
6180 IMAGE ##,###~~~~~
6190 NEXT J::NEXT I
    
```

$$\tau_i = \underset{\sim}{\varphi}(i) \underset{\sim}{\gamma}(i)$$

$$TUI = \underset{\sim}{\rho}(i) \underset{\sim}{\Omega}(i)$$

Modificaciones para integrar T seg:

- 1) $T_i = \varphi\left(\frac{T}{4}\right) \gamma\left(\frac{T}{4}\right)$
- 2) $TUI = \rho\left(\frac{T}{4}\right) \Omega\left(\frac{T}{4}\right)$

3) AÑADIR:

$$535: E = E \cdot \frac{T}{4}$$

(T=4seg)

$$E = T_1^T Q T U_1 + T_2^T Q T U_2 + \dots + T_4^T Q T U_4$$

SIMP

Ejemplo de adecuación de "MATQ" al cálculo de $\hat{M}_i(T)$ [ecuación [63.6] y [62.12]]

$$\underset{\sim}{W}(T) = \int_0^T \left[\underset{\sim}{\varphi}(t-\tau) \underset{\sim}{\gamma}(t-\kappa T + \tau) \underset{\sim}{Q} \underset{\sim}{\rho}(t-\kappa T + \tau) \underset{\sim}{\Omega}(t-\tau) \right] d\tau$$


```

6200 SUBR END
6210 SUB MINT(X(,),F,C,LI)
6220 PRINT FRASE ALI
6230 TA=INT(80/C)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT #1:Y(T,,I)
6270 NEXT J::NEXT I
6280 SUBR END
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(T,,I)=0
6330 FOR K=1 TO XY
6340 Z(T,,I)=Z(T,,I)+X(T,K)*Y(K,,I)
6350 NEXT K::NEXT I::NEXT J
6360 SUBR END
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(T,,J)=X(I,I,T)
6410 NEXT J::NEXT I
6420 SUBR END
6430 SUB MADD(X(,),X$,Y(,),Z(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(T,,I)=X(T,,I)+Y(T,,I)
6470 IF X$="-" THEN Z(T,,I)=X(T,,I)-Y(T,,I)
6480 NEXT J::NEXT I
6490 SUBR END
6500 SUB MZER(X(,),F,C)
6510 FOR I=1 TO F
6520 FOR J=1 TO C
6530 X(T,,I)=0.0
6540 NEXT J::NEXT I
6550 SUBR END
6560 SUB MIND(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(T,,I)=0.0
6600 IF I=J THEN X(T,,I)=0.5
6610 NEXT J::NEXT I
6620 SUBR END
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(T,,I)=A*X(T,,I)
6670 NEXT J::NEXT I
6680 SUBR END

```

```

10 DIM Q(7,7),R(7,1),XT(1,7),A(7,7),ST(7,7),Y(7,7)
12 DIM OR(7,7),WR(7,1)
20 DIM C(7,7),D(7,1),W(7,7),F(7,7),NT(7,7)
30 DIM RR(7,7),TW(7,1)
40 PRINT FRASE ALL
50 PRINT "ORDRE DEL SISTEMA"
60 INPUT Z
70 PRINT "MAT A"
80 CALL MINT(A(,),7,7) ↓ A(t)
90 PRINT FRASE ALL
100 PRINT "MAT B"
110 CALL MINT(B(,),7,1) ↓ B(t)
115 PRINT FRASE ALL
120 PRINT "MAT Q"
135 CALL MINT(Q(,),7,7) ↓ Q(t)
140 PRINT FRASE ALL
145 PRINT "N. ITERACIONES"
150 INPUT N
170 PRINT "T="
180 INPUT T ↓ T
190 CALL MTRA(A(,),ST(,),7,7)
200 CALL MTRA(R(,),XT(,),7,1)
210 CALL MPRC(T,Q(,),Y(,),7,7)
220 CALL MPRC(D(,),R(,),C(,),7,7,1)
230 V=T*T/2
240 CALL MPRC(V,C(,),D(,),7,1)
250 CALL MPRC(XT(,),C(,),W(,),1,7,1)
260 RV=W(1,1)*T*T*T/3
270 FOR II=1 TO 7
280 FOR JJ=1 TO 7
290 RR(II,JJ)=Y(II,JJ)
300 NEXT JJ
310 TW(II,1)=D(II,1)
320 NEXT II
330 K=0
340 M=T/(K+2)
350 CALL MPRC(M,ST(,),C(,),7,7)
360 CALL MPRC(M,A(,),D(,),7,7)
370 CALL MPRC(C(,),Y(,),W(,),7,7,7)
380 CALL MPRC(Y(,),D(,),F(,),7,7,7)
390 CALL MADD(W(,),"+",F(,),Y(,),7,7)
400 CALL MADD(RR(,),"+",Y(,),OR(,),7,7)
402 FOR II=1 TO 7
404 FOR JJ=1 TO 7
406 RR(II,JJ)=OR(II,JJ)
408 NEXT JJ: NEXT II
410 M=T/(K+3)
420 CALL MPRC(M,ST(,),C(,),7,7)
430 CALL MPRC(M,R(,),D(,),7,1)
440 CALL MPRC(C(,),D(,),W(,),7,7,1)
450 CALL MPRC(Y(,),D(,),F(,),7,7,1)
460 CALL MADD(W(,),"+",F(,),D(,),7,1)
470 CALL MADD(TW(,),"+",D(,),WR(,),7,1)
472 FOR II=1 TO 7
474 TW(II,1)=WR(II,1)

```

MATPES

Cálculo de $\hat{Q}(T)$, $V(T)$ y $\hat{R}(T)$ de la ecuación [63.6] a partir del desarrollo de Taylor (hasta el 4º término) de $\Phi(T)$.

- Desarrollo de $\Phi(T)$ como en "TRAD"
- Integración por el método de Simpson.

```

474 NEXT I
480 CALL MTRA(N(,),NT(,),Z,1)
490 M=T/(K+4)
500 CALL MPRC(M,XT(,),C(,),1,7)
510 CALL MPRC(M,R(,),Q(,),Z,1)
520 CALL MPRD(C(,),N(,),W(,),1,7,1)
530 CALL MPRD(NT(,),Q(,),F(,),1,Z,1)
540 R=W(1,1)+F(1,1)
550 RV=RV+R
560 PRINT RV,0 → V(T)/T
570 OPEN #1:"DISC2:PFS0"
580 OPEN #2:"DISC2:PFSW"
590 CALL MOUT(TW(,),Z,1,2) → R̂(T)/T
610 PRINT FRASE ALL
615 CALL MOUT(RQ(,),Z,Z,1) → Q̂(T)/T
620 CLOSE #1
630 CLOSE #2
640 N=N-1
650 K=K+1
660 IF N=0 THEN GOTO 680
670 GOTO 340
680 BRK
690 GOTO 130
6130 SUB MOUT(X(,),F,C,LL)
6140 TA=INT(80/C)
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6170 PRINT AT (I+2,(J-1)*TA) USING A180:X(I,,J)
6175 PRINT #11 USING A180:X(I,,J)
6180 IMAGE ##,###^####
6190 NEXT J::NEXT I
6200 SUBEND
6210 SUB MINT(X(,),F,C)
6220 REM PRINT FRASE ALL
6230 TA=INT(80/C)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT AT (I+2,(J-1)*TA):X(I,,J)
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(I,,J)=0
6330 FOR K=1 TO XY
6340 Z(I,,J)=Z(I,,J)+X(I,K)*Y(K,J)
6350 NEXT K::NEXT I::NEXT J
6360 SUBEND
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(I,,J)=X(I,,I)
6410 NEXT J::NEXT I
6420 SUBEND
6430 SUB MADD(X(,),X$,Y(,),Z(,),F,C)

```

```
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(I,J)=X(I,J)+Y(I,J)
6470 IF X$="-" THEN Z(I,J)=X(I,J)-Y(I,J)
6480 NEXT J::NEXT I
6490 SUBEND
6500 SUB MZER(X(,),F,C)
6510 FOR I=1 TO F
6520 FOR J=1 TO C
6530 X(I,J)=0.0
6540 NEXT J::NEXT I
6550 SUBEND
6560 SUB MINO(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(I,J)=0.0
6600 IF I=J THEN X(I,J)=1.0
6610 NEXT J::NEXT I
6620 SUBEND
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,J)=A*X(I,J)
6670 NEXT J::NEXT I
6680 SUBEND
```

```

10 DIM A(7,7),R(7,7),C(7,7),D(7,7),I(7,7),P(7,7),W(7,7),Z(7,7)
11 DIM ZT(7,7),WT(7,7),F(7,7)
12 PRINT ERASE ALL
13 DIM D(7,7)
15 Y=7

```

ORDEN DEL SISTEMA

```

20 PRINT "N ITERACIONES"
30 INPUT H
31 PRINT ERASE ALL
33 PRINT "COND. INICIALES"
34 TA=INT(80/Y)
35 FOR U=1 TO Y
40 FOR J=1 TO Y
45 INPUT AT (U+2, (J-1)*TA):P(U,J)
50 NEXT J:NEXT U

```

Valores iniciales de la matriz de Riccati P(KT)

```

60 OPEN #1:"DISC2:TRAB"
70 OPEN #2:"DISC2:TRAB"
80 CALL MINT(W(,),Y,Y,1)
90 CALL MINT(Z(,),Y,1,2)

```

$\Phi(KT)$

$\Theta(KT)$

```

100 CLOSE #1
105 CLOSE #2
110 CALL MPRD(P(,),Z(,),A(,),Y,Y,1)
120 CALL MPRD(P(,),W(,),R(,),Y,Y,Y)
130 CALL MTRA(Z(,),ZT(,),Y,1)
140 CALL MTRA(W(,),WT(,),Y,Y)
150 CALL MPRD(ZT(,),A(,),C(,),1,Y,1)
155 CALL M7ER(D(,),Y,Y)
160 CALL MPRD(WT(,),A(,),D(,),Y,Y,1)
170 CALL MTRA(D(,),ZT(,),Y,1)
180 CALL MPRD(WT(,),B(,),F(,),Y,Y,Y)

```

Definición de R

```

190 D=C(1,1)+1
200 M=1/D
205 CALL M7ER(R(,),Y,Y)
210 CALL MPRD(M,ZT(,),R(,),1,Y)
215 CALL M7ER(A(,),Y,Y)
220 CALL MPRD(D(,),R(,),A(,),Y,1,Y)
230 CALL MADD(F(,),"-",A(,),D(,),Y,Y)
240 CALL MIND(I(,),Y)

```

Definición de Q

```

245 I(5,5)=1
250 CALL MADD(I(,),"+",D(,),P(,),Y,Y)
255 FOR U=1 TO Y
256 FOR J=U TO Y
257 P(U,J)=(P(U,J)+P(J,U))/2
258 NEXT J:NEXT U
260 FOR U=1 TO Y
261 FOR J=U TO Y
262 P(U,J)=P(U,J)
263 NEXT J:NEXT U
269 IF H=0 THEN GOTO 500
270 H=H-1
280 PRINT ERASE ALL
290 PRINT H
291 TA=INT(80/Y)
292 FOR U=1 TO Y
293 FOR J=1 TO Y

```

Compensación de los defectos de simetría de P(KT) por truncamientos y redondeos.

```

294 PRINT AT(U+2, (J-1)*TA) USING 295:P(U,J)

```

$\tilde{P}(KT)$

RTRT

Resolución de la ecuación de Riccati [62.18].

```

295 IMAGE ##.###^^^
296 NEXT J::NEXT I
300 CALL MZER(D(,),Y,Y)
302 CALL MZER(A(,),Y,Y)
303 CALL MZER(B(,),Y,Y)
304 CALL MZER(ZT(,),Y,Y)
305 CALL MZER(WT(,),Y,Y)
306 CALL MZER(C(,),Y,Y)
307 CALL MZER(F(,),Y,Y)
308 CALL MZER(I(,),Y,Y)
499 GOTO 110
500 OPEN #4:"DISC2:TR11"
501 CALL MOUT(B(,),1,Y,4)
505 CLOSE #4
541 END
6130 SUB MOUT(X(,),F,C,LT)
6140 TA=INT(RO/C)
6145 PRINT FRASE ALL
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6170 PRINT AT (I+2,(J-1)*TA) USING 6180:X(I,J)
6180 IMAGE ##.###^^^
6187 PRINT #LT:X(I,J)
6190 NEXT J::NEXT I
6200 SUBEND
6210 SUB MINT(X(,),F,C,LT)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT #LT:X(I,J)
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(I,J)=0
6330 FOR K=1 TO XY
6340 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
6350 NEXT K::NEXT I::NEXT J
6360 SUBEND
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(I,J)=X(I,I)
6410 NEXT J::NEXT I
6420 SUBEND
6430 SUB MADD(X(,),X$,Y(,),Z(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(I,J)=X(I,J)+Y(I,J)
6470 IF X$="-" THEN Z(I,J)=X(I,J)-Y(I,J)
6480 NEXT J::NEXT I
6490 SUBEND
6500 SUB MZER(X(,),F,C)
6510 FOR I=1 TO F
6520 FOR J=1 TO C

```

```
6530 X(I,J)=0
6540 NEXT J::NEXT I
6550 SUBEND
6560 SUB MIND(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(I,J)=0.0
6600 IF I=J THEN X(I,J)=0.5
6610 NEXT J::NEXT I
6620 SUBEND
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,J)=A*X(I,J)
6670 NEXT J::NEXT I
6680 SUBEND
```

```

1 REM *** A 60 I 70 HI HA FLS FITXERS D'ENTRADA. A 500 FI DE SORTIDA ***
10 DIM A(7,7),R(7,7),C(7,7),Q(7,7),I(7,7),P(7,7),W(7,7),Z(7,7)
11 DIM ZT(7,7),WT(7,7),F(7,7),NT(1,7),M(1,7)
12 PRINT FRASE ALL
13 DIM D(7,7)
15 Y=7
20 PRINT "N ITERACIONS"
30 INPUT H
31 PRINT FRASE ALL
33 PRINT "COND. INITIALS"
34 TA=INT(80/Y)
35 FOR II=1 TO Y
40 FOR .I=1 TO Y
45 INPUT AT ((II+2,.(I-1)*TA):P(II,.I)
50 NEXT .I::NEXT II
51 PRINT FRASE ALL "MAT Q"
53 FOR II=1 TO Y
54 FOR .I=1 TO Y
55 INPUT AT ((II+2,.(I-1)*TA):I(II,.I)
56 NEXT .I::NEXT II
57 PRINT FRASE ALL "MAT M"
59 FOR II=1 TO Y
60 INPUT AT ((II+2,0):M(1,II)
61 NEXT II
65 OPEN #1:"DISC:TR"
70 OPEN #2:"DISC:TH4"
80 CALL MINT(W(.),Y,Y,1) —  $\Phi(T)$ 
90 CALL MINT(Z(.),Y,1,2) —  $\Theta(T)$ 
100 CLOSE #1
105 CLOSE #2
110 CALL MPRD(P(.),Z(.),A(.),Y,Y,1)
120 CALL MPRD(P(.),W(.),R(.),Y,Y,Y)
130 CALL MTRA(Z(.),ZT(.),Y,1)
140 CALL MTRA(W(.),WT(.),Y,Y)
150 CALL MPRD(ZT(.),A(.),C(.),1,Y,1)
155 CALL MZER(D(.),Y,Y)
160 CALL MPRD(WT(.),A(.),D(.),Y,Y,1)
170 CALL MTRA(D(.),NT(.),Y,1)
175 CALL MADD(NT(.),"+",M(.),ZT(.),1,Y)
180 CALL MPRD(WT(.),R(.),F(.),Y,Y,Y)
190 D=C(1,1)+1.4673
200 VV=1/D
205 CALL MZER(R(.),Y,Y)
210 CALL MPRD(VV,ZT(.),R(.),1,Y)
215 CALL MZER(A(.),Y,Y)
220 CALL MPRD(D(.),R(.),A(.),Y,1,Y)
230 CALL MADD(F(.),"-",A(.),D(.),Y,Y)
250 CALL MADD(I(.),"+",D(.),P(.),Y,Y)
255 FOR II=1 TO Y
256 FOR .I=1 TO Y
257 P(II,.I)=(P(II,.I)+P(.I,II))/2
258 NEXT .I::NEXT II
260 FOR II=1 TO Y
261 FOR .I=1 TO Y
262 P(.I,II)=P(II,.I)

```

orden del sistema

$P(0)$

Q

Entrada de la matriz $M(T)$.

$\Phi(T)$

$\Theta(T)$

Definición de R

RTR2

Ampliación de "RTRT" para que también soporte la resolución de la ecuación de Riccati [62.16].


```

263 NEXT .I::NEXT I1
269 IF H=0 THEN GOTO 500
270 H=H-1
280 PRINT FRASE ALL
290 PRINT H
291 TA=INT(80/Y)
292 FOR I1=1 TO Y
293 FOR .I=1 TO Y
294 PRINT AT(I1+2,(.I-1)*TA) USING 295:P(I1,.I)
295 IMAGE ##.###^
296 NEXT .I::NEXT I1
300 CALL MZER(D(,),Y,Y)
302 CALL MZER(A(,),Y,Y)
303 CALL MZER(B(,),Y,Y)
304 CALL MZER(7T(,),Y,Y)
305 CALL MZER(WT(,),Y,Y)
306 CALL MZER(C(,),Y,Y)
307 CALL MZER(F(,),Y,Y)
499 GOTO 110
500 OPEN #4:"DSC:TF"
501 CALL MOUT(R(,),1,Y,4)
505 CLOSE #4
541 END
6130 SUB MOUT(X(,),F,C,I,T)
6140 TA=INT(80/C)
6145 PRINT FRASE ALL
6150 FOR I=1 TO F
6160 FOR .I=1 TO C
6170 PRINT AT (I+2,(.I-1)*TA) USING 6180:X(I,.I)
6180 IMAGE ##.###^
6187 PRINT #I T:X(I,.I)
6190 NEXT .I::NEXT I
6200 SUBEND
6210 SUB MTNT(X(,),F,C,I,T)
6240 FOR I=1 TO F
6250 FOR .I=1 TO C
6260 INPUT #I T:X(I,.I)
6270 NEXT .I::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),7(,),FX,XY,CY)
6300 FOR .I=1 TO CY
6310 FOR I=1 TO FX
6320 7(I,.I)=0
6330 FOR K=1 TO XY
6340 7(I,.I)=7(I,.I)+X(I,K)*Y(K,.I)
6350 NEXT K::NEXT I::NEXT .I
6360 SUBEND
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR .I=1 TO F
6400 XT(I,.I)=X(.I,I)
6410 NEXT .I::NEXT I
6420 SUBEND
6430 SUB MADD(X(,),X$,Y(,),7(,),F,C)
6440 FOR I=1 TO F

```

```
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(I,,J)=X(I,,J)+Y(I,,J)
6470 IF X$="-" THEN Z(I,,J)=X(I,,J)-Y(I,,J)
6480 NEXT J::NEXT I
6490 SUREND
6500 SUB MZER(X(,),F,C)
6510 FOR I=1 TO F
6520 FOR J=1 TO C
6530 X(I,,J)=0
6540 NEXT J::NEXT I
6550 SUREND
6560 SUB MINN(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(I,,J)=0.0
6600 IF I=J THEN X(I,,J)=0.5
6610 NEXT J::NEXT I
6620 SUREND
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,,J)=A*X(I,,J)
6670 NEXT J::NEXT I
6680 SUREND
```

```

10 DIM T1(7,7),T2(7,1),F(7,7),FT(7,7),TT(1,7),TR(1,7)
11 DIM TP(1,7),KII(7,1),OM(7,1)
12 DIM P(7,7),W(7,1),Z(7,7),C(7,7)
14 DIM M(1,1),S(7,1),A(7,1),F(7,1),N(1,1)
15 Y=7
16 MR=.000489
17 PRINT FRASE ALL
18 R=1.088
19 V=.4673
20 PRINT "N DE ITERAC."
22 INPUT H
24 PRINT "COND. INIC."
26 TA=INT(80/Y)
28 FOR I=1 TO Y
30 FOR J=1 TO Y
32 INPUT AT (I+2,(J-1)*TA):P(J,I)
34 NEXT J:NEXT I
35 FOR I=1 TO Y
36 READ KII(I,1)
37 NEXT I
38 DATA 2.164,-.1069,.236,.07336,.428,-.007295,.003036
40 FOR I=1 TO Y
41 READ OM(I,1)
42 NEXT I
43 DATA -.2114,.04375,-.01793,-.00605,.0339,.0167,-.0034
45 OPEN #1:"DISC:T8"
46 OPEN #2:"DISC:P1"
47 OPEN #3:"DISC:TIH4"
48 CALL MINT(F(,),Y,Y,1)
49 CALL MINT(T1(,),Y,1,2)
50 CALL MINT(T2(,),Y,1,3)
51 CLOSE #1
52 CLOSE #2
53 CLOSE #3
54 CALL MTRA(F(,),FT(,),Y,Y)
55 CALL MTRA(T1(,),TT(,),Y,1)
56 CALL MTRA(T2(,),TR(,),Y,1)
57 CALL MPRD(P(,),T2(,),W(,),Y,Y,1)
58 CALL MPRD(TR(,),W(,),M(,),1,Y,1)
59 G=M(1,1)+V
60 R=1/G
61 CALL MPRD(P(,),F(,),Z(,),Y,Y,Y)
62 CALL MPRD(P(,),T1(,),S(,),Y,Y,1)
63 CALL MPRD(FT(,),W(,),A(,),Y,Y,1)
64 CALL MPRD(FT(,),Z(,),C(,),Y,Y,Y)
65 CALL MPRD(FT(,),S(,),F(,),Y,Y,1)
66 CALL MPRD(TR(,),S(,),N(,),1,Y,1)
67 N(1,1)=N(1,1)+MR
68 CALL MPRD(TT(,),S(,),F(,),1,Y,1)
69 RT=R+F(1,1)-N(1,1)*R*N(1,1)
70 RT=1/RT
71 MI=R*N(1,1)
72 CALL MAOP(A(,),"+",OM(,),Z(,),Y,1)
73 CALL MAOP(F(,),"+",KII(,),A(,),Y,1)
74 CALL MPRD(MI,Z(,),W(,),Y,1)

```

orden del sistema

$M_3(CT)$

$R(T)$

$V(T)$

$P(O)$

$M_1(CT)$

$M_2(CT)$

Φ_1

Θ_1

Θ_2

MULTC

Resolución de la nueva ecuación de Riccati [63.28].

(para sistemas con una entrada de control).

y de las leyes de control [63.26] y [63.27].

```

180 CALL MADD(W(.), "-", A(.), S(.), Y, 1)
185 CALL MTRA(S(.), TT(.), Y, 1)
190 CALL MPRC(RI, TT(.), TR(.), 1, Y)
200 CALL MPRD(S(.), TR(.), F(.), Y, 1, Y)
205 CALL MTRA(Z(.), TT(.), Y, 1)
210 CALL MPRC(R, TT(.), TP(.), 1, Y)
220 CALL MPRD(Z(.), TP(.), T1(.), Y, 1, Y)
230 CALL MADD(F(.), "+", T1(.), Z(.), Y, Y)
240 FOR I=1 TO Y
241 FOR J=1 TO Y
242 READ F(I, J)
243 NEXT J::NEXT I
244 DATA 110, -5.72, 15.26, 4.51, 21, -1.01, 1.4, -5.72, .6647, -.375, -.12, -.61
245 DATA .0005, -.018, 15.26, -.375, 3.7462, 1.168, 4.079, -1., .373, 4.51, -.12
246 DATA 1.168, .529, 1.44, -.054, -.046, 21, -.61, 4.079, 1.44, 8, -.046, .088
247 DATA -1.01, .0005, -1, -.054, -.046, 1.8452, -.245, 1.4, -.018, .373, -.046
248 DATA .088, -.245, .2481
249 RESTORE 244
250 CALL MADD(F(.), "+", C(.), FT(.), Y, Y)
260 CALL MADD(FT(.), "-", Z(.), P(.), Y, Y)
270 FOR J=1 TO Y
280 FOR I=1 TO Y
290 P(I, J)=(P(I, I)+P(J, I))/2
295 P(J, I)=P(I, J)
300 NEXT I::NEXT J
310 IF H=0 THEN GOTO 1000
320 H=H-1
330 PRINT FRASE ALL
340 PRINT H
350 FOR I=1 TO Y
360 FOR J=1 TO Y
370 PRINT AT (I+2, (J-1)*TA) USING 380:P(I, J) —————→ P(KT)
380 IMAGE ##.###^
400 NEXT J::NEXT I
500 GOTO 50
1000 OPEN #9:"DSC:FTN"
1001 PRINT FRASE ALL
1010 CALL MOU(TR(.), 1, Y, 9) —————→ u(KT)
1020 CLOSE #9
1050 BRK
1060 CALL MPRD(T(.), TR(.), T1(.), 1, 1, Y)
1070 CALL MADD(T1(.), "+", TT(.), TR(.), 1, Y)
1080 CALL MPRC(R, TR(.), T1(.), 1, Y)
1090 OPEN #8:"DSC:FTAN"
1100 CALL MOU(T1(.), 1, Y, 8) —————→ u(KT+z)
1200 CLOSE #8
1300 END
6130 SUB MOU(X(.), F, C, I)
6140 TA=INT(80/C)
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6165 PRINT #I: X(I, J)
6170 PRINT AT (I+2, (J-1)*TA) USING 6180:X(I, J)
6180 IMAGE ##.###^
6190 NEXT J::NEXT I

```

QCT

```

6200 SUBEND
6210 SUB MINT(X(.),F,C,LI)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPUT #1: X(I,J)
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(.),Y(.),Z(.),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(I,J)=0
6330 FOR K=1 TO XY
6340 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
6350 NEXT K::NEXT I::NEXT J
6360 SUBEND
6370 SUB MTRA(X(.),XT(.),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(I,J)=X(I,I)
6410 NEXT J::NEXT I
6420 SUBEND
6430 SUB MADD(X(.),X$,Y(.),Z(.),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(I,J)=X(I,J)+Y(I,J)
6470 IF X$="-" THEN Z(I,J)=X(I,J)-Y(I,J)
6480 NEXT J::NEXT I
6490 SUBEND
6540 SUB MIND(X(.),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(I,J)=0.0
6600 IF I=J THEN X(I,J)=0.5
6610 NEXT J::NEXT I
6620 SUBEND
6630 SUB MPRC(A,X(.),Z(.),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,J)=A*X(I,J)
6670 NEXT J::NEXT I
6680 SUBEND

```

```

10 DIM T1(7,7),T2(7,1),F(7,7),FT(7,7),TT(1,7),TR(1,7)
11 DIM TP(1,7)
12 DIM P(7,7),W(7,1),Z(7,7),C(7,7)
14 DIM M(1,1),S(7,1),A(7,1),F(7,1),D(1,1)
15 Y=7
17 PRINT ERASE ALL
18 R=1
19 V=1
20 PRINT "N D'ITERAC."
22 INPUT H
24 PRINT "COND. INIC."
26 TA=INT(80/Y)
28 FOR J=1 TO Y
30 FOR I=1 TO Y
32 INPUT AT (I+2,(J-1)*TA):P(I,J)
34 NEXT J::NEXT I
50 OPEN #1:"DISC:TRB1"
55 OPEN #2:"DISC:TRC1"
60 OPEN #3:"DISC2:TRA2"
70 CALL MINT(F(,),Y,Y,1)
75 CALL MINT(T1(,),Y,1,2)
80 CALL MINT(T2(,),Y,1,3)
85 CLOSE #1
86 CLOSE #2
87 CLOSE #3
90 CALL MTRA(F(,),FT(,),Y,Y)
95 CALL MTRA(T1(,),TT(,),Y,1)
100 CALL MTRA(T2(,),TR(,),Y,1)
105 CALL MPRD(P(,),T2(,),W(,),Y,Y,1)
110 CALL MPRD(TR(,),W(,),M(,),1,Y,1)
115 G=M(1,1)+V
120 R=1/G
125 CALL MPRD(P(,),F(,),Z(,),Y,Y,Y)
130 CALL MPRD(P(,),T1(,),S(,),Y,Y,1)
135 CALL MPRD(FT(,),W(,),A(,),Y,Y,1)
140 CALL MPRD(FT(,),Z(,),C(,),Y,Y,Y)
145 CALL MPRD(FT(,),S(,),F(,),Y,Y,1)
150 CALL MPRD(TR(,),S(,),D(,),1,Y,1)
155 CALL MPRD(TT(,),S(,),F(,),1,Y,1)
160 RT=R+F(1,1)-D(1,1)*R*D(1,1)
165 RT=1/RT
170 MI=R*D(1,1)
175 CALL MPRC(MI,A(,),W(,),Y,1)
180 CALL MADD(W(,),"-",E(,),S(,),Y,1)
185 CALL MTRA(S(,),TT(,),Y,1)
190 CALL MPRC(RT,TT(,),TR(,),1,Y)
200 CALL MPRD(S(,),TR(,),F(,),Y,1,Y)
205 CALL MTRA(A(,),TT(,),Y,1)
210 CALL MPRC(R,TT(,),TP(,),1,Y)
220 CALL MPRD(A(,),TP(,),T1(,),Y,1,Y)
230 CALL MADD(F(,),"+",T1(,),Z(,),Y,Y)
240 CALL MINT(F(,),Y)
245 F(5,5)=1
250 CALL MADD(F(,),"+",C(,),FT(,),Y,Y)
260 CALL MADD(FT(,),"-",Z(,),P(,),Y,Y)

```

orden del sistema

Fijación de R y V.

P(0)

Φ , θ_1 , θ_2

Definición de $\hat{Q}(T)$

MULTR

Particularización de "MULTC" al criterio integral [63.10] (Penalización de las desviaciones sólo en los instantes de muestreo).

```

270 FOR I=1 TO Y
280 FOR J=1 TO Y
290 P(I,J)=(P(J,J)+P(J,I))/2
295 P(J,I)=P(I,J)
300 NEXT J::NEXT I
310 IF H=0 THEN GOTO 1000
320 H=H-1
330 PRINT FRASE ALL
340 PRINT H
350 FOR I=1 TO Y
360 FOR J=1 TO Y
370 PRINT AT (I+2,(J-1)*TA) USING 380:P(I,J) → P(KT)
380 IMAGE ##.###^
400 NEXT J::NEXT I
500 GOTO 50
1000 OPEN #9:"DSC:FIN"
1001 PRINT FRASE ALL
1010 CALL MOUT(TR(,),1,Y,9) → μ(KT)
1020 CLOSE #9
1050 BRK
1060 CALL MPRD(D(,),TR(,),T1(,),1,1,Y)
1070 CALL MADD(T1(,),"+",TT(,),TR(,),1,Y)
1080 CALL MPRD(R,TR(,),T1(,),1,Y)
1090 OPEN #8:"DSC:FTALL"
1100 CALL MOUT(T1(,),1,Y,8) → μ(KT+z)
1200 CLOSE #8
1300 END
6130 SUB MOUT(X(,),F,C,LL)
6140 TA=INT(80/C)
6150 FOR I=1 TO F
6160 FOR J=1 TO C
6165 PRINT #11:X(I,J)
6170 PRINT AT (I+2,(J-1)*TA) USING 6180:X(I,J)
6180 IMAGE ##.###^
6190 NEXT J::NEXT I
6200 SUBEND
6210 SUB MINT(X(,),F,C,LL)
6240 FOR I=1 TO F
6250 FOR J=1 TO C
6260 INPLT #11:X(I,J)
6270 NEXT J::NEXT I
6280 SUBEND
6290 SUB MPRD(X(,),Y(,),Z(,),FX,XY,CY)
6300 FOR J=1 TO CY
6310 FOR I=1 TO FX
6320 Z(I,J)=0
6330 FOR K=1 TO XY
6340 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)
6350 NEXT K::NEXT I::NEXT J
6360 SUBEND
6370 SUB MTRA(X(,),XT(,),F,C)
6380 FOR I=1 TO C
6390 FOR J=1 TO F
6400 XT(I,J)=X(I,I)
6410 NEXT J::NEXT I

```

```
6420 SUBEND
6430 SUB MADD(X(,),X$,Y(,),Z(,),F,C)
6440 FOR I=1 TO F
6450 FOR J=1 TO C
6460 IF X$="+" THEN Z(I,J)=X(I,J)+Y(I,J)
6470 IF X$="-" THEN Z(I,J)=X(I,J)-Y(I,J)
6480 NEXT J::NEXT I
6490 SUBEND
6560 SUB MIND(X(,),N)
6570 FOR I=1 TO N
6580 FOR J=1 TO N
6590 X(I,J)=0.0
6600 IF I=J THEN X(I,J)=0.5
6610 NEXT J::NEXT I
6620 SUBEND
6630 SUB MPRC(A,X(,),Z(,),F,C)
6640 FOR I=1 TO F
6650 FOR J=1 TO C
6660 Z(I,J)=A*X(I,J)
6670 NEXT J::NEXT I
6680 SUBEND
```


APENDICE G :

Resultados de simulación anexos al Capítulo 6.

RESULTADOS DE SIMULACION.

Entrada: Perturbación indicial de 0,01 p.u.MW en el Area 1.

Bloques listados:

20 : Generación del Area 1 (p.u.MW).

24 : Desviaciones frecuencia del Area 1 (Hz).

27 : Intercambio de potencia del Area 1 al Area 2 (p.u.MW).

38 : Generación del Area 2 (p.u.MW).

46 : Integral del ACE del Area 1, $\int ACE_1 dt.$

55 : Integral del error cuadrático de frecuencia del Area 1,

$$\int f_1^2 dt.$$

56 : Integral del error cuadrático del intercambio de potencia

$$\int P_{12}^2 dt.$$

30 : Desviaciones de frecuencia del Area 2 (Hz).

SD1

RLO discreto de acción simple (sin retardo) ajustado con los valores obtenidos en el diseño sobre el modelo continuo (caso ① del Capítulo 5).

T = 8 segundos.

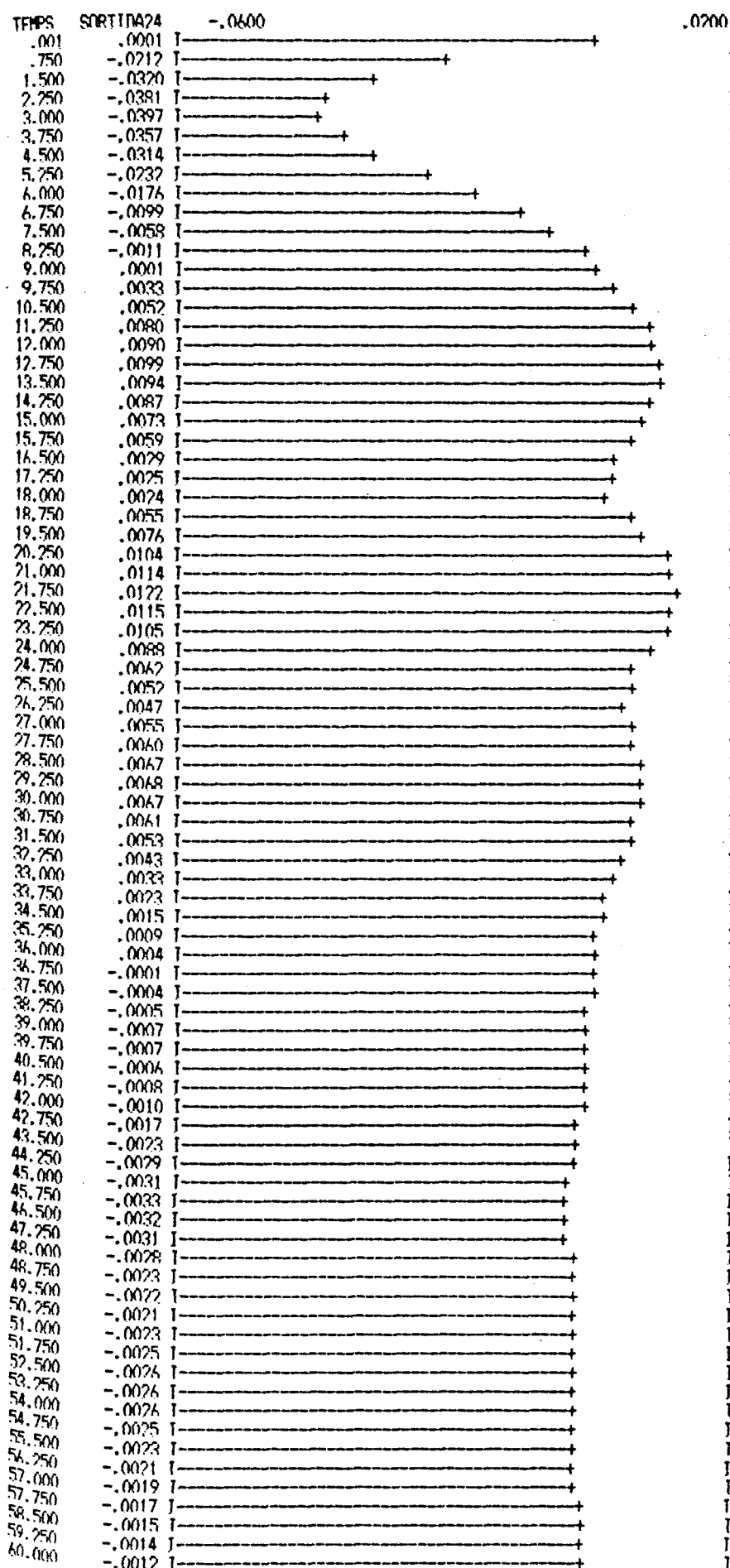
(simulación sin retardo de cálculo).

PLC FTY Y (24) MJNTM (-.1000) MAXTM (.1000)

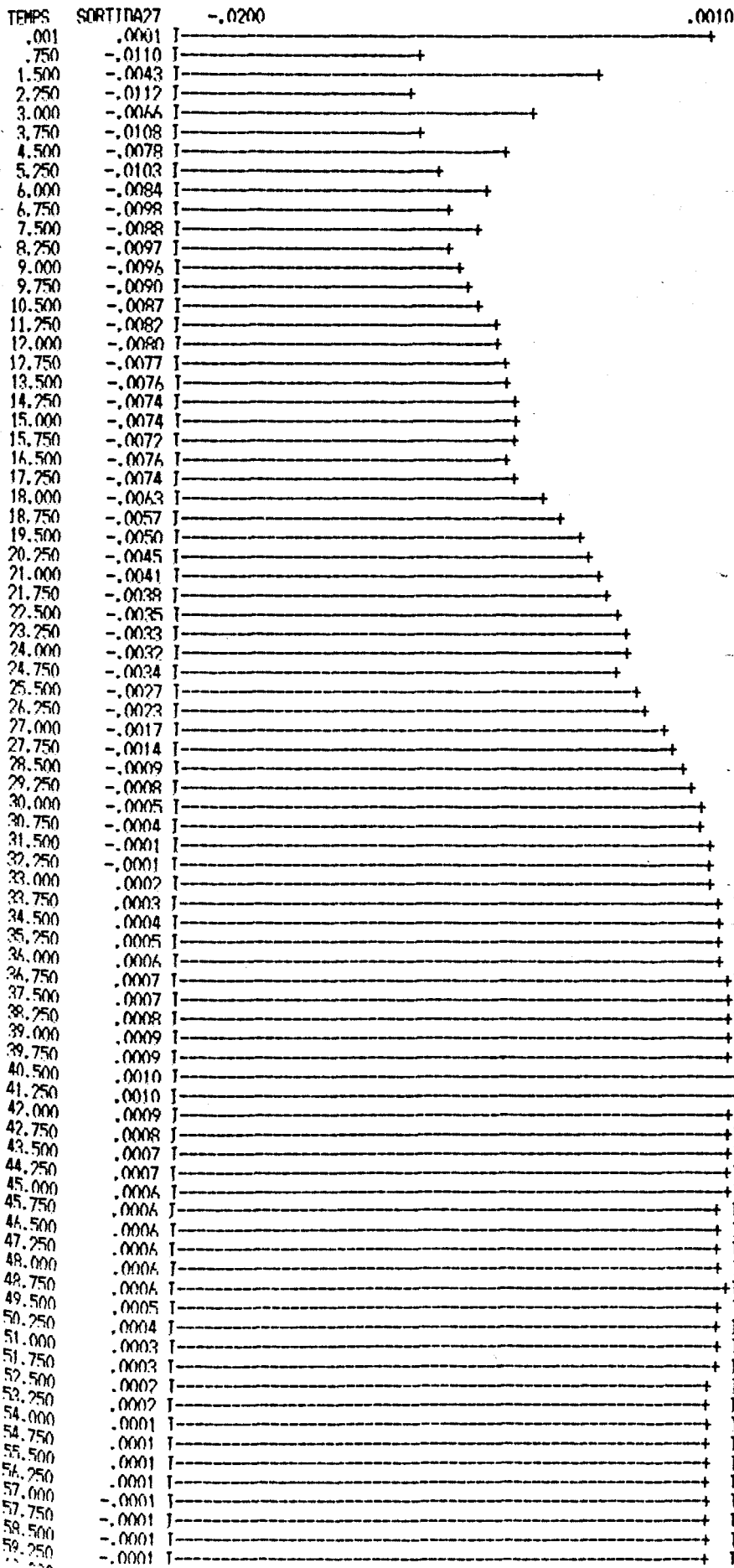
SD1.1

TEMPS	SORTIDA24	-.1000	.1000
.001	.0001	I	I
.750	-.0212	I	I
1.500	-.0320	I	I
2.250	-.0381	I	I
3.000	-.0397	I	I
3.750	-.0357	I	I
4.500	-.0314	I	I
5.250	-.0232	I	I
6.000	-.0176	I	I
6.750	-.0099	I	I
7.500	-.0058	I	I
8.250	-.0011	I	I
9.000	.0001	I	I
9.750	.0033	I	I
10.500	.0052	I	I
11.250	.0080	I	I
12.000	.0090	I	I
12.750	.0099	I	I
13.500	.0094	I	I
14.250	.0087	I	I
15.000	.0073	I	I
15.750	.0059	I	I
16.500	.0029	I	I
17.250	.0025	I	I
18.000	.0024	I	I
18.750	.0055	I	I
19.500	.0076	I	I
20.250	.0104	I	I
21.000	.0114	I	I
21.750	.0122	I	I
22.500	.0115	I	I
23.250	.0105	I	I
24.000	.0088	I	I
24.750	.0062	I	I
25.500	.0052	I	I
26.250	.0047	I	I
27.000	.0055	I	I
27.750	.0060	I	I
28.500	.0067	I	I
29.250	.0068	I	I
30.000	.0067	I	I
30.750	.0061	I	I
31.500	.0053	I	I
32.250	.0043	I	I
33.000	.0033	I	I
33.750	.0023	I	I
34.500	.0015	I	I
35.250	.0009	I	I
36.000	.0004	I	I
36.750	-.0001	I	I
37.500	-.0004	I	I
38.250	-.0005	I	I
39.000	-.0007	I	I
39.750	-.0007	I	I
40.500	-.0006	I	I
41.250	-.0008	I	I
42.000	-.0010	I	I
42.750	-.0017	I	I
43.500	-.0023	I	I
44.250	-.0029	I	I
45.000	-.0031	I	I
45.750	-.0033	I	I
46.500	-.0032	I	I
47.250	-.0031	I	I
48.000	-.0028	I	I
48.750	-.0023	I	I
49.500	-.0022	I	I
50.250	-.0021	I	I
51.000	-.0023	I	I
51.750	-.0025	I	I
52.500	-.0026	I	I
53.250	-.0026	I	I
54.000	-.0026	I	I
54.750	-.0025	I	I
55.500	-.0023	I	I
56.250	-.0021	I	I
57.000	-.0019	I	I
57.750	-.0017	I	I
58.500	-.0015	I	I
59.250	-.0014	I	I
60.000	-.0012	I	I

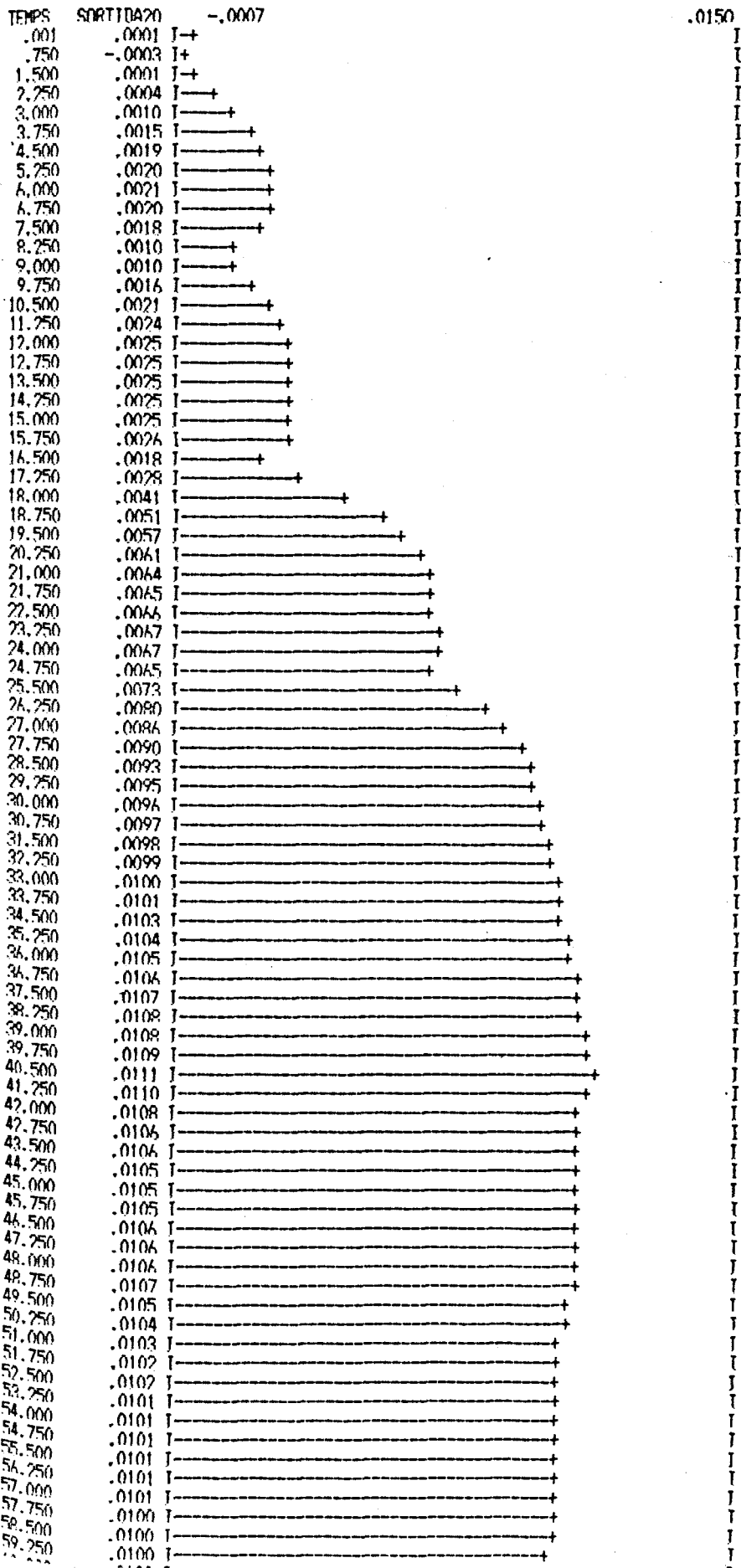
BLDG. FIX V (24) MINIM (-.0600) MAXIM (.0200)

SD1.2

BLOC EIX Y (27) MINIM (-.0200) MAXIM (.0010)

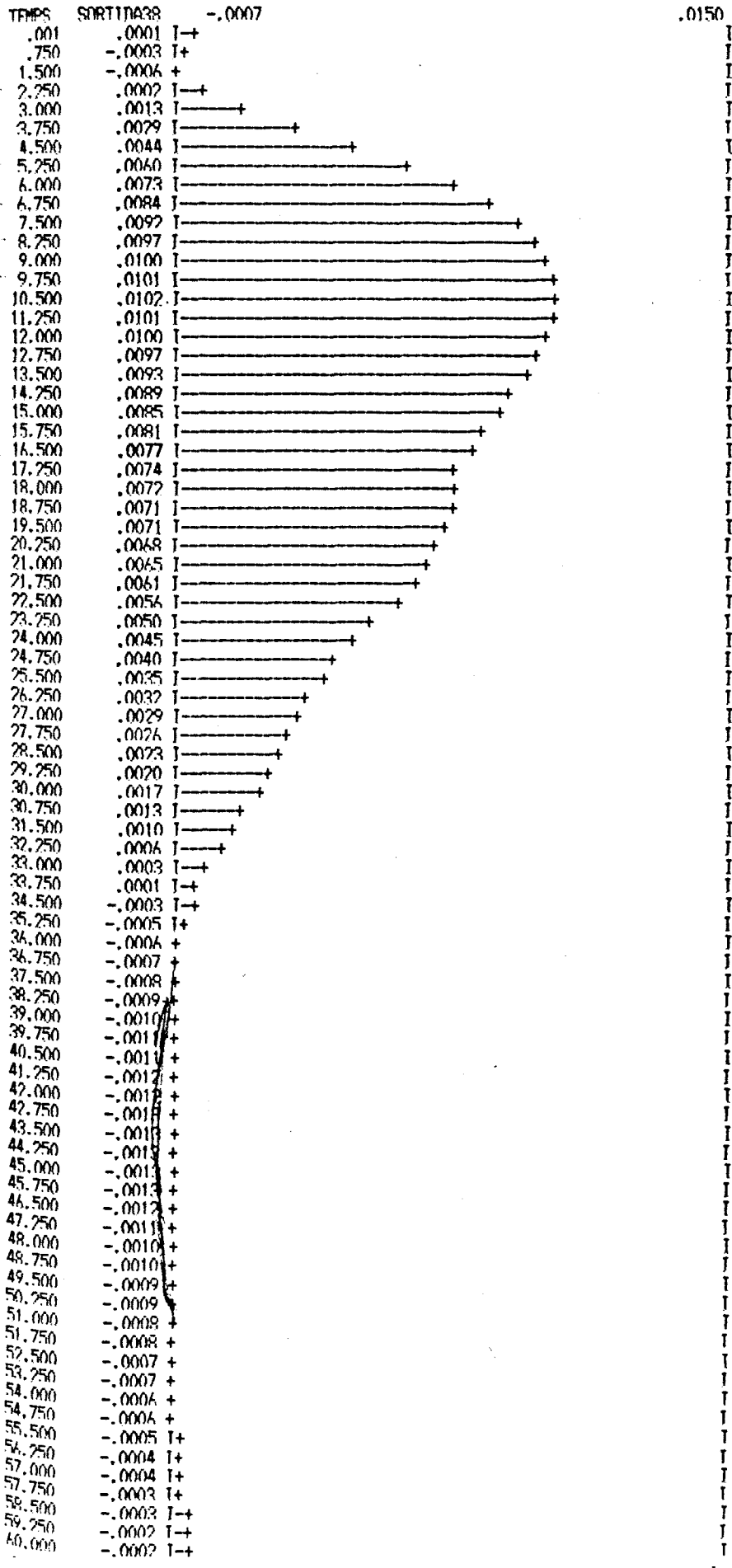


RUC FIX Y (20) MINIM (-.0007) MAXIM (.0150)



NO. FIX V (38) MINIM (-.0007) MAXIM (.0150)

SD1.6



TEMPS	SORTIDA4A	SORTIDA3O	SORTIDA5S	SORTIDA5A
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0453	-.0159	.0057	.0005
8.00	-.0854	-.0074	.0059	.0007
10.00	-.1041	.0034	.0059	.0008
12.00	-.1195	.0091	.0060	.0010
14.00	-.1331	.0088	.0062	.0011
16.00	-.1463	.0053	.0063	.0012
18.00	-.1602	.0025	.0063	.0013
20.00	-.1701	.0089	.0064	.0014
22.00	-.1761	.0117	.0066	.0014
24.00	-.1808	.0088	.0069	.0014
26.00	-.1856	.0045	.0069	.0014
28.00	-.1881	.0060	.0070	.0014
30.00	-.1884	.0064	.0071	.0014
32.00	-.1878	.0045	.0072	.0014
34.00	-.1869	.0019	.0072	.0014
36.00	-.1859	.0003	.0072	.0014
38.00	-.1847	-.0005	.0072	.0014
40.00	-.1837	-.0008	.0072	.0014
42.00	-.1814	-.0011	.0072	.0014
44.00	-.1803	-.0026	.0072	.0014
46.00	-.1796	-.0033	.0072	.0014
48.00	-.1792	-.0028	.0072	.0014
50.00	-.1786	-.0021	.0072	.0014
52.00	-.1784	-.0025	.0073	.0014
54.00	-.1786	-.0026	.0073	.0014
56.00	-.1789	-.0022	.0073	.0014
58.00	-.1793	-.0016	.0073	.0014
60.00	-.1796	-.0012	.0073	.0014
62.00	-.1800	-.0010	.0073	.0014
64.00	-.1805	-.0009	.0073	.0014
66.00	-.1809	-.0008	.0073	.0014
68.00	-.1813	-.0004	.0073	.0014
70.00	-.1814	-.0002	.0073	.0014
72.00	-.1816	-.0002	.0073	.0014
74.00	-.1818	-.0003	.0073	.0014
76.00	-.1819	-.0002	.0073	.0014
78.00	-.1818	-.0001	.0073	.0014
80.00	-.1818	-.0001	.0073	.0014
82.00	-.1817	-.0002	.0073	.0014
84.00	-.1816	-.0003	.0073	.0014
86.00	-.1815	-.0003	.0073	.0014
88.00	-.1815	-.0003	.0073	.0014
90.00	-.1813	-.0003	.0073	.0014
92.00	-.1813	-.0003	.0073	.0014
94.00	-.1812	-.0003	.0073	.0014
96.00	-.1812	-.0003	.0073	.0014
98.00	-.1811	-.0003	.0073	.0014
100.00	-.1811	-.0003	.0073	.0014
102.00	-.1811	-.0003	.0073	.0014
104.00	-.1811	-.0002	.0073	.0014
106.00	-.1811	-.0002	.0073	.0014
108.00	-.1811	-.0002	.0073	.0014
110.00	-.1811	-.0002	.0073	.0014
112.00	-.1811	-.0002	.0073	.0014
114.00	-.1812	-.0001	.0073	.0014
116.00	-.1812	-.0001	.0073	.0014
118.00	-.1812	-.0001	.0073	.0014
120.00	-.1812	-.0001	.0073	.0014
122.00	-.1812	-.0001	.0073	.0014
124.00	-.1812	-.0001	.0073	.0014
126.00	-.1812	-.0001	.0073	.0014
128.00	-.1812	-.0001	.0073	.0014
130.00	-.1812	-.0001	.0073	.0014
132.00	-.1812	-.0001	.0073	.0014
134.00	-.1812	-.0001	.0073	.0014
136.00	-.1812	-.0001	.0073	.0014
138.00	-.1812	-.0001	.0073	.0014
140.00	-.1812	-.0001	.0073	.0014
142.00	-.1812	-.0001	.0073	.0014
144.00	-.1812	-.0001	.0073	.0014
146.00	-.1812	-.0001	.0073	.0014
148.00	-.1811	-.0001	.0073	.0014
150.00	-.1811	-.0001	.0073	.0014
152.00	-.1811	-.0001	.0073	.0014
154.00	-.1811	-.0001	.0073	.0014
156.00	-.1811	-.0001	.0073	.0014
158.00	-.1811	-.0001	.0073	.0014
160.00	-.1811	-.0001	.0073	.0014

SD2

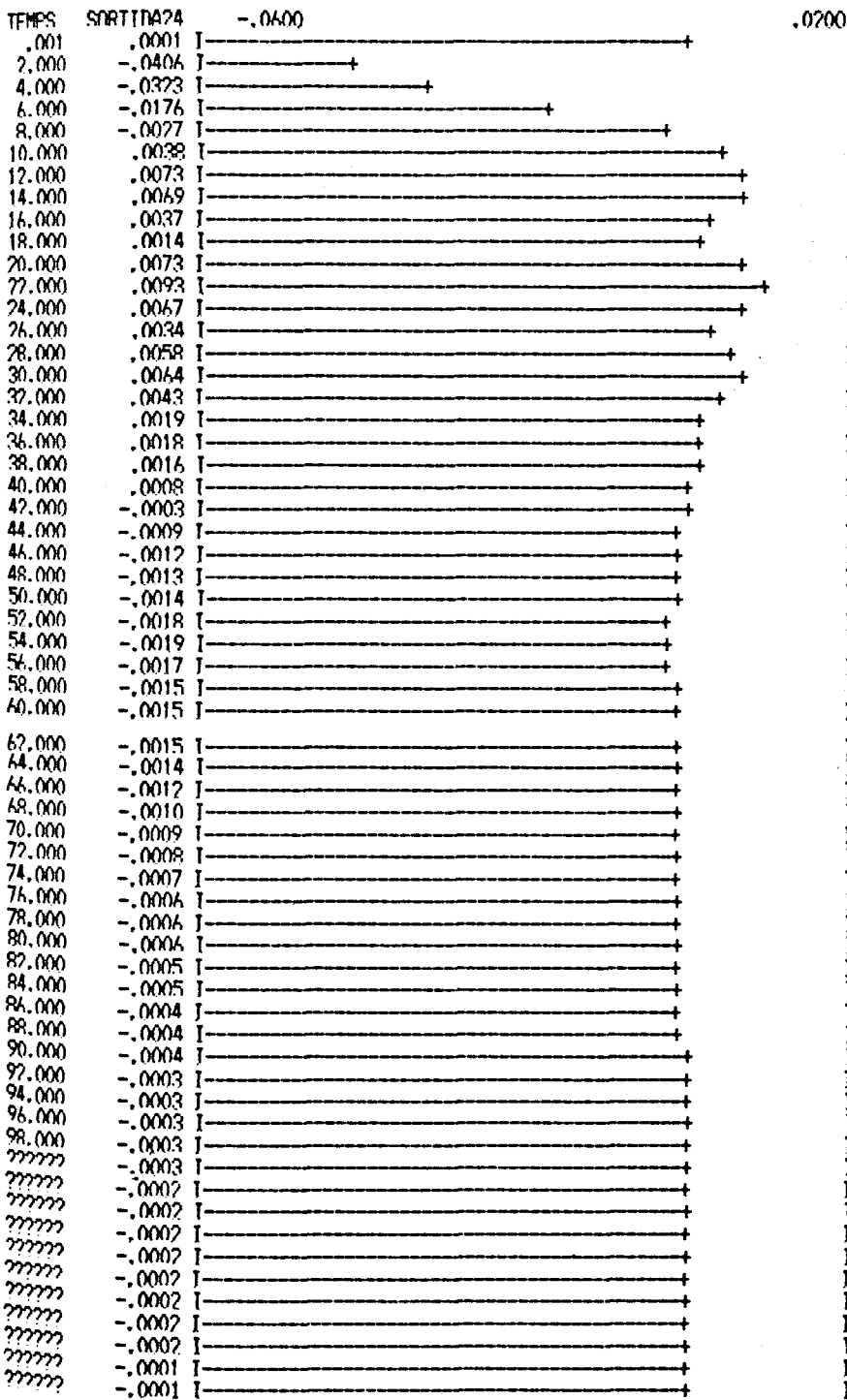
RLO discreto de acción simple (sin retardo) diseñado según [62.13] (penalización en kT) y modelo de simulación.

$T = 8$ segundos.

(simulación sin retardo de cálculo).

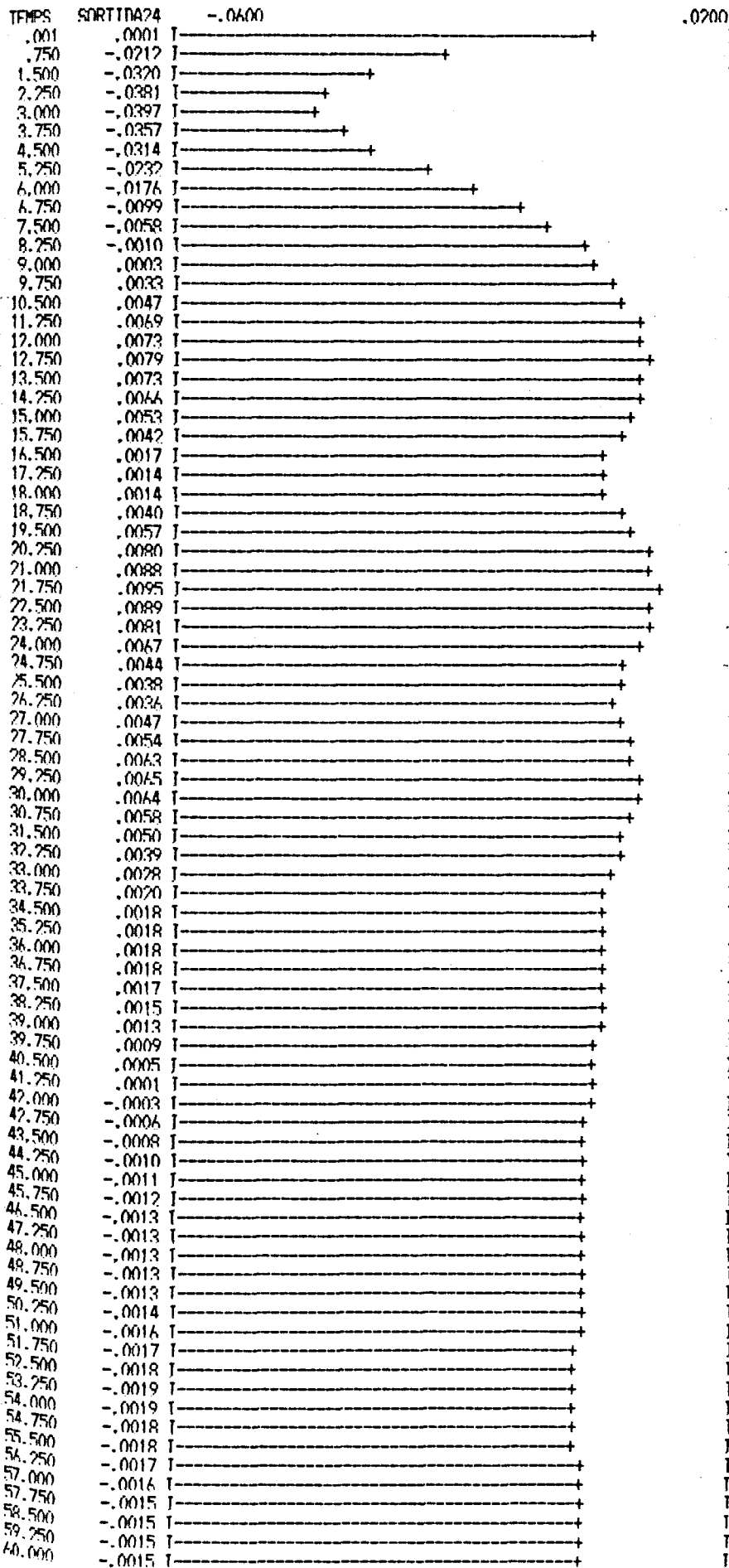
BLOC FIX Y (24) MINIM (-.0600) MAXIM (.0200)

SD2.1



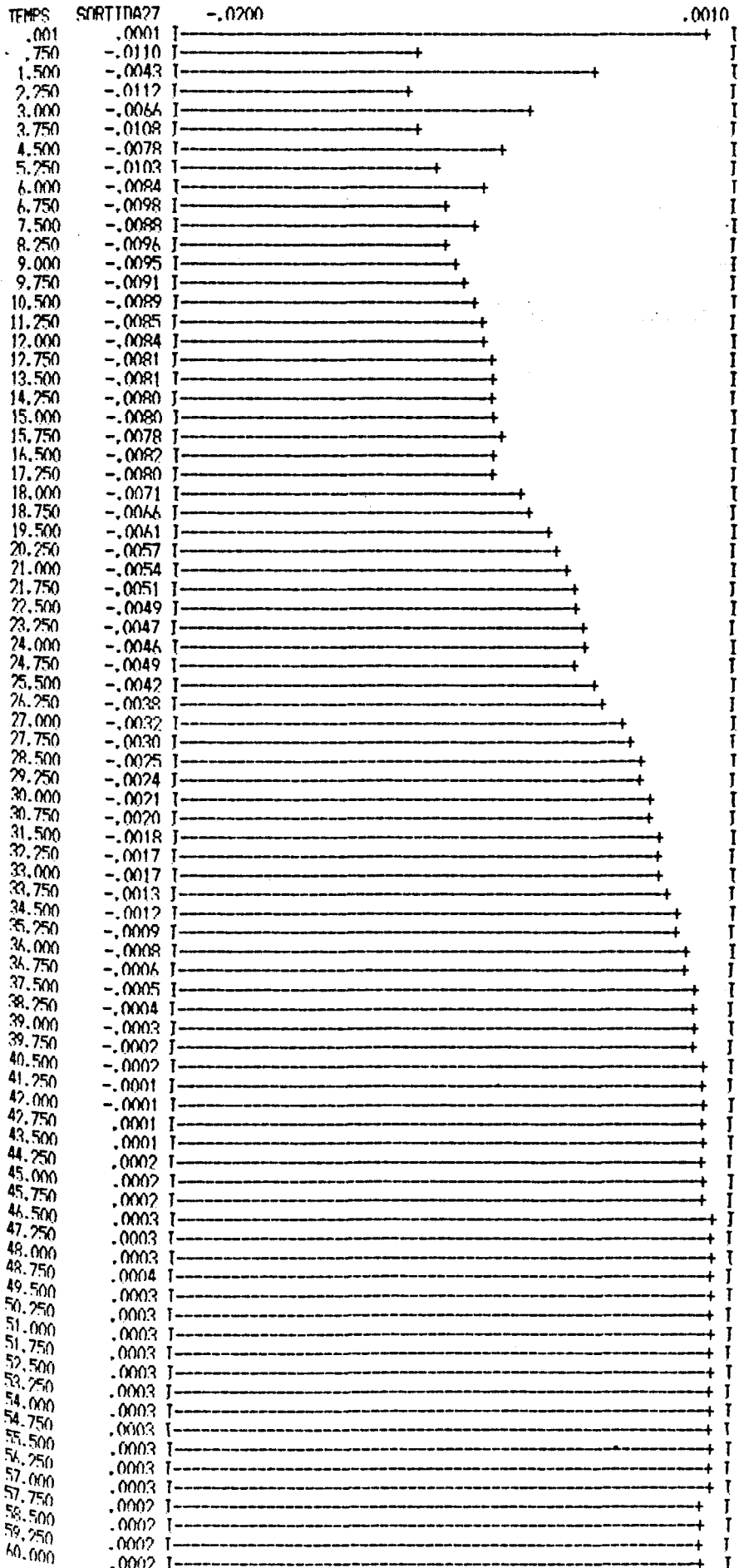
RINC FLX Y (24) MINJM (-.0600) MAXJM (.0200)

SD2.2



BLD: FIX Y (27) MINIM (-.0200) MAXIM (.0010)

SD2.3



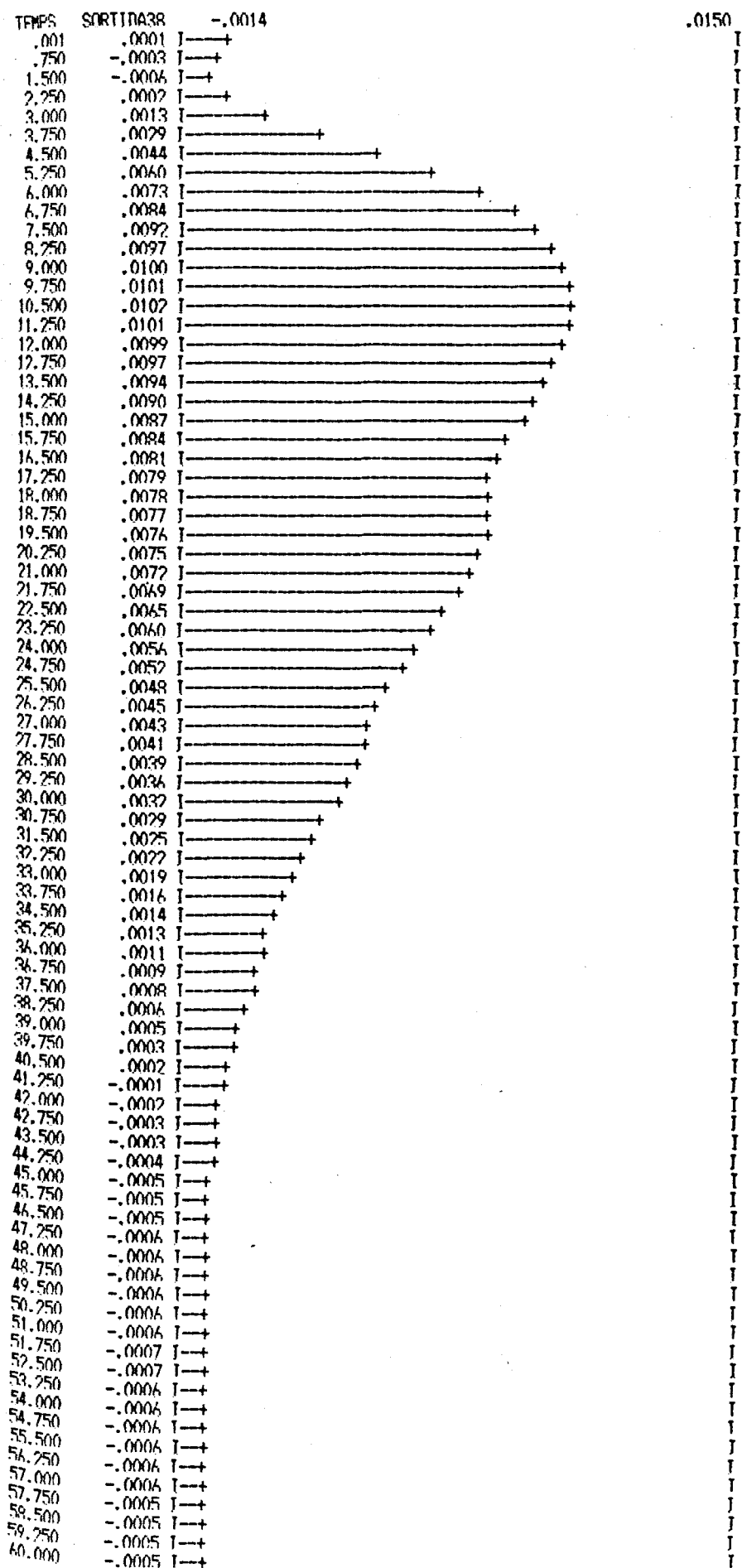
RUC: FIX Y (20) MINIM (-.0007) MAXIM (.0150)

SD2.4

TEMPS	SORTIDA20	-.0007	.0150
.001	.0001	I+	I
.750	-.0003	I+	I
1.500	.0001	I+	I
2.250	.0004	I→	I
3.000	.0010	I→	I
3.750	.0015	I→	I
4.500	.0019	I→	I
5.250	.0020	I→	I
6.000	.0021	I→	I
6.750	.0020	I→	I
7.500	.0018	I→	I
8.250	.0012	I→	I
9.000	.0010	I→	I
9.750	.0015	I→	I
10.500	.0018	I→	I
11.250	.0019	I→	I
12.000	.0020	I→	I
12.750	.0020	I→	I
13.500	.0020	I→	I
14.250	.0020	I→	I
15.000	.0020	I→	I
15.750	.0020	I→	I
16.500	.0014	I→	I
17.250	.0022	I→	I
18.000	.0032	I→	I
18.750	.0040	I→	I
19.500	.0046	I→	I
20.250	.0049	I→	I
21.000	.0050	I→	I
21.750	.0051	I→	I
22.500	.0052	I→	I
23.250	.0053	I→	I
24.000	.0053	I→	I
24.750	.0050	I→	I
25.500	.0058	I→	I
26.250	.0065	I→	I
27.000	.0071	I→	I
27.750	.0075	I→	I
28.500	.0077	I→	I
29.250	.0079	I→	I
30.000	.0080	I→	I
30.750	.0081	I→	I
31.500	.0082	I→	I
32.250	.0081	I→	I
33.000	.0083	I→	I
33.750	.0087	I→	I
34.500	.0090	I→	I
35.250	.0092	I→	I
36.000	.0094	I→	I
36.750	.0095	I→	I
37.500	.0096	I→	I
38.250	.0097	I→	I
39.000	.0097	I→	I
39.750	.0098	I→	I
40.500	.0099	I→	I
41.250	.0099	I→	I
42.000	.0100	I→	I
42.750	.0100	I→	I
43.500	.0101	I→	I
44.250	.0101	I→	I
45.000	.0102	I→	I
45.750	.0102	I→	I
46.500	.0102	I→	I
47.250	.0103	I→	I
48.000	.0103	I→	I
48.750	.0103	I→	I
49.500	.0103	I→	I
50.250	.0103	I→	I
51.000	.0103	I→	I
51.750	.0102	I→	I
52.500	.0102	I→	I
53.250	.0102	I→	I
54.000	.0103	I→	I
54.750	.0103	I→	I
55.500	.0103	I→	I
56.250	.0103	I→	I
57.000	.0103	I→	I
57.750	.0102	I→	I
58.500	.0102	I→	I
59.250	.0102	I→	I
60.000	.0102	I→	I

RLOC FIX Y (38) MTNTH (-.0014) MAXTH (.0150)

SD2.5



TEMPS	SORTINA46	SORTINA30	SORTINA55	SORTINA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0653	-.0159	.0057	.0005
8.00	-.0854	-.0024	.0059	.0007
10.00	-.1040	.0032	.0059	.0008
12.00	-.1201	.0076	.0060	.0010
14.00	-.1350	.0067	.0061	.0011
16.00	-.1498	.0037	.0061	.0012
18.00	-.1651	.0015	.0061	.0014
20.00	-.1772	.0068	.0062	.0014
22.00	-.1862	.0091	.0063	.0015
24.00	-.1942	.0067	.0065	.0015
26.00	-.2022	.0033	.0065	.0016
28.00	-.2079	.0054	.0066	.0016
30.00	-.2115	.0062	.0066	.0016
32.00	-.2141	.0043	.0067	.0016
34.00	-.2167	.0018	.0067	.0016
36.00	-.2183	.0016	.0067	.0016
38.00	-.2190	.0015	.0067	.0016
40.00	-.2193	.0007	.0067	.0016
42.00	-.2195	-.0003	.0067	.0016
44.00	-.2194	-.0010	.0067	.0016
46.00	-.2193	-.0013	.0067	.0016
48.00	-.2191	-.0014	.0067	.0016
50.00	-.2187	-.0014	.0067	.0016
52.00	-.2185	-.0018	.0067	.0016
54.00	-.2183	-.0019	.0068	.0016
56.00	-.2182	-.0017	.0068	.0016
58.00	-.2181	-.0015	.0068	.0016
60.00	-.2180	-.0015	.0068	.0016
62.00	-.2180	-.0015	.0068	.0016
64.00	-.2180	-.0013	.0068	.0016
66.00	-.2181	-.0011	.0068	.0016
68.00	-.2181	-.0010	.0068	.0016
70.00	-.2182	-.0009	.0068	.0016
72.00	-.2183	-.0009	.0068	.0016
74.00	-.2184	-.0008	.0068	.0016
76.00	-.2184	-.0006	.0068	.0016
78.00	-.2185	-.0006	.0068	.0016
80.00	-.2185	-.0005	.0068	.0016
82.00	-.2186	-.0005	.0068	.0016
84.00	-.2186	-.0004	.0068	.0016
86.00	-.2186	-.0004	.0068	.0016
88.00	-.2187	-.0004	.0068	.0016
90.00	-.2187	-.0004	.0068	.0016
92.00	-.2187	-.0003	.0068	.0016
94.00	-.2187	-.0003	.0068	.0016
96.00	-.2187	-.0003	.0068	.0016
98.00	-.2187	-.0003	.0068	.0016
100.00	-.2187	-.0003	.0068	.0016
102.00	-.2186	-.0002	.0068	.0016
104.00	-.2186	-.0002	.0068	.0016
106.00	-.2186	-.0002	.0068	.0016
108.00	-.2186	-.0002	.0068	.0016
110.00	-.2186	-.0002	.0068	.0016
112.00	-.2186	-.0002	.0068	.0016
114.00	-.2186	-.0002	.0068	.0016
116.00	-.2186	-.0002	.0068	.0016
118.00	-.2186	-.0002	.0068	.0016
120.00	-.2186	-.0001	.0068	.0016
122.00	-.2186	-.0001	.0068	.0016
124.00	-.2186	-.0001	.0068	.0016
126.00	-.2186	-.0001	.0068	.0016
128.00	-.2186	-.0001	.0068	.0016
130.00	-.2186	-.0001	.0068	.0016
132.00	-.2186	-.0001	.0068	.0016
134.00	-.2186	-.0001	.0068	.0016
136.00	-.2186	-.0001	.0068	.0016
138.00	-.2186	-.0001	.0068	.0016
140.00	-.2186	-.0001	.0068	.0016
142.00	-.2186	-.0001	.0068	.0016
144.00	-.2186	-.0001	.0068	.0016
146.00	-.2186	-.0001	.0068	.0016
148.00	-.2186	-.0001	.0068	.0016
150.00	-.2186	-.0001	.0068	.0016
152.00	-.2186	-.0001	.0068	.0016
154.00	-.2186	-.0001	.0068	.0016
156.00	-.2186	-.0001	.0068	.0016
158.00	-.2186	-.0001	.0068	.0016
160.00	-.2186	-.0001	.0068	.0016

CONDITIONS INITIALES J PARAMETRES

BI NO.	CI/PAR 1	PAR 2	PAR 3
1	1.0000	0.0000	0.0000
4	.0377	0.0000	0.0000
6	.0247	-.0738	0.0000
7	12.9700	0.0000	0.0000
9	5.3518	0.0000	0.0000
10	.0509	0.0000	0.0000
13	0.0000	.0380	0.0000
14	0.0000	-.1672	0.0000
15	.0100	0.0000	0.0000
16	2.0746	0.0000	0.0000
18	.9640	0.0000	0.0000
21	2.0746	0.0000	0.0000
22	-1.0000	1.0000	-1.0000
23	6.2500	0.0000	0.0000
24	0.0000	-.0937	0.0000
26	1.5300	0.0000	0.0000
28	1.0000	1.0000	-1.0000
29	6.2490	0.0000	0.0000
30	0.0000	-1.2343	0.0000
31	.0525	0.0000	0.0000
32	0.0000	-.0295	0.0000
33	2.0000	0.0000	0.0000
35	1.0000	0.0000	0.0000
37	2.0000	0.0000	0.0000
41	3.3670	-.2022	.3716
42	.1238	.7647	-.0034
44	.0920	0.0000	0.0000
49	0.0000	-.1292	0.0000
50	.0200	0.0000	0.0000
51	-.0001	0.0000	0.0000
52	1.9475	0.0000	0.0000
59	8.0000	-5.9750	0.0000
61	2.0000	0.0000	0.0000
63	8.0000	.0250	0.0000
64	4.0000	0.0000	0.0000
66	1.7770	-2.6666	0.0000
68	8.0000	-3.9750	0.0000
69	8.0000	0.0000	0.0000
71	20000.0000	0.0000	0.0000
74	.0100	0.0000	0.0000
75	60.0000	0.0000	0.0000

SD3

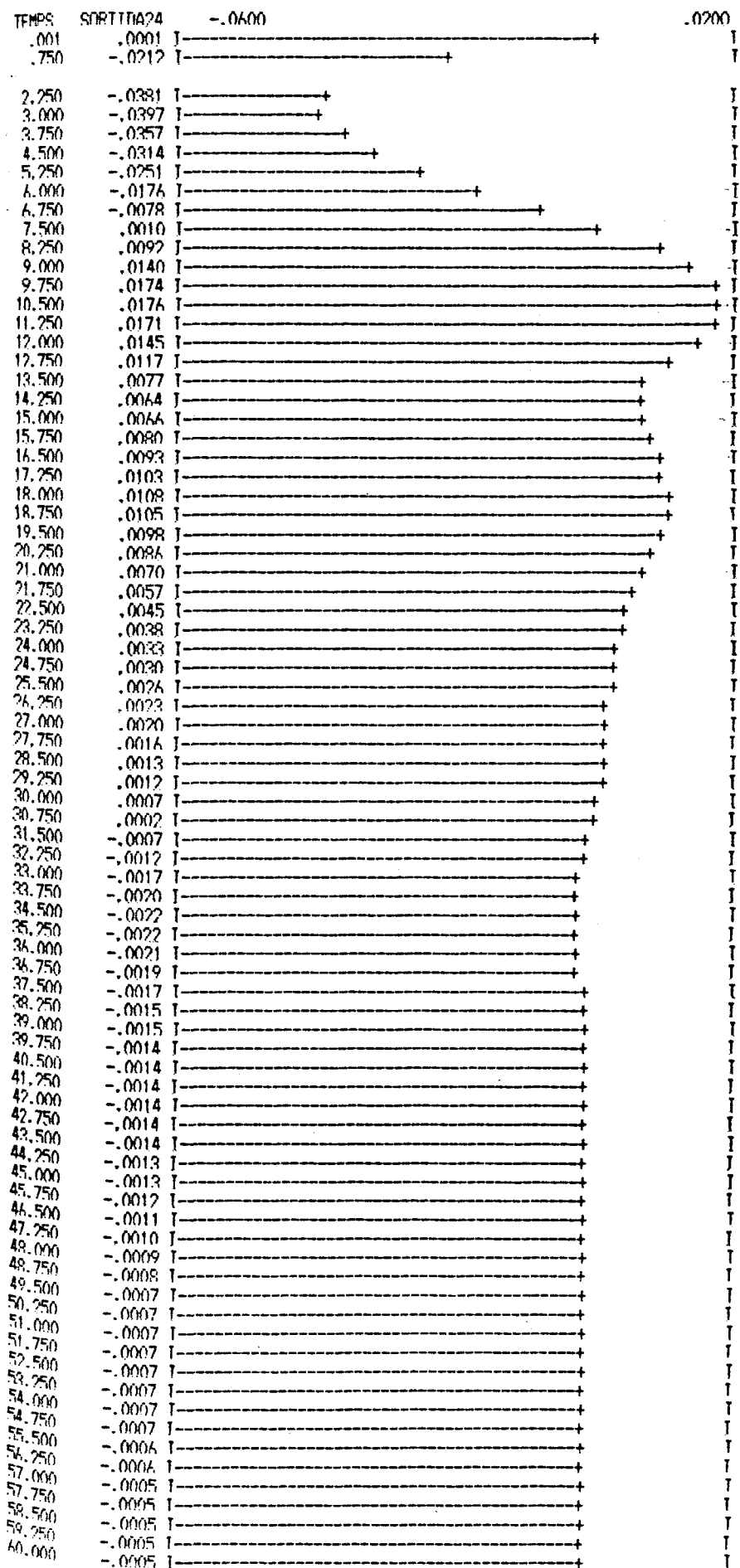
RLO discreto de acción simple (sin retardo) diseñado según [62.11] (penalización continua).

T = 8 segundos.

(simulación sin retardo de cálculo).

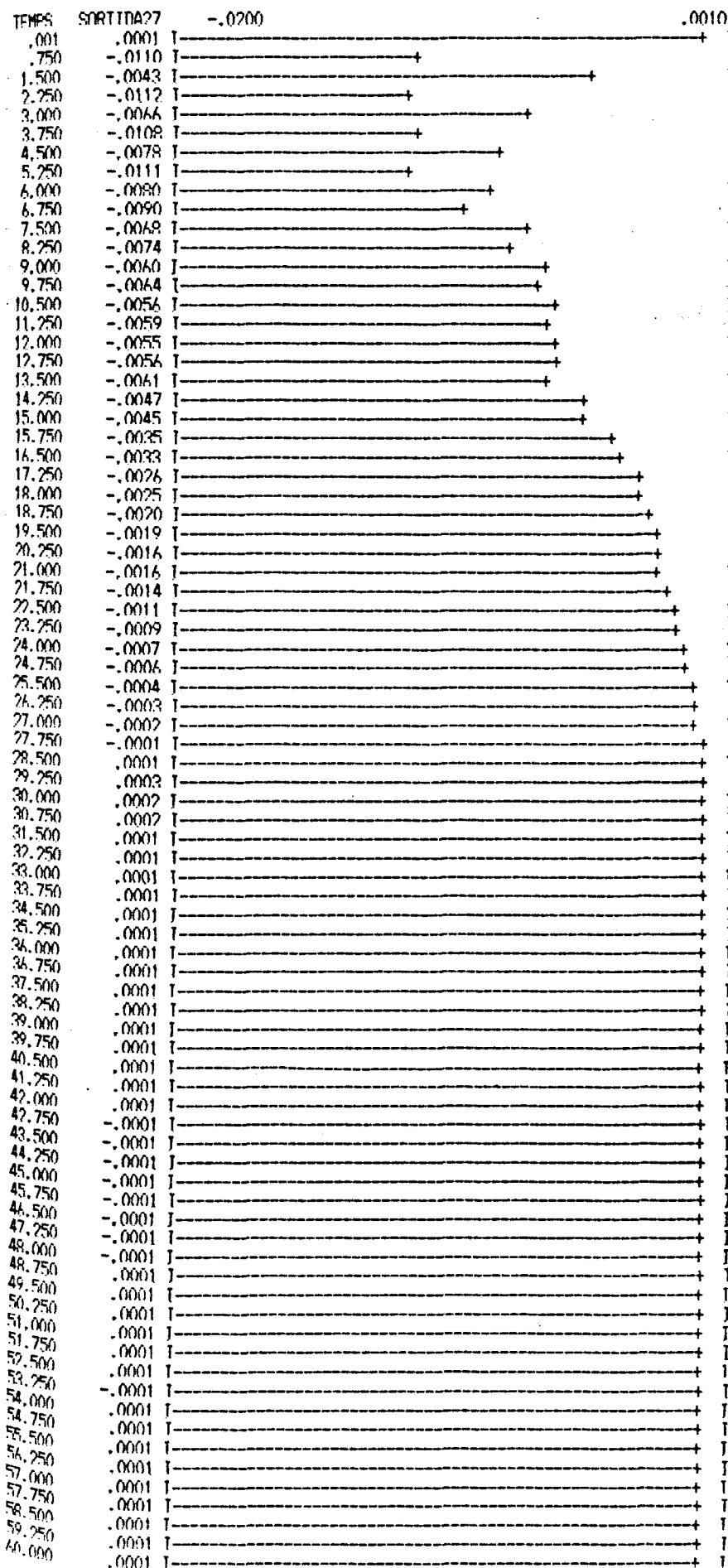
RDC ETX Y (24) MINIM (-.0600) MAXIM (.0200)

SD3.1



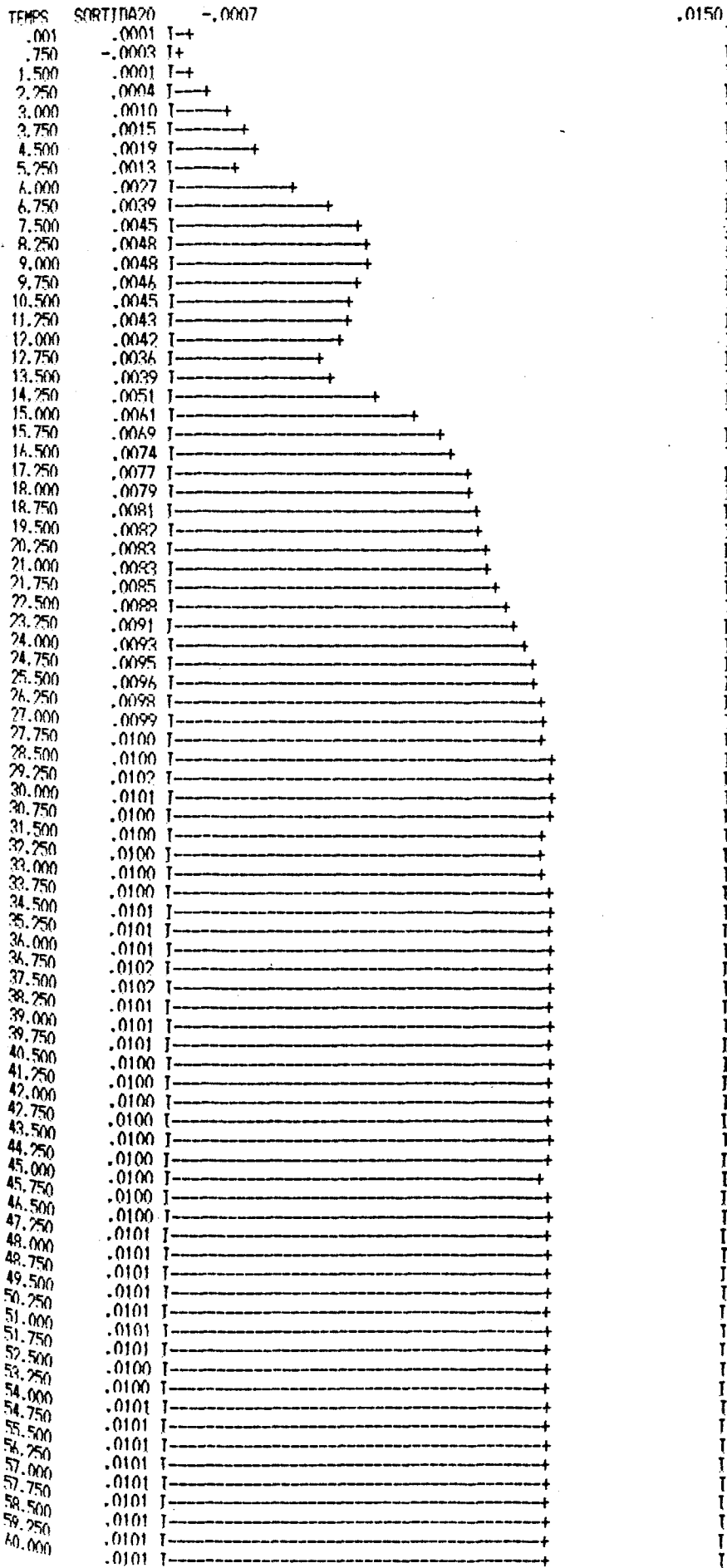
R(FC) FTY Y (27) MINIM (-.0200) MAXIM (.0010)

SD3.2



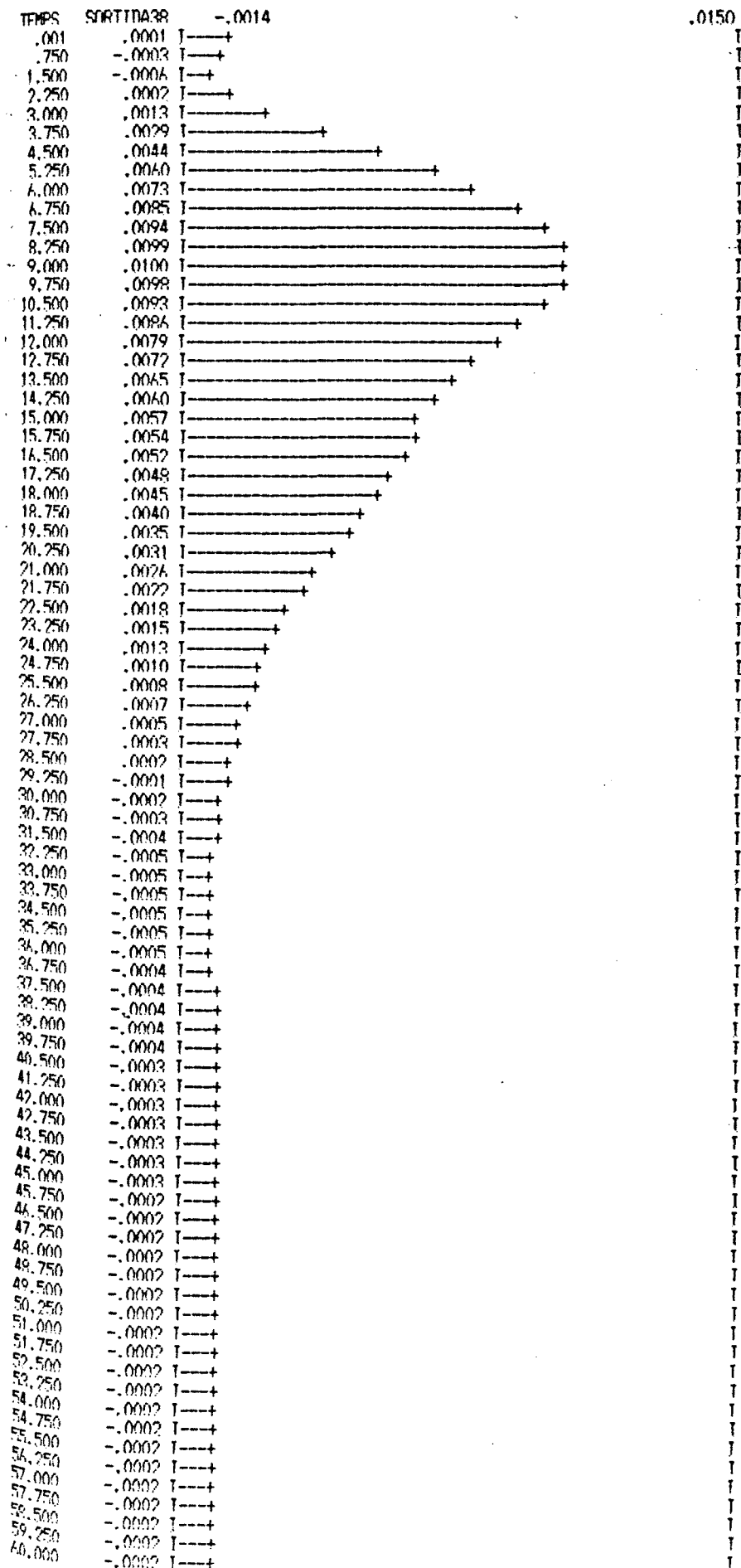
BLOC FIX Y (20) MINIM (-.0007) MAXIM (.0150)

SD3.3



R OF FIX Y (38) MINIM (-.0014) MAXIM (.0150)

SD3.4



TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0660	-.0177	.0058	.0005
8.00	-.0827	.0065	.0059	.0006
10.00	-.0932	.0170	.0063	.0007
12.00	-.1014	.0148	.0069	.0008
14.00	-.1109	.0055	.0071	.0008
16.00	-.1180	.0082	.0072	.0009
18.00	-.1219	.0104	.0074	.0009
20.00	-.1239	.0088	.0076	.0009
22.00	-.1256	.0050	.0077	.0009
24.00	-.1267	.0032	.0077	.0009
26.00	-.1272	.0023	.0078	.0009
28.00	-.1271	.0015	.0078	.0009
30.00	-.1267	.0008	.0078	.0009
32.00	-.1265	-.0011	.0078	.0009
34.00	-.1267	-.0021	.0078	.0009
36.00	-.1270	-.0021	.0078	.0009
38.00	-.1271	-.0015	.0078	.0009
40.00	-.1273	-.0014	.0078	.0009
42.00	-.1275	-.0014	.0078	.0009
44.00	-.1278	-.0013	.0078	.0009
46.00	-.1281	-.0012	.0078	.0009
48.00	-.1283	-.0009	.0078	.0009
50.00	-.1284	-.0007	.0078	.0009
52.00	-.1285	-.0007	.0078	.0009
54.00	-.1284	-.0007	.0078	.0009
56.00	-.1287	-.0006	.0078	.0009
58.00	-.1287	-.0005	.0078	.0009
60.00	-.1287	-.0005	.0078	.0009
62.00	-.1287	-.0005	.0078	.0009
64.00	-.1287	-.0005	.0078	.0009
66.00	-.1286	-.0005	.0078	.0009
68.00	-.1286	-.0005	.0078	.0009
70.00	-.1286	-.0004	.0078	.0009
72.00	-.1286	-.0004	.0078	.0009
74.00	-.1286	-.0004	.0078	.0009
76.00	-.1286	-.0004	.0078	.0009
78.00	-.1286	-.0003	.0078	.0009
80.00	-.1286	-.0003	.0078	.0009
82.00	-.1286	-.0003	.0078	.0009
84.00	-.1286	-.0003	.0078	.0009
86.00	-.1286	-.0002	.0078	.0009
88.00	-.1286	-.0002	.0078	.0009
90.00	-.1286	-.0002	.0078	.0009
92.00	-.1286	-.0002	.0078	.0009
94.00	-.1286	-.0002	.0078	.0009
96.00	-.1285	-.0002	.0078	.0009
98.00	-.1285	-.0002	.0078	.0009
100.00	-.1285	-.0002	.0078	.0009
102.00	-.1285	-.0001	.0078	.0009
104.00	-.1285	-.0001	.0078	.0009
106.00	-.1285	-.0001	.0078	.0009
108.00	-.1285	-.0001	.0078	.0009
110.00	-.1285	-.0001	.0078	.0009
112.00	-.1285	-.0001	.0078	.0009
114.00	-.1285	-.0001	.0078	.0009
116.00	-.1285	-.0001	.0078	.0009
118.00	-.1285	-.0001	.0078	.0009
120.00	-.1285	-.0001	.0078	.0009
122.00	-.1285	-.0001	.0078	.0009
124.00	-.1285	-.0001	.0078	.0009
126.00	-.1285	-.0001	.0078	.0009
128.00	-.1285	-.0001	.0078	.0009
130.00	-.1285	-.0001	.0078	.0009
132.00	-.1285	-.0001	.0078	.0009
134.00	-.1285	-.0001	.0078	.0009
136.00	-.1285	-.0001	.0078	.0009
138.00	-.1285	-.0001	.0078	.0009
140.00	-.1285	-.0001	.0078	.0009
142.00	-.1285	-.0001	.0078	.0009
144.00	-.1285	-.0001	.0078	.0009
146.00	-.1285	-.0001	.0078	.0009
148.00	-.1285	-.0001	.0078	.0009
150.00	-.1285	-.0001	.0078	.0009
152.00	-.1285	-.0001	.0078	.0009
154.00	-.1285	-.0001	.0078	.0009
156.00	-.1285	-.0001	.0078	.0009
158.00	-.1285	-.0001	.0078	.0009
160.00	-.1285	-.0001	.0078	.0009

SD4

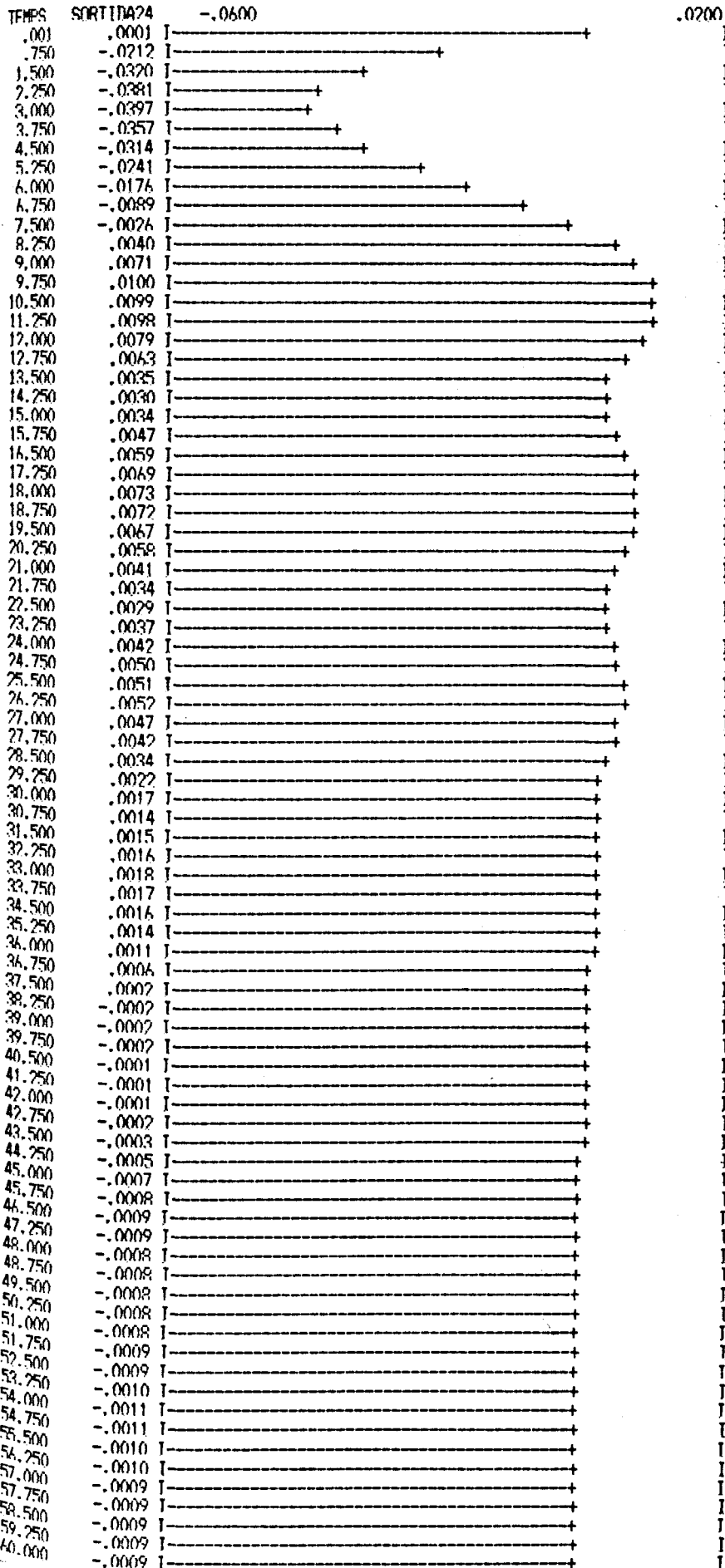
RLO discreto de acción simple con un retardo de 4 segundos en el cálculo de la acción de control ($T = 8$ segundos).

Diseño según [62.13] (penalización en kT) y sin considerar el retardo.

(simulación con el retardo de cálculo).

RUC: FIX Y (24) MINIM (-.0600) MAXIM (.0200)

SD4.1



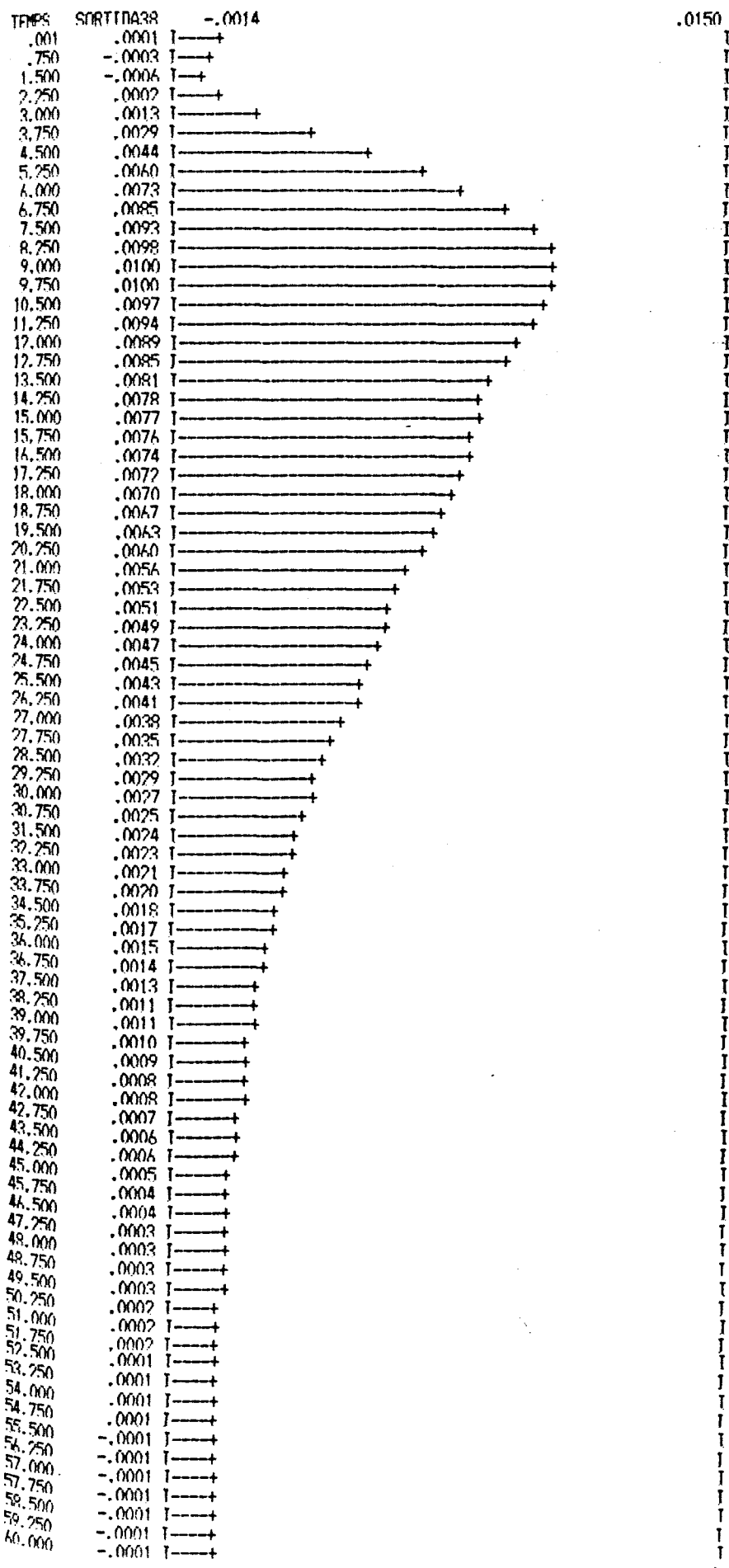
R.DC FIX Y (20) MINIM (-.0007) MAXIM (.0150)

SD4.3

TEMPS	SDRTIDA20	-.0007	.0150
.001	.0001	I+	I
.750	-.0003	I+	I
1.500	.0001	I+	I
2.250	.0004	I+	I
3.000	.0010	I+	I
3.750	.0015	I+	I
4.500	.0019	I+	I
5.250	.0017	I+	I
6.000	.0024	I+	I
6.750	.0029	I+	I
7.500	.0031	I+	I
8.250	.0031	I+	I
9.000	.0029	I+	I
9.750	.0027	I+	I
10.500	.0025	I+	I
1.250	.0023	I+	I
2.000	.0022	I+	I
17.750	.0017	I+	I
13.500	.0019	I+	I
14.250	.0028	I+	I
15.000	.0035	I+	I
15.750	.0040	I+	I
16.500	.0044	I+	I
17.250	.0046	I+	I
18.000	.0047	I+	I
18.750	.0048	I+	I
19.500	.0048	I+	I
20.250	.0049	I+	I
21.000	.0046	I+	I
21.750	.0051	I+	I
22.500	.0057	I+	I
23.250	.0062	I+	I
24.000	.0065	I+	I
24.750	.0068	I+	I
25.500	.0069	I+	I
26.250	.0070	I+	I
27.000	.0071	I+	I
27.750	.0072	I+	I
28.500	.0072	I+	I
29.250	.0072	I+	I
30.000	.0075	I+	I
30.750	.0078	I+	I
31.500	.0080	I+	I
32.250	.0082	I+	I
33.000	.0083	I+	I
33.750	.0084	I+	I
34.500	.0085	I+	I
35.250	.0086	I+	I
36.000	.0086	I+	I
36.750	.0086	I+	I
37.500	.0087	I+	I
38.250	.0089	I+	I
39.000	.0090	I+	I
39.750	.0091	I+	I
40.500	.0092	I+	I
41.250	.0092	I+	I
42.000	.0093	I+	I
42.750	.0093	I+	I
43.500	.0094	I+	I
44.250	.0094	I+	I
45.000	.0094	I+	I
45.750	.0094	I+	I
46.500	.0095	I+	I
47.250	.0096	I+	I
48.000	.0096	I+	I
48.750	.0097	I+	I
49.500	.0097	I+	I
50.250	.0097	I+	I
51.000	.0097	I+	I
51.750	.0097	I+	I
52.500	.0098	I+	I
53.250	.0098	I+	I
54.000	.0098	I+	I
54.750	.0098	I+	I
55.500	.0099	I+	I
56.250	.0099	I+	I
57.000	.0099	I+	I
57.750	.0099	I+	I
58.500	.0099	I+	I
59.250	.0099	I+	I
60.000	.0099	I+	I

ROE: FTX Y (38) MINIM (-.0014) MAXIM (.0150)

SD4.4



TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0657	-.0168	.0057	.0005
8.00	-.0842	.0019	.0059	.0006
10.00	-.0988	.0095	.0060	.0008
12.00	-.1123	.0084	.0062	.0009
14.00	-.1270	.0022	.0062	.0010
16.00	-.1399	.0050	.0063	.0011
18.00	-.1505	.0071	.0064	.0012
20.00	-.1597	.0060	.0065	.0012
22.00	-.1690	.0025	.0065	.0013
24.00	-.1767	.0042	.0065	.0013
26.00	-.1827	.0050	.0066	.0013
28.00	-.1876	.0038	.0066	.0013
30.00	-.1925	.0014	.0066	.0014
32.00	-.1966	.0015	.0066	.0014
34.00	-.1998	.0016	.0066	.0014
36.00	-.2025	.0010	.0066	.0014
38.00	-.2050	-.0002	.0066	.0014
40.00	-.2072	-.0002	.0066	.0014
42.00	-.2088	-.0001	.0066	.0014
44.00	-.2102	-.0004	.0066	.0014
46.00	-.2115	-.0009	.0066	.0014
48.00	-.2126	-.0009	.0066	.0014
50.00	-.2135	-.0008	.0066	.0014
52.00	-.2143	-.0009	.0066	.0014
54.00	-.2149	-.0011	.0066	.0014
56.00	-.2155	-.0010	.0066	.0014
58.00	-.2160	-.0009	.0066	.0014
60.00	-.2164	-.0009	.0066	.0014
62.00	-.2167	-.0010	.0066	.0014
64.00	-.2170	-.0009	.0066	.0014
66.00	-.2173	-.0008	.0067	.0014
68.00	-.2175	-.0008	.0067	.0014
70.00	-.2177	-.0008	.0067	.0014
72.00	-.2178	-.0008	.0067	.0014
74.00	-.2179	-.0007	.0067	.0014
76.00	-.2180	-.0007	.0067	.0014
78.00	-.2181	-.0007	.0067	.0014
80.00	-.2182	-.0006	.0067	.0014
82.00	-.2183	-.0006	.0067	.0014
84.00	-.2183	-.0005	.0067	.0014
86.00	-.2184	-.0005	.0067	.0014
88.00	-.2184	-.0005	.0067	.0014
90.00	-.2184	-.0004	.0067	.0014
92.00	-.2185	-.0004	.0067	.0014
94.00	-.2185	-.0004	.0067	.0014
96.00	-.2185	-.0004	.0067	.0014
98.00	-.2185	-.0003	.0067	.0014
100.00	-.2185	-.0003	.0067	.0014
102.00	-.2185	-.0003	.0067	.0014
104.00	-.2185	-.0003	.0067	.0014
106.00	-.2185	-.0003	.0067	.0014
108.00	-.2186	-.0002	.0067	.0014
110.00	-.2186	-.0002	.0067	.0014
112.00	-.2186	-.0002	.0067	.0014
114.00	-.2186	-.0002	.0067	.0014
116.00	-.2186	-.0002	.0067	.0014
118.00	-.2186	-.0002	.0067	.0014
120.00	-.2186	-.0002	.0067	.0014
122.00	-.2186	-.0002	.0067	.0014
124.00	-.2186	-.0001	.0067	.0014
126.00	-.2186	-.0001	.0067	.0014
128.00	-.2186	-.0001	.0067	.0014
130.00	-.2186	-.0001	.0067	.0014
132.00	-.2186	-.0001	.0067	.0014
134.00	-.2186	-.0001	.0067	.0014
136.00	-.2186	-.0001	.0067	.0014
138.00	-.2186	-.0001	.0067	.0014
140.00	-.2186	-.0001	.0067	.0014
142.00	-.2186	-.0001	.0067	.0014
144.00	-.2186	-.0001	.0067	.0014
146.00	-.2186	-.0001	.0067	.0014
148.00	-.2186	-.0001	.0067	.0014
150.00	-.2186	-.0001	.0067	.0014
152.00	-.2185	-.0001	.0067	.0014
154.00	-.2185	-.0001	.0067	.0014
156.00	-.2185	-.0001	.0067	.0014
158.00	-.2185	-.0001	.0067	.0014
160.00	-.2185	-.0001	.0067	.0014

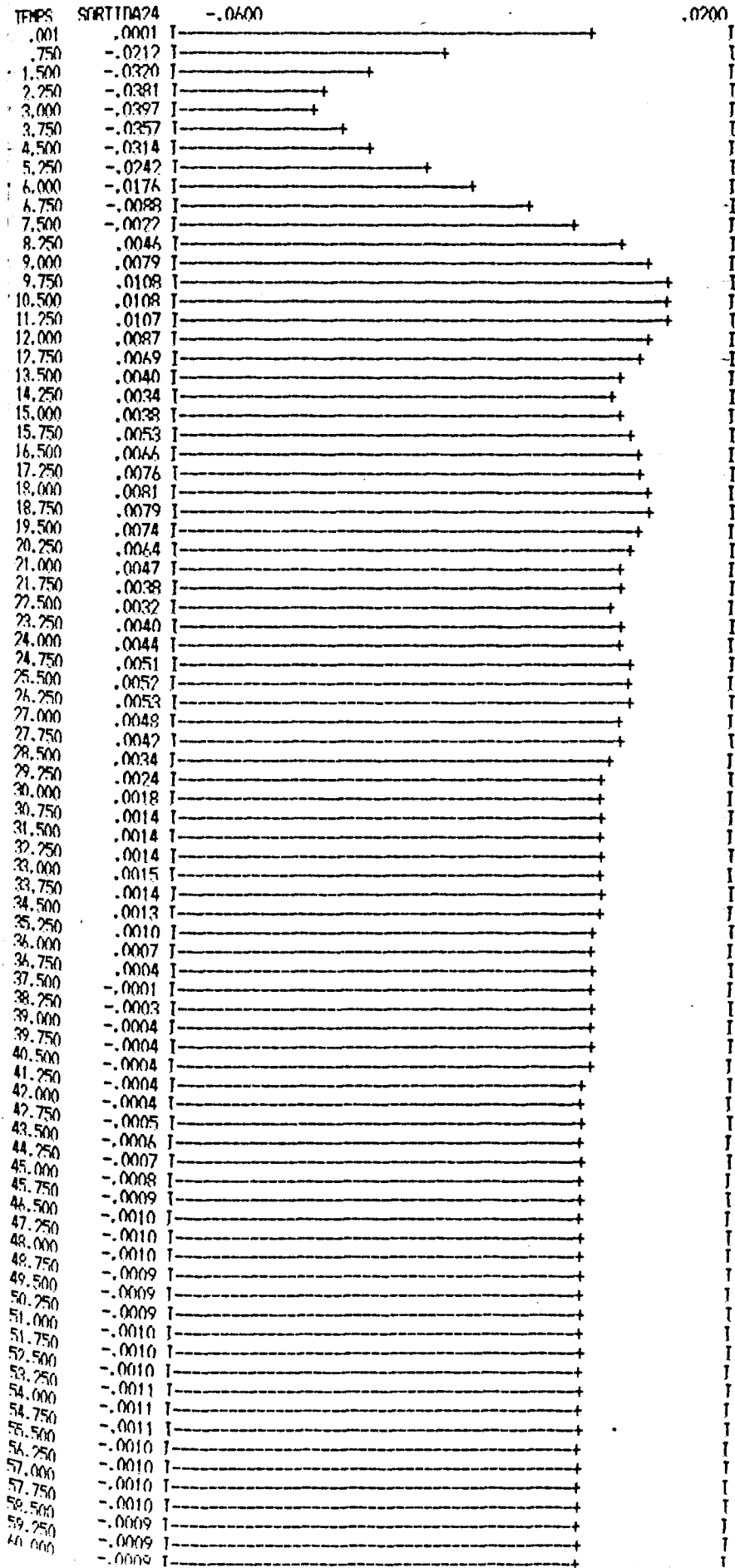
SD5

RLO discreto de acción simple con un retardo de 4 segundos en el cálculo de la acción de control ($T = 8$ segundos).

Diseño según [62.13] (penalización en kT) y considerando el retardo.

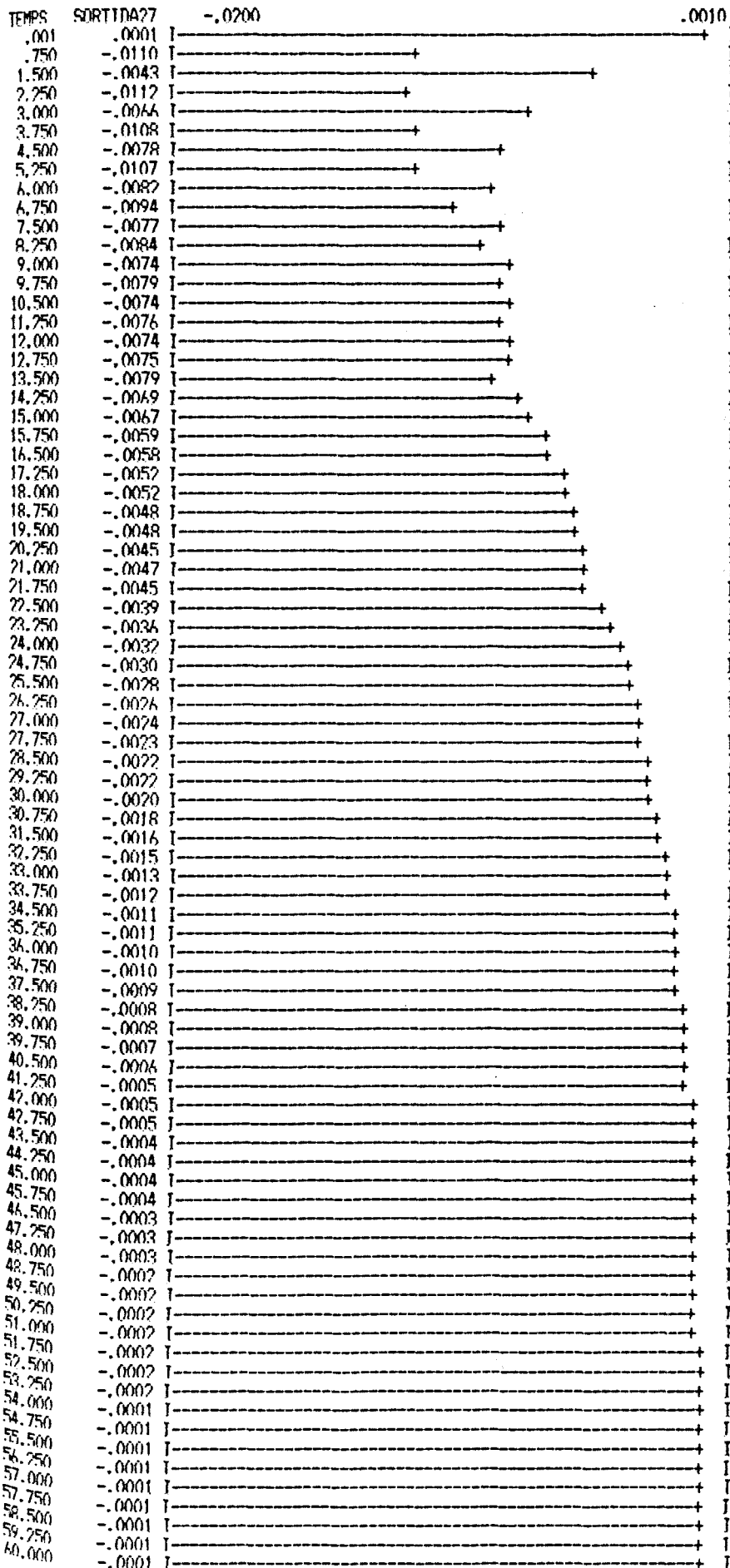
(simulación con el retardo de cálculo).

R(C FIX Y (24) MINIM (-.0600) MAXIM (.0200)



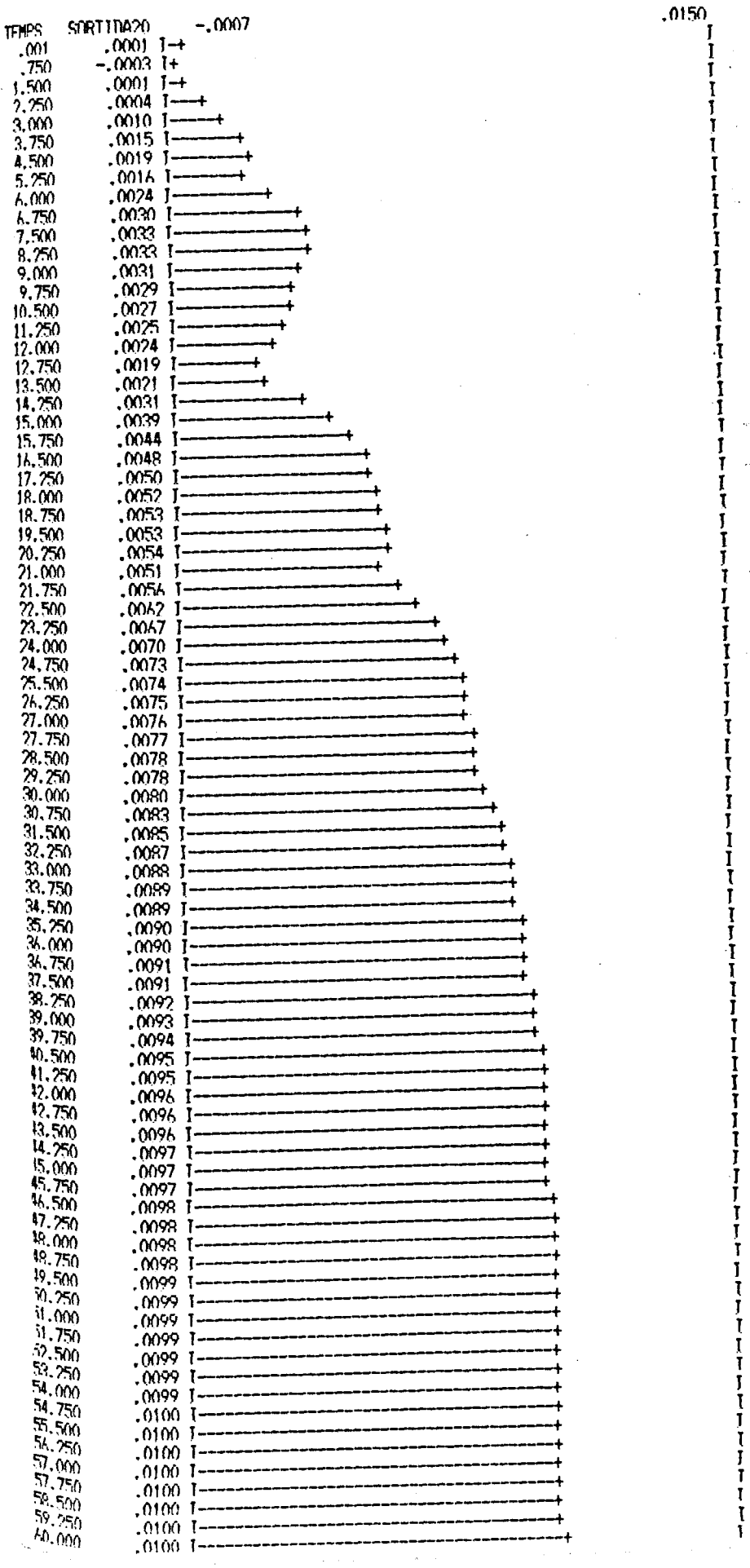
RUC ETX Y (27) MINIM (-.0200) MAXIM (.0010)

SD5.2



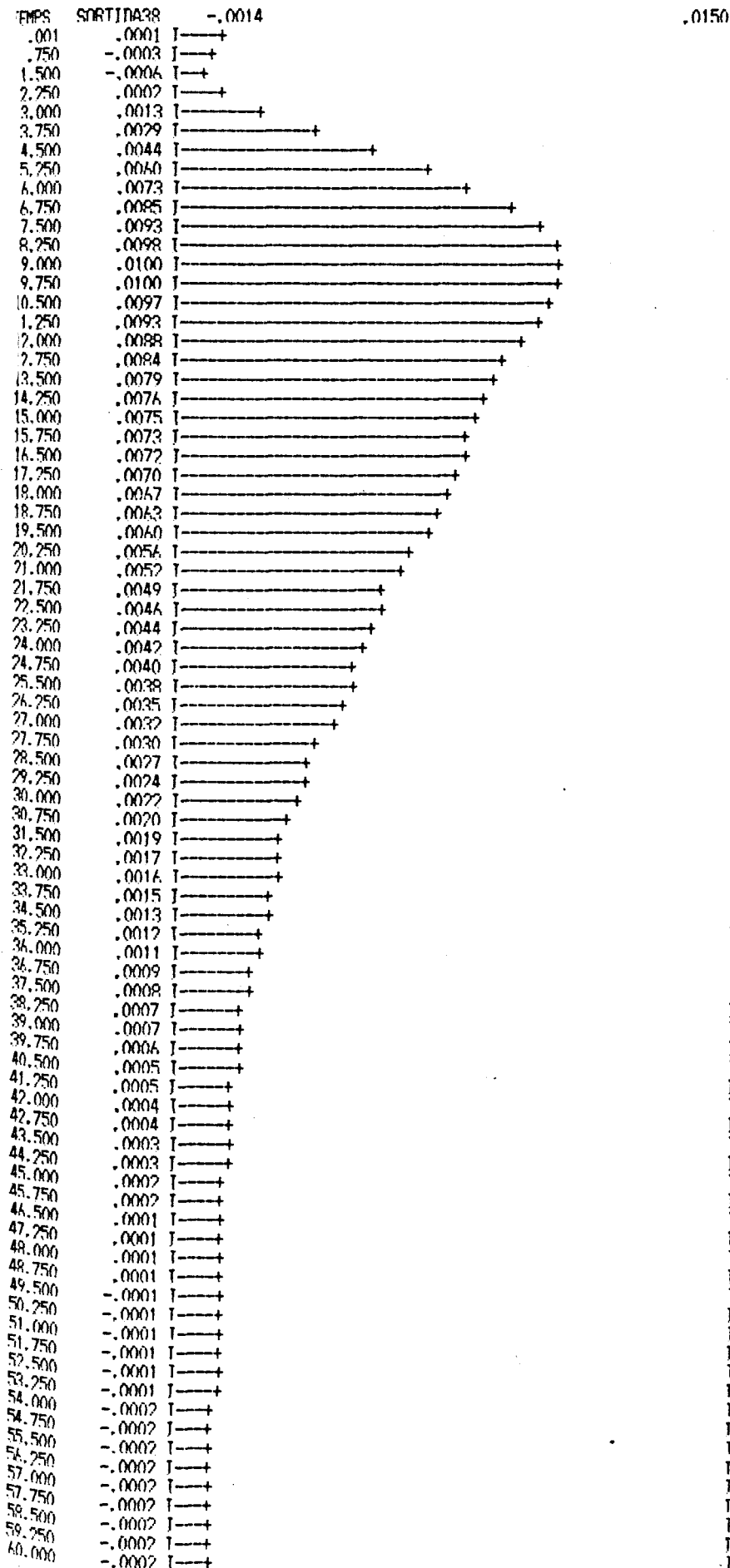
SD5.3

RUC FIX Y (20) MINIM (-.0007) MAXIM (.0150)



RUC FIX V (38) MINIM (-.0014) MAXIM (.0150)

SD5.4



TEMPS	SORTIDA4A	SORTIDA30	SORTIDA55	SORTIDA5A
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0007
4.00	-.0478	-.0369	.0043	.0003
6.00	-.0457	-.0169	.0057	.0005
8.00	-.0840	.0024	.0059	.0006
10.00	-.0982	.0104	.0060	.0008
12.00	-.1110	.0092	.0062	.0009
14.00	-.1251	.0025	.0063	.0010
16.00	-.1373	.0055	.0064	.0011
18.00	-.1468	.0078	.0065	.0011
20.00	-.1550	.0066	.0066	.0012
22.00	-.1632	.0029	.0066	.0012
24.00	-.1698	.0043	.0067	.0012
26.00	-.1746	.0051	.0067	.0013
28.00	-.1785	.0039	.0067	.0013
30.00	-.1823	.0015	.0068	.0013
32.00	-.1854	.0013	.0068	.0013
34.00	-.1877	.0013	.0068	.0013
36.00	-.1896	.0007	.0068	.0013
38.00	-.1913	-.0003	.0068	.0013
40.00	-.1928	-.0004	.0068	.0013
42.00	-.1939	-.0005	.0068	.0013
44.00	-.1948	-.0007	.0068	.0013
46.00	-.1956	-.0010	.0068	.0013
48.00	-.1963	-.0010	.0068	.0013
50.00	-.1968	-.0010	.0068	.0013
52.00	-.1973	-.0010	.0068	.0013
54.00	-.1977	-.0011	.0068	.0013
56.00	-.1980	-.0010	.0068	.0013
58.00	-.1983	-.0010	.0068	.0013
60.00	-.1985	-.0009	.0068	.0013
62.00	-.1987	-.0010	.0068	.0013
64.00	-.1988	-.0009	.0068	.0013
66.00	-.1990	-.0008	.0068	.0013
68.00	-.1991	-.0008	.0068	.0013
70.00	-.1992	-.0008	.0068	.0013
72.00	-.1993	-.0007	.0068	.0013
74.00	-.1993	-.0006	.0068	.0013
76.00	-.1994	-.0006	.0068	.0013
78.00	-.1994	-.0006	.0068	.0013
80.00	-.1994	-.0005	.0068	.0013
82.00	-.1995	-.0005	.0068	.0013
84.00	-.1995	-.0005	.0068	.0013
86.00	-.1995	-.0004	.0068	.0013
88.00	-.1995	-.0004	.0068	.0013
90.00	-.1995	-.0004	.0068	.0013
92.00	-.1995	-.0004	.0068	.0013
94.00	-.1995	-.0003	.0068	.0013
96.00	-.1995	-.0003	.0068	.0013
98.00	-.1995	-.0003	.0068	.0013
100.00	-.1995	-.0003	.0068	.0013
102.00	-.1995	-.0003	.0068	.0013
104.00	-.1995	-.0002	.0068	.0013
106.00	-.1995	-.0002	.0068	.0013
108.00	-.1995	-.0002	.0068	.0013
110.00	-.1995	-.0002	.0068	.0013
112.00	-.1995	-.0002	.0068	.0013
114.00	-.1995	-.0002	.0068	.0013
116.00	-.1995	-.0002	.0068	.0013
118.00	-.1995	-.0002	.0068	.0013
120.00	-.1995	-.0001	.0068	.0013
122.00	-.1995	-.0001	.0068	.0013
124.00	-.1995	-.0001	.0068	.0013
126.00	-.1995	-.0001	.0068	.0013
128.00	-.1995	-.0001	.0068	.0013
130.00	-.1995	-.0001	.0068	.0013
132.00	-.1995	-.0001	.0068	.0013
134.00	-.1995	-.0001	.0068	.0013
136.00	-.1995	-.0001	.0068	.0013
138.00	-.1995	-.0001	.0068	.0013
140.00	-.1995	-.0001	.0068	.0013
142.00	-.1995	-.0001	.0068	.0013
144.00	-.1995	-.0001	.0068	.0013
146.00	-.1995	-.0001	.0068	.0013
148.00	-.1995	-.0001	.0068	.0013
150.00	-.1995	-.0001	.0068	.0013
152.00	-.1995	-.0001	.0068	.0013
154.00	-.1995	-.0001	.0068	.0013
156.00	-.1995	-.0001	.0068	.0013
158.00	-.1995	-.0001	.0068	.0013
160.00	-.1995	-.0001	.0068	.0013

SD6

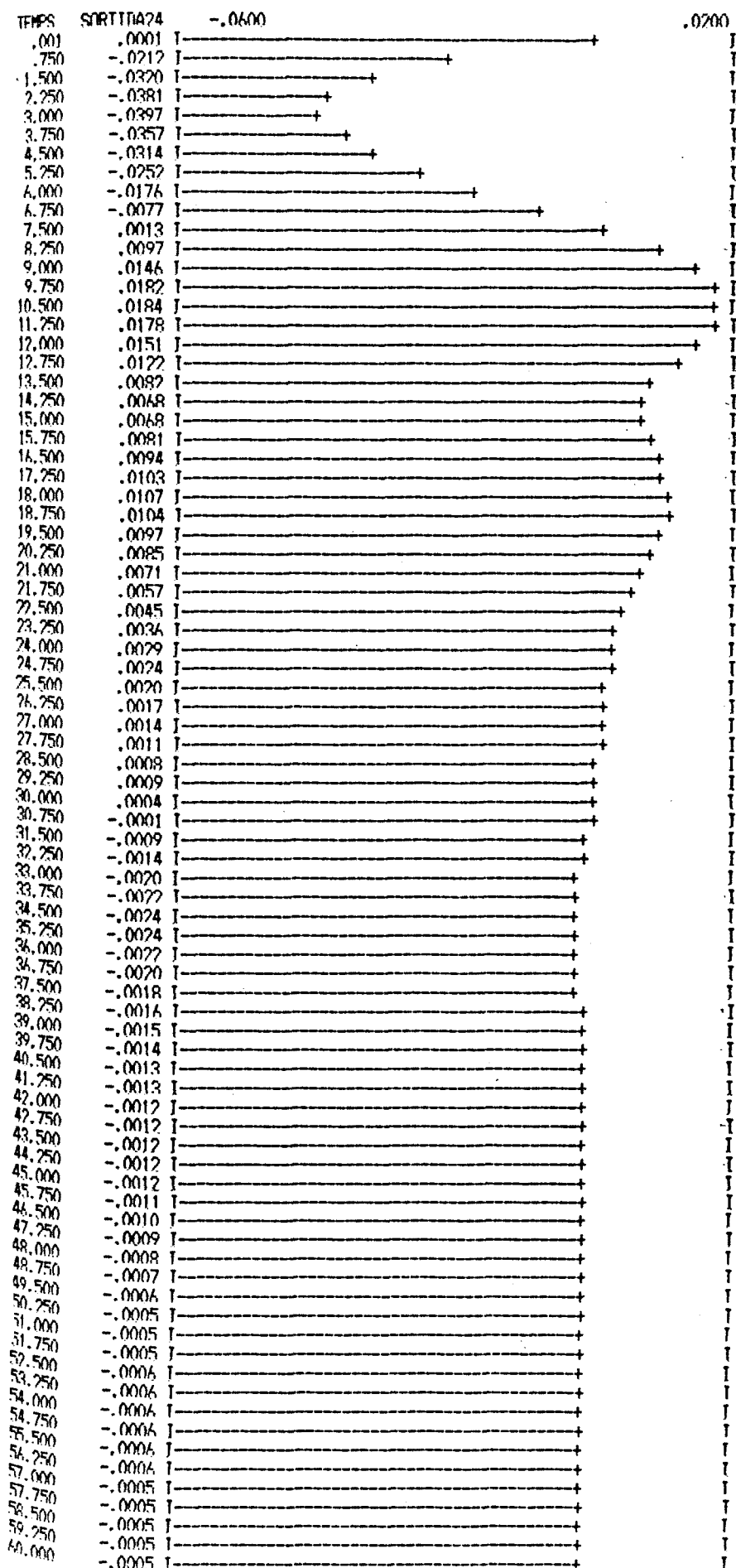
RLO discreto de acción simple con un retardo de 4 segundos en el cálculo de la acción de control ($T = 8$ segundos).

Diseñado según [62.11] (penalización continua) y considerando el retardo.

(simulación con el retardo de cálculo).

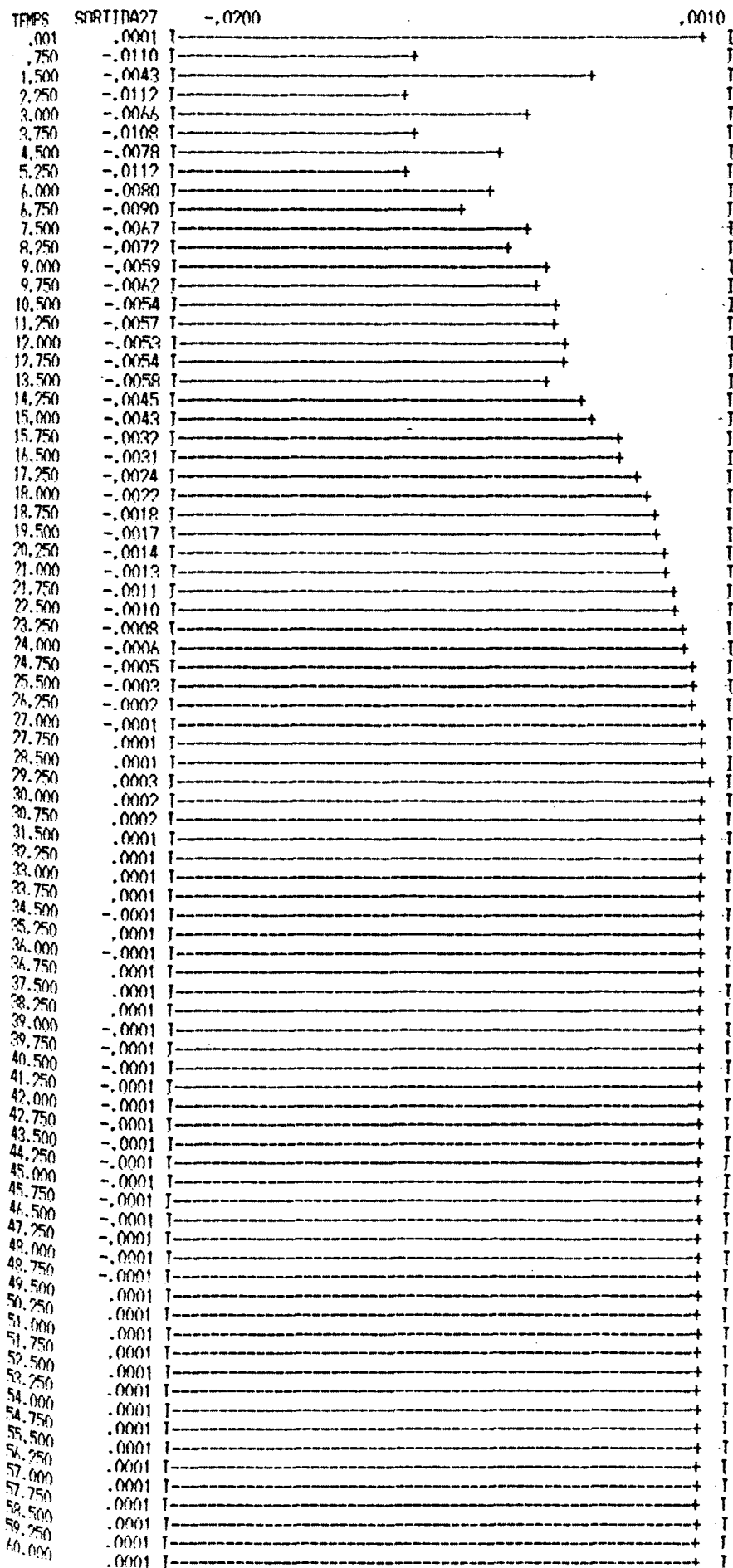
RUC FTX Y (24) MINIM (-.0600) MAXIM (.0200)

SD6.1



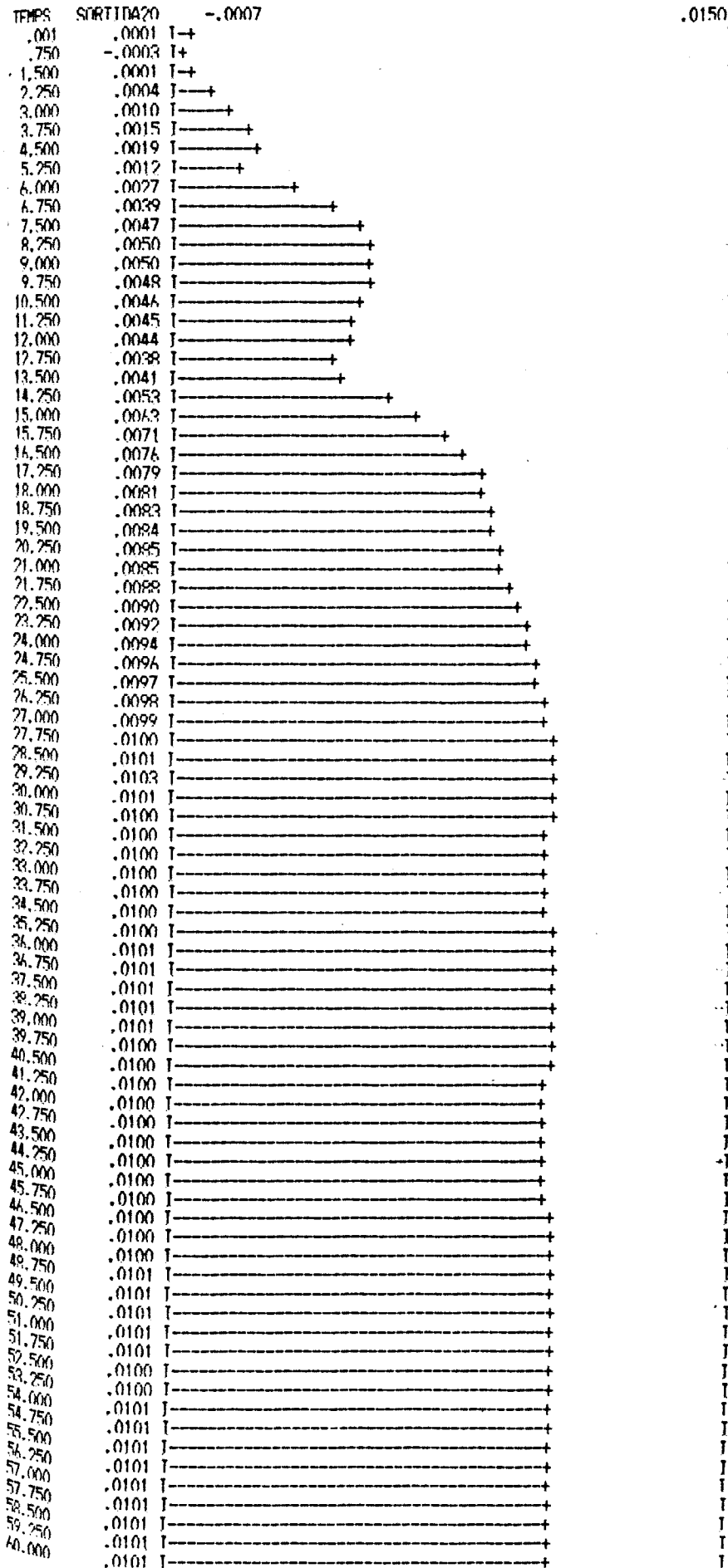
RI OF FIX Y (27) MINIM (-.0200) MAXIM (.0010)

SD6.2



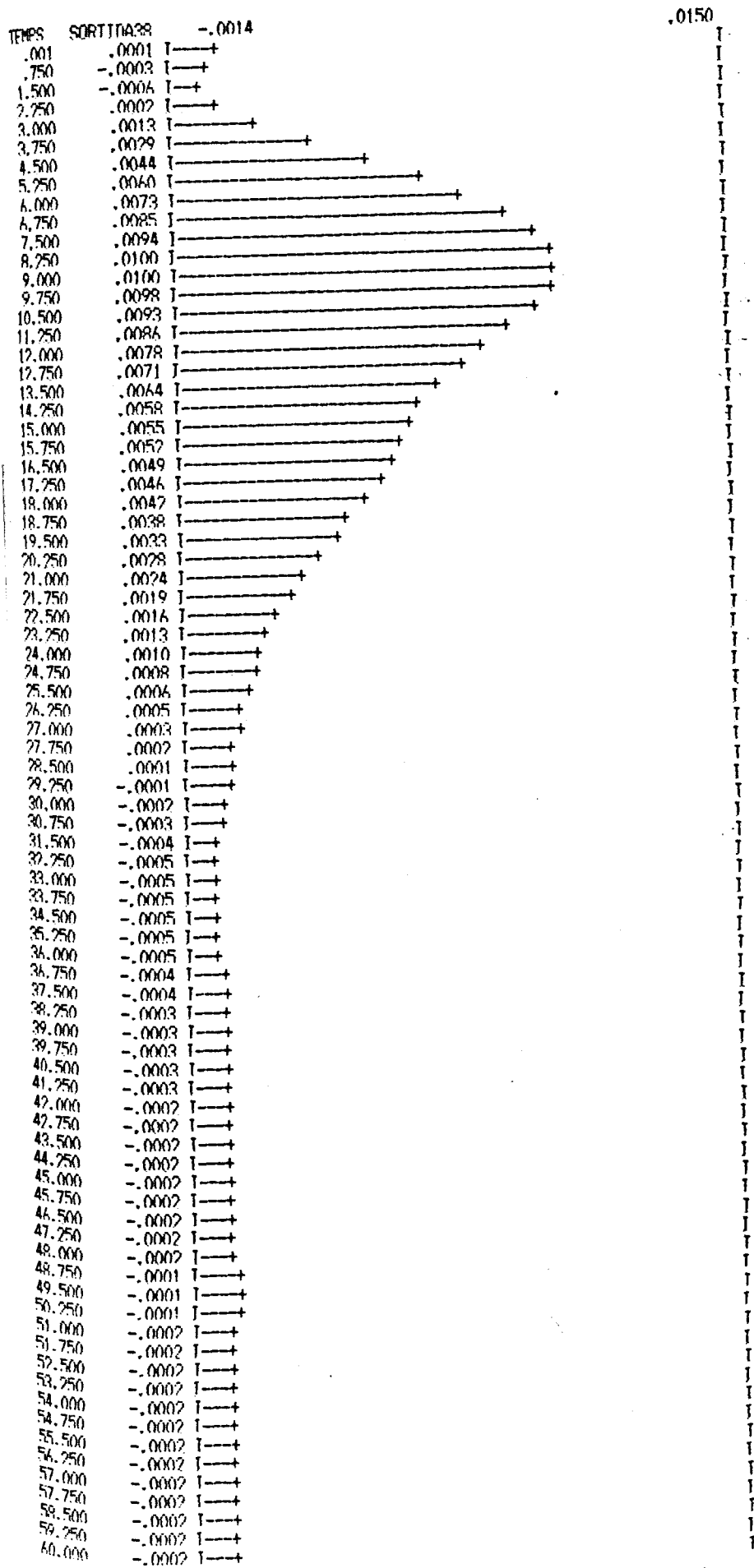
RUC FIX Y (20) MINIM (-.0007) MAXIM (.0150)

SD6.3



SD6.4

R.00 ETX Y (38) MINIM (-.0014) MAXIM (.0150)



TEMPS	SRRTINA4A	SRRTINA30	SRRTINA55	SRRTINA5A
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0661	-.0178	.0058	.0005
8.00	-.0826	.0069	.0059	.0006
10.00	-.0927	.0177	.0063	.0007
12.00	-.1003	.0155	.0070	.0008
14.00	-.1093	.0059	.0072	.0008
16.00	-.1159	.0083	.0073	.0009
18.00	-.1193	.0104	.0075	.0009
20.00	-.1210	.0088	.0077	.0009
22.00	-.1222	.0051	.0078	.0009
24.00	-.1230	.0028	.0079	.0009
26.00	-.1233	.0017	.0079	.0009
28.00	-.1233	.0009	.0079	.0009
30.00	-.1228	.0006	.0079	.0009
32.00	-.1226	-.0013	.0079	.0009
34.00	-.1229	-.0023	.0079	.0009
36.00	-.1233	-.0022	.0079	.0009
38.00	-.1237	-.0017	.0079	.0009
40.00	-.1239	-.0013	.0079	.0009
42.00	-.1242	-.0012	.0079	.0009
44.00	-.1245	-.0012	.0079	.0009
46.00	-.1248	-.0011	.0079	.0009
48.00	-.1251	-.0008	.0079	.0009
50.00	-.1252	-.0006	.0079	.0009
52.00	-.1252	-.0005	.0079	.0009
54.00	-.1253	-.0006	.0079	.0009
56.00	-.1254	-.0006	.0079	.0009
58.00	-.1254	-.0005	.0079	.0009
60.00	-.1254	-.0005	.0079	.0009
62.00	-.1253	-.0005	.0079	.0009
64.00	-.1253	-.0005	.0079	.0009
66.00	-.1253	-.0005	.0079	.0009
68.00	-.1253	-.0005	.0079	.0009
70.00	-.1253	-.0004	.0079	.0009
72.00	-.1253	-.0004	.0079	.0009
74.00	-.1253	-.0004	.0079	.0009
76.00	-.1253	-.0004	.0079	.0009
78.00	-.1253	-.0003	.0079	.0009
80.00	-.1253	-.0003	.0079	.0009
82.00	-.1253	-.0003	.0079	.0009
84.00	-.1253	-.0003	.0079	.0009
86.00	-.1253	-.0002	.0079	.0009
88.00	-.1253	-.0002	.0079	.0009
90.00	-.1253	-.0002	.0079	.0009
92.00	-.1253	-.0002	.0079	.0009
94.00	-.1252	-.0002	.0079	.0009
96.00	-.1252	-.0002	.0079	.0009
98.00	-.1252	-.0002	.0079	.0009
100.00	-.1252	-.0002	.0079	.0009
102.00	-.1252	-.0001	.0079	.0009
104.00	-.1252	-.0001	.0079	.0009
106.00	-.1252	-.0001	.0079	.0009
108.00	-.1252	-.0001	.0079	.0009
110.00	-.1252	-.0001	.0079	.0009
112.00	-.1252	-.0001	.0079	.0009
114.00	-.1252	-.0001	.0079	.0009
116.00	-.1252	-.0001	.0079	.0009
118.00	-.1252	-.0001	.0079	.0009
120.00	-.1252	-.0001	.0079	.0009
122.00	-.1252	-.0001	.0079	.0009
124.00	-.1252	-.0001	.0079	.0009
126.00	-.1252	-.0001	.0079	.0009
128.00	-.1252	-.0001	.0079	.0009
130.00	-.1252	-.0001	.0079	.0009
132.00	-.1252	-.0001	.0079	.0009
134.00	-.1252	-.0001	.0079	.0009
136.00	-.1252	-.0001	.0079	.0009
138.00	-.1252	-.0001	.0079	.0009
140.00	-.1252	-.0001	.0079	.0009
142.00	-.1252	-.0001	.0079	.0009
144.00	-.1252	-.0001	.0079	.0009
146.00	-.1252	-.0001	.0079	.0009
148.00	-.1252	-.0001	.0079	.0009
150.00	-.1252	-.0001	.0079	.0009
152.00	-.1252	-.0001	.0079	.0009
154.00	-.1252	-.0001	.0079	.0009
156.00	-.1252	-.0001	.0079	.0009
158.00	-.1252	-.0001	.0079	.0009
160.00	-.1252	-.0001	.0079	.0009

SD7

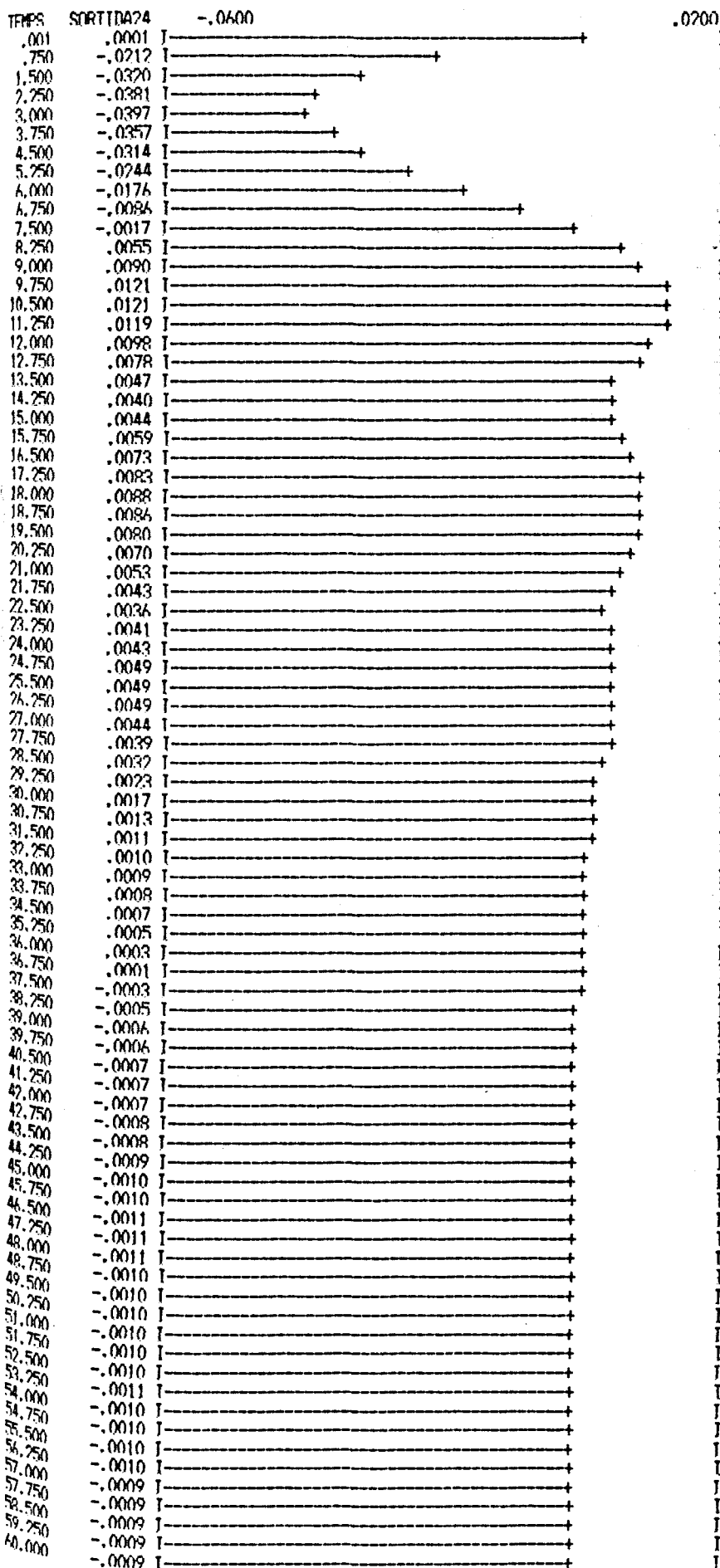
RLO discreto de acción simple con un retardo de 4 segundos en el cálculo de la acción de control ($T = 8$ segundos).

Ajustado con los valores obtenidos con el modelo continuo (caso $\textcircled{\text{I}}$ del Capítulo 5).

(simulación con el retardo de cálculo).

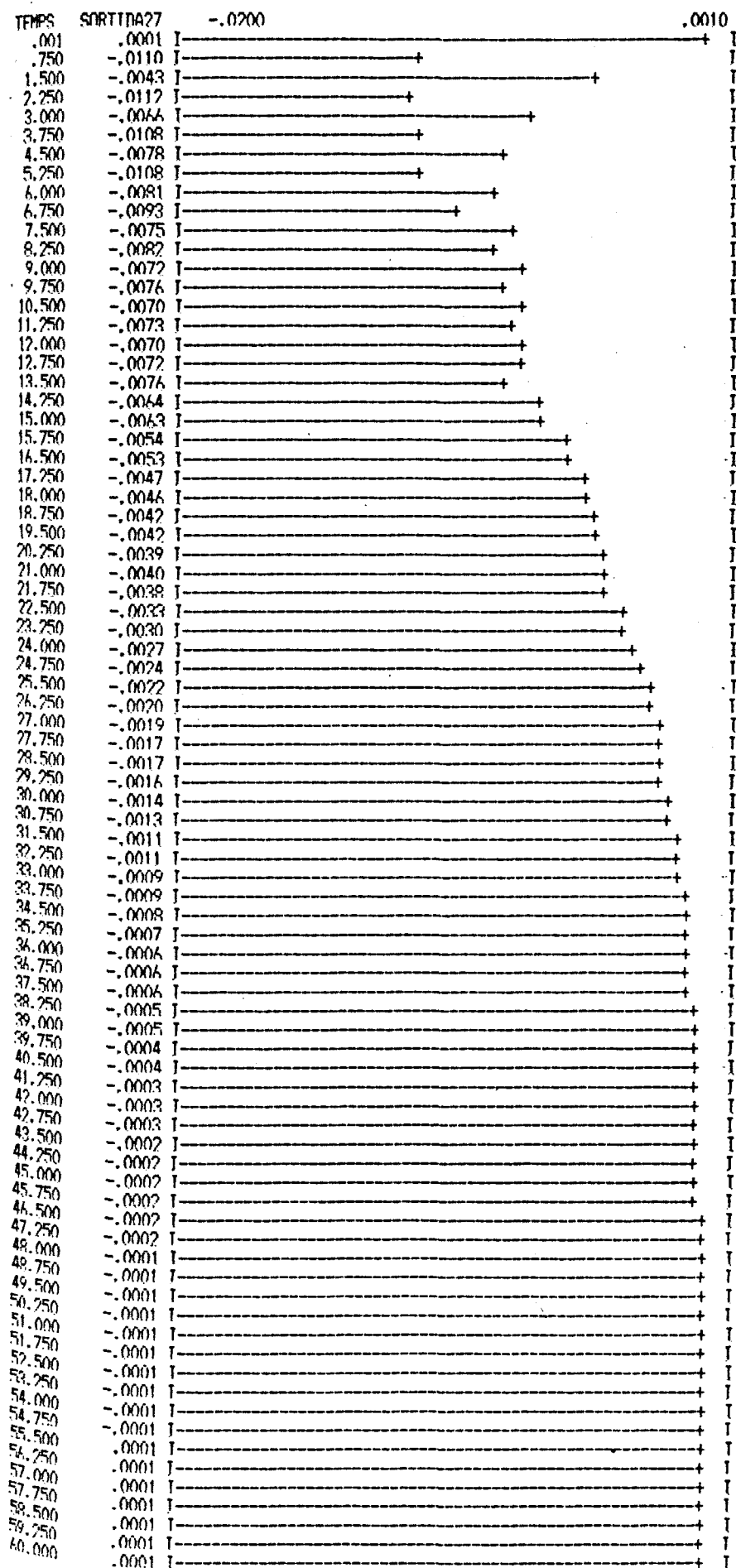
R.O.C. EIX Y (24) MINIM (-.0600) MAXIM (.0200)

SD7.1



RUC: EIX Y (27) MINIM (-.0200) MAXIM (.0010)

SD7.2



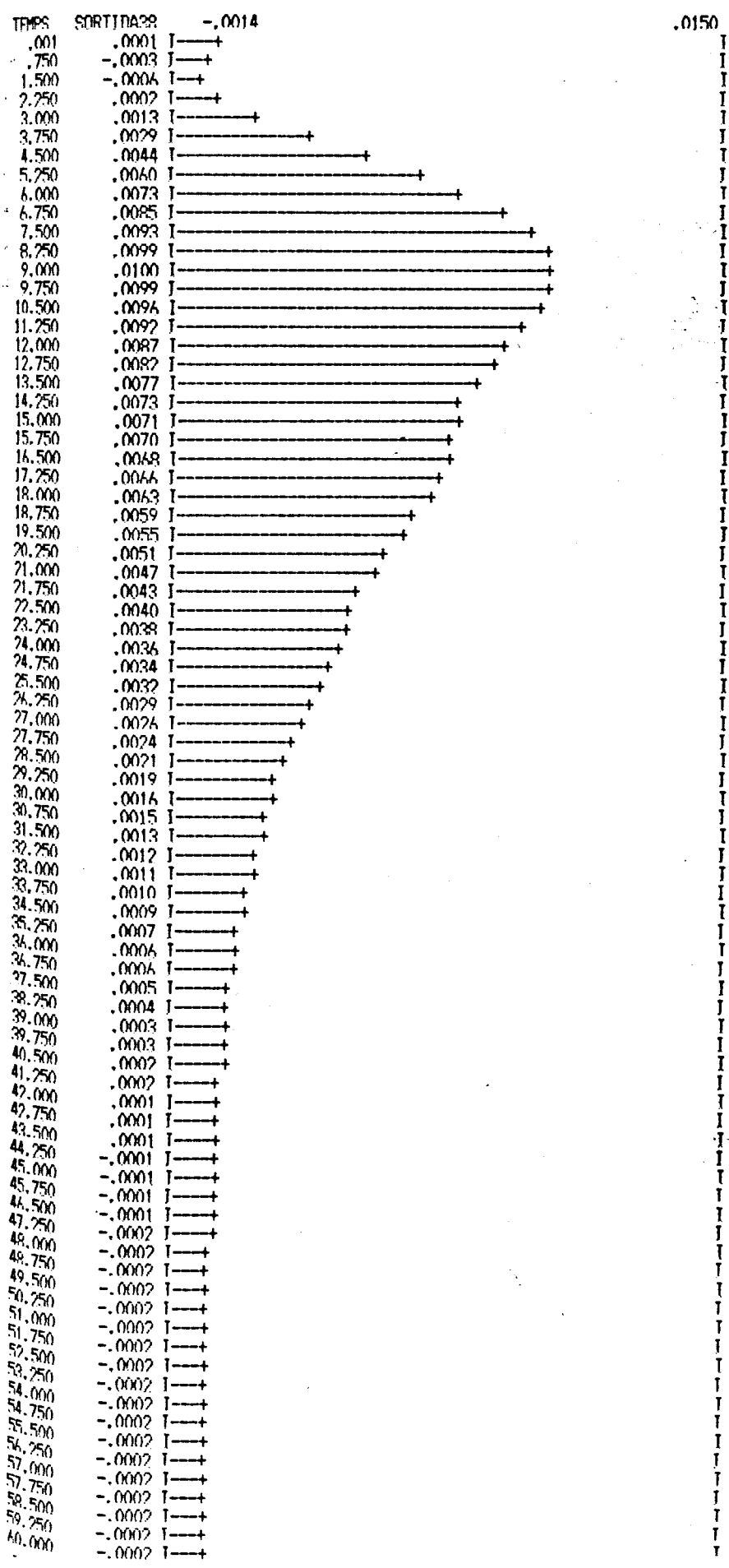
BLOC FIX Y (20) MJNTH (-.0007) MAYTH (.0150)

SD7.3

TEMPS	SORTIDA20	-.0007	.0150
.001	.0001	I+	I
.750	-.0003	I+	I
1.500	.0001	I+	I
2.250	.0004	I→+	I
3.000	.0010	I→+	I
3.750	.0015	I→+	I
4.500	.0019	I→+	I
5.250	.0016	I→+	I
6.000	.0025	I→+	I
6.750	.0031	I→+	I
7.500	.0035	I→+	I
8.250	.0035	I→+	I
9.000	.0034	I→+	I
9.750	.0032	I→+	I
10.500	.0030	I→+	I
11.250	.0029	I→+	I
12.000	.0027	I→+	I
12.750	.0022	I→+	I
13.500	.0024	I→+	I
14.250	.0035	I→+	I
15.000	.0043	I→+	I
15.750	.0049	I→+	I
16.500	.0053	I→+	I
17.250	.0056	I→+	I
18.000	.0057	I→+	I
18.750	.0058	I→+	I
19.500	.0059	I→+	I
20.250	.0060	I→+	I
21.000	.0057	I→+	I
21.750	.0062	I→+	I
22.500	.0068	I→+	I
23.250	.0073	I→+	I
24.000	.0076	I→+	I
24.750	.0078	I→+	I
25.500	.0080	I→+	I
26.250	.0081	I→+	I
27.000	.0082	I→+	I
27.750	.0083	I→+	I
28.500	.0083	I→+	I
29.250	.0083	I→+	I
30.000	.0084	I→+	I
30.750	.0088	I→+	I
31.500	.0089	I→+	I
32.250	.0091	I→+	I
33.000	.0092	I→+	I
33.750	.0092	I→+	I
34.500	.0093	I→+	I
35.250	.0094	I→+	I
36.000	.0094	I→+	I
36.750	.0094	I→+	I
37.500	.0095	I→+	I
38.250	.0096	I→+	I
39.000	.0096	I→+	I
39.750	.0096	I→+	I
40.500	.0097	I→+	I
41.250	.0097	I→+	I
42.000	.0098	I→+	I
42.750	.0098	I→+	I
43.500	.0098	I→+	I
44.250	.0098	I→+	I
45.000	.0099	I→+	I
45.750	.0099	I→+	I
46.500	.0099	I→+	I
47.250	.0099	I→+	I
48.000	.0099	I→+	I
48.750	.0100	I→+	I
49.500	.0100	I→+	I
50.250	.0100	I→+	I
51.000	.0100	I→+	I
51.750	.0100	I→+	I
52.500	.0100	I→+	I
53.250	.0100	I→+	I
54.000	.0100	I→+	I
54.750	.0100	I→+	I
55.500	.0100	I→+	I
56.250	.0100	I→+	I
57.000	.0100	I→+	I
57.750	.0101	I→+	I
58.500	.0101	I→+	I
59.250	.0101	I→+	I
60.000	.0101	I→+	I

BLDC FTX V (38) MINIM (-.0014) MAXIM (.0150)

SD7.4



SD7.5

TFMPS	SRRTDA4A	SRRTDA30	SRRTDA55	SRRTDA5A
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0658	-.0170	.0057	.0005
8.00	-.0838	.0032	.0059	.0006
10.00	-.0972	.0116	.0061	.0007
12.00	-.1092	.0102	.0063	.0008
14.00	-.1225	.0031	.0064	.0010
16.00	-.1336	.0062	.0065	.0010
18.00	-.1420	.0085	.0066	.0011
20.00	-.1489	.0072	.0067	.0011
22.00	-.1556	.0034	.0068	.0011
24.00	-.1610	.0043	.0068	.0012
26.00	-.1648	.0047	.0069	.0012
28.00	-.1677	.0034	.0069	.0012
30.00	-.1703	.0015	.0069	.0012
32.00	-.1725	.0010	.0069	.0012
34.00	-.1741	.0007	.0069	.0012
36.00	-.1754	.0003	.0069	.0012
38.00	-.1765	-.0005	.0069	.0012
40.00	-.1774	-.0007	.0069	.0012
42.00	-.1781	-.0008	.0069	.0012
44.00	-.1787	-.0009	.0069	.0012
46.00	-.1791	-.0011	.0069	.0012
48.00	-.1795	-.0011	.0069	.0012
50.00	-.1799	-.0010	.0069	.0012
52.00	-.1801	-.0010	.0069	.0012
54.00	-.1803	-.0011	.0069	.0012
56.00	-.1805	-.0010	.0070	.0012
58.00	-.1807	-.0009	.0070	.0012
60.00	-.1808	-.0009	.0070	.0012
62.00	-.1809	-.0009	.0070	.0012
64.00	-.1810	-.0008	.0070	.0012
66.00	-.1810	-.0007	.0070	.0012
68.00	-.1811	-.0007	.0070	.0012
70.00	-.1811	-.0007	.0070	.0012
72.00	-.1812	-.0006	.0070	.0012
74.00	-.1812	-.0006	.0070	.0012
76.00	-.1812	-.0005	.0070	.0012
78.00	-.1812	-.0005	.0070	.0012
80.00	-.1812	-.0005	.0070	.0012
82.00	-.1812	-.0004	.0070	.0012
84.00	-.1812	-.0004	.0070	.0012
86.00	-.1812	-.0004	.0070	.0012
88.00	-.1812	-.0004	.0070	.0012
90.00	-.1812	-.0003	.0070	.0012
92.00	-.1812	-.0003	.0070	.0012
94.00	-.1812	-.0003	.0070	.0012
96.00	-.1812	-.0003	.0070	.0012
98.00	-.1812	-.0003	.0070	.0012
100.00	-.1812	-.0002	.0070	.0012
102.00	-.1812	-.0002	.0070	.0012
104.00	-.1812	-.0002	.0070	.0012
106.00	-.1812	-.0002	.0070	.0012
108.00	-.1812	-.0002	.0070	.0012
110.00	-.1812	-.0002	.0070	.0012
112.00	-.1812	-.0002	.0070	.0012
114.00	-.1812	-.0002	.0070	.0012
116.00	-.1812	-.0001	.0070	.0012
118.00	-.1812	-.0001	.0070	.0012
120.00	-.1812	-.0001	.0070	.0012
122.00	-.1812	-.0001	.0070	.0012
124.00	-.1812	-.0001	.0070	.0012
126.00	-.1812	-.0001	.0070	.0012
128.00	-.1812	-.0001	.0070	.0012
130.00	-.1812	-.0001	.0070	.0012
132.00	-.1812	-.0001	.0070	.0012
134.00	-.1812	-.0001	.0070	.0012
136.00	-.1812	-.0001	.0070	.0012
138.00	-.1812	-.0001	.0070	.0012
140.00	-.1812	-.0001	.0070	.0012
142.00	-.1812	-.0001	.0070	.0012
144.00	-.1812	-.0001	.0070	.0012
146.00	-.1812	-.0001	.0070	.0012
148.00	-.1812	-.0001	.0070	.0012
150.00	-.1812	-.0001	.0070	.0012
152.00	-.1812	-.0001	.0070	.0012
154.00	-.1812	-.0001	.0070	.0012
156.00	-.1812	-.0001	.0070	.0012
158.00	-.1812	-.0001	.0070	.0012
160.00	-.1812	-.0001	.0070	.0012

SDD1

RLO de doble acción ($z = 4$, $T = 8$), $u(kT) = u(kT + z) =$ valores obtenidos con el modelo continuo (caso $\textcircled{\text{I}}$ del Capítulo 5).

(simulación con un retardo de cálculo de 1 segundo).

 ***** PROGRAMA DE SIMULACIÓ *****
 ***** DE SISTEMAS CONTINUS I DISCRETS *****

SDD1.1

CONFIGURACIÓ

BLOC	TIPUS	ENT. 1	ENT. 2	ENT. 3
1	K	0	0	0
2	W	3	24	5
3	R	66	35	49
4	G	2	0	0
5	I	4	0	0
7	G	5	0	0
8	+	7	9	0
9	G	12	0	0
10	G	9	0	0
11	I	10	0	0
12	+	5	-11	0
13	Z	41	58	0
14	Z	57	62	0
15	K	0	0	0
16	G	5	0	0
17	+	16	-21	0
18	G	17	0	0
19	I	17	0	0
20	+	19	-18	0
21	G	19	0	0
22	W	15	20	27
23	G	22	0	0
24	T	23	24	0
25	+	24	-30	0
26	G	25	0	0
27	I	26	0	0
28	+	27	38	0
29	G	28	0	0
30	J	29	30	0
31	G	40	0	0
32	I	31	32	0
33	G	32	0	0
34	+	33	-37	0
35	G	49	0	0
36	I	34	0	0
37	R	36	0	0
38	+	36	-34	0
39	X	27	27	0
40	+	-50	-30	0
41	W	5	9	20
42	W	24	46	27
43	+	13	14	0
44	G	24	0	0
45	+	44	27	0
46	J	45	0	0
47	I	66	0	0
48	X	24	24	0
49	Z	43	67	0
50	G	54	0	0
51	G	30	0	0
52	G	30	0	0
53	+	52	-27	0
54	I	53	0	0
55	I	48	0	0
56	I	39	0	0
57	+	42	51	0
58	T	59	-74	0
59	+	60	0	0
60	K	73	61	0
61	+	0	0	0
62	K	63	-74	0
63	T	65	0	0
64	+	0	0	0
65	K	73	-64	0
66	R	75	61	1
67	+	68	-74	0
68	T	70	0	0
69	K	0	0	0
70	+	73	-69	0
73	I	1	0	0
74	K	0	0	0
75	X	47	67	0

(Modelo de simulaci3n)

CONDITIONS INICIALS I PARAMETRES

SDD1.2

BLCC	CI/PAR 1	PAR 2	PAR 3
1	1.0000	0.0000	0.0000
2	-1.0000	-1.0000	-1.0000
4	.0377	0.0000	0.0000
7	12.9700	0.0000	0.0000
9	5.3518	0.0000	0.0000
10	.0509	0.0000	0.0000
13	0.0000	.0325	0.0000
14	0.0000	-.1422	0.0000
15	.0100	0.0000	0.0000
16	2.0746	0.0000	0.0000
18	.9440	0.0000	0.0000
21	2.0746	0.0000	0.0000
22	-1.0000	1.0000	-1.0000
23	6.2500	0.0000	0.0000
24	0.0000	-.0937	0.0000
26	1.5300	0.0000	0.0000
29	6.2490	0.0000	0.0000
30	0.0000	-1.2343	0.0000
31	.0525	0.0000	0.0000
32	0.0000	-.0295	0.0000
33	2.0000	0.0000	0.0000
35	.7600	0.0000	0.0000
37	2.0000	0.0000	0.0000
39	12.0000	-2.9750	0.0000
41	2.9250	-.1756	.3229
42	.1081	-.6629	-.0015
44	.0920	0.0000	0.0000
47	0.0000	-2.0000	1.0000
49	0.0000	-.1297	0.0000
50	.0200	0.0000	0.0000
51	-.0005	0.0000	0.0000
52	1.9475	0.0000	0.0000
55	0.0000	-.0100	-.0100
59	8.0000	-1.9750	0.0000
61	-2.0000	0.0000	0.0000
63	8.0000	-3.9750	0.0000
64	4.0000	0.0000	0.0000
66	1.7770	-2.6666	0.0000
68	4.0000	-.9750	0.0000
69	5.0000	0.0000	0.0000
72	13.0000	0.0000	0.0000
74	.0100	0.0000	0.0000
75	40.0000	0.0000	0.0000

SDD1.3

TEMPS	SORTIDA44	SORTIDA30	SORTIDA55	SORTIDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0657	-.0172	.0057	.0005
8.00	-.0847	.0011	.0059	.0006
10.00	-.0987	.0114	.0061	.0008
12.00	-.1108	.0108	.0063	.0009
14.00	-.1239	.0036	.0065	.0010
16.00	-.1362	.0046	.0065	.0011
18.00	-.1449	.0087	.0066	.0011
20.00	-.1518	.0082	.0068	.0011
22.00	-.1583	.0044	.0068	.0012
24.00	-.1640	.0038	.0069	.0012
26.00	-.1678	.0050	.0069	.0012
28.00	-.1704	.0042	.0070	.0012
30.00	-.1727	.0021	.0070	.0012
32.00	-.1747	.0009	.0070	.0012
34.00	-.1761	.0006	.0070	.0012
36.00	-.1771	.0004	.0070	.0012
38.00	-.1779	-.0003	.0070	.0012
40.00	-.1786	-.0008	.0070	.0012
42.00	-.1792	-.0010	.0070	.0012
44.00	-.1795	-.0010	.0070	.0012
46.00	-.1798	-.0011	.0070	.0012
48.00	-.1801	-.0013	.0070	.0012
50.00	-.1804	-.0013	.0070	.0012
52.00	-.1805	-.0011	.0070	.0012
54.00	-.1807	-.0011	.0070	.0012
56.00	-.1808	-.0011	.0070	.0012
58.00	-.1810	-.0011	.0070	.0012
60.00	-.1810	-.0009	.0070	.0012
62.00	-.1811	-.0009	.0070	.0012
64.00	-.1812	-.0008	.0070	.0012
66.00	-.1812	-.0007	.0070	.0012
68.00	-.1812	-.0007	.0070	.0012
70.00	-.1812	-.0007	.0070	.0012
72.00	-.1813	-.0007	.0070	.0012
74.00	-.1813	-.0005	.0070	.0012
76.00	-.1813	-.0005	.0070	.0012
78.00	-.1812	-.0005	.0070	.0012
80.00	-.1813	-.0005	.0070	.0012
82.00	-.1813	-.0004	.0070	.0012
84.00	-.1813	-.0004	.0070	.0012
86.00	-.1812	-.0004	.0070	.0012
88.00	-.1813	-.0004	.0070	.0012
90.00	-.1813	-.0003	.0070	.0012
92.00	-.1812	-.0003	.0070	.0012
94.00	-.1812	-.0003	.0070	.0012
96.00	-.1813	-.0003	.0070	.0012
98.00	-.1813	-.0002	.0070	.0012
100.00	-.1812	-.0002	.0070	.0012

SDD2

RLO de doble acción ($\zeta = 4$, $T = 8$).

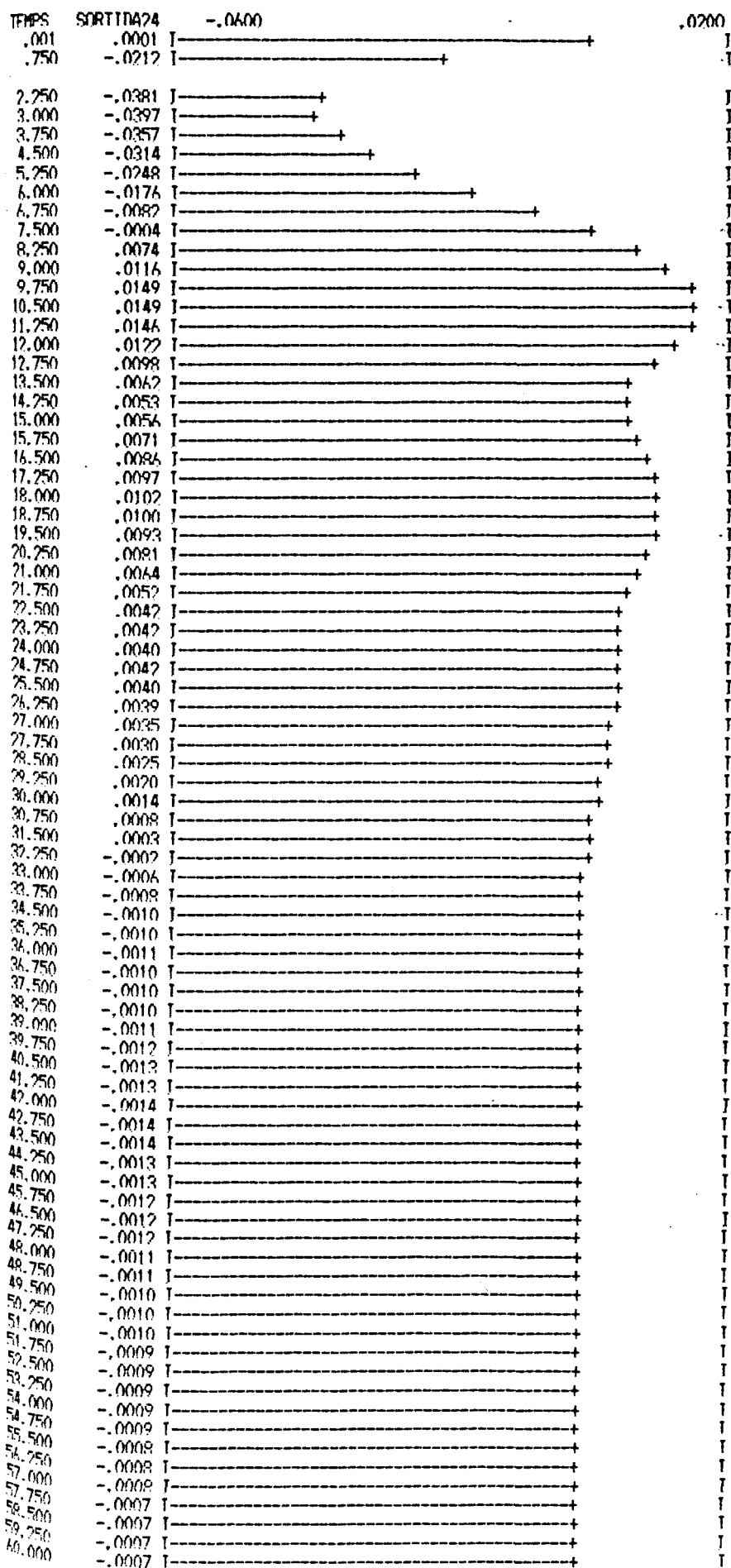
Penalización continua, sin importar el esfuerzo de control
en $kT + \zeta$

(simulación con un retardo de cálculo de 1 segundo).

FMPS	SRRTDA44	SRRTDA30	SRRTDA55	SRRTDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0349	.0043	.0003
6.00	-.0659	-.0174	.0057	.0005
8.00	-.0832	.0049	.0059	.0006
10.00	-.0951	.0144	.0062	.0007
12.00	-.1052	.0126	.0066	.0008
14.00	-.1165	.0043	.0067	.0009
16.00	-.1255	.0074	.0068	.0009
18.00	-.1313	.0099	.0070	.0010
20.00	-.1354	.0084	.0072	.0010
22.00	-.1394	.0044	.0073	.0010
24.00	-.1422	.0039	.0073	.0010
26.00	-.1439	.0038	.0073	.0010
28.00	-.1448	.0028	.0074	.0010
30.00	-.1454	.0013	.0074	.0010
32.00	-.1459	-.0002	.0074	.0010
34.00	-.1464	-.0009	.0074	.0010
36.00	-.1468	-.0011	.0074	.0010
38.00	-.1471	-.0010	.0074	.0010
40.00	-.1473	-.0012	.0074	.0010
42.00	-.1476	-.0014	.0074	.0010
44.00	-.1478	-.0013	.0074	.0010
46.00	-.1480	-.0012	.0074	.0010
48.00	-.1482	-.0011	.0074	.0010
50.00	-.1484	-.0010	.0074	.0010
52.00	-.1485	-.0009	.0074	.0010
54.00	-.1486	-.0009	.0074	.0010
56.00	-.1488	-.0008	.0074	.0010
58.00	-.1488	-.0007	.0074	.0010
60.00	-.1489	-.0007	.0074	.0010
62.00	-.1489	-.0007	.0074	.0010
64.00	-.1489	-.0006	.0074	.0010
66.00	-.1490	-.0006	.0074	.0010
68.00	-.1490	-.0005	.0074	.0010
70.00	-.1490	-.0005	.0074	.0010
72.00	-.1490	-.0005	.0074	.0010
74.00	-.1490	-.0004	.0074	.0010
76.00	-.1490	-.0004	.0074	.0010
78.00	-.1490	-.0004	.0074	.0010
80.00	-.1490	-.0004	.0074	.0010
82.00	-.1489	-.0003	.0074	.0010
84.00	-.1489	-.0003	.0074	.0010
86.00	-.1489	-.0003	.0074	.0010
88.00	-.1489	-.0003	.0074	.0010
90.00	-.1489	-.0003	.0074	.0010
92.00	-.1489	-.0002	.0074	.0010
94.00	-.1489	-.0002	.0074	.0010
96.00	-.1489	-.0002	.0074	.0010
98.00	-.1489	-.0002	.0074	.0010
100.00	-.1489	-.0002	.0074	.0010
102.00	-.1489	-.0002	.0074	.0010
104.00	-.1489	-.0002	.0074	.0010
106.00	-.1489	-.0001	.0074	.0010
108.00	-.1489	-.0001	.0074	.0010
110.00	-.1489	-.0001	.0074	.0010
112.00	-.1489	-.0001	.0074	.0010
114.00	-.1489	-.0001	.0074	.0010
116.00	-.1489	-.0001	.0074	.0010
118.00	-.1489	-.0001	.0074	.0010
120.00	-.1489	-.0001	.0074	.0010
122.00	-.1489	-.0001	.0074	.0010
124.00	-.1489	-.0001	.0074	.0010
126.00	-.1489	-.0001	.0074	.0010
128.00	-.1489	-.0001	.0074	.0010
130.00	-.1489	-.0001	.0074	.0010
132.00	-.1489	-.0001	.0074	.0010
134.00	-.1489	-.0001	.0074	.0010
136.00	-.1489	-.0001	.0074	.0010
138.00	-.1489	-.0001	.0074	.0010
140.00	-.1489	-.0001	.0074	.0010
142.00	-.1489	-.0001	.0074	.0010
144.00	-.1489	-.0001	.0074	.0010
146.00	-.1489	-.0001	.0074	.0010
148.00	-.1489	-.0001	.0074	.0010
150.00	-.1489	-.0001	.0074	.0010
152.00	-.1489	-.0001	.0074	.0010
154.00	-.1489	-.0001	.0074	.0010
156.00	-.1489	-.0001	.0074	.0010
158.00	-.1489	-.0001	.0074	.0010
160.00	-.1489	-.0001	.0074	.0010

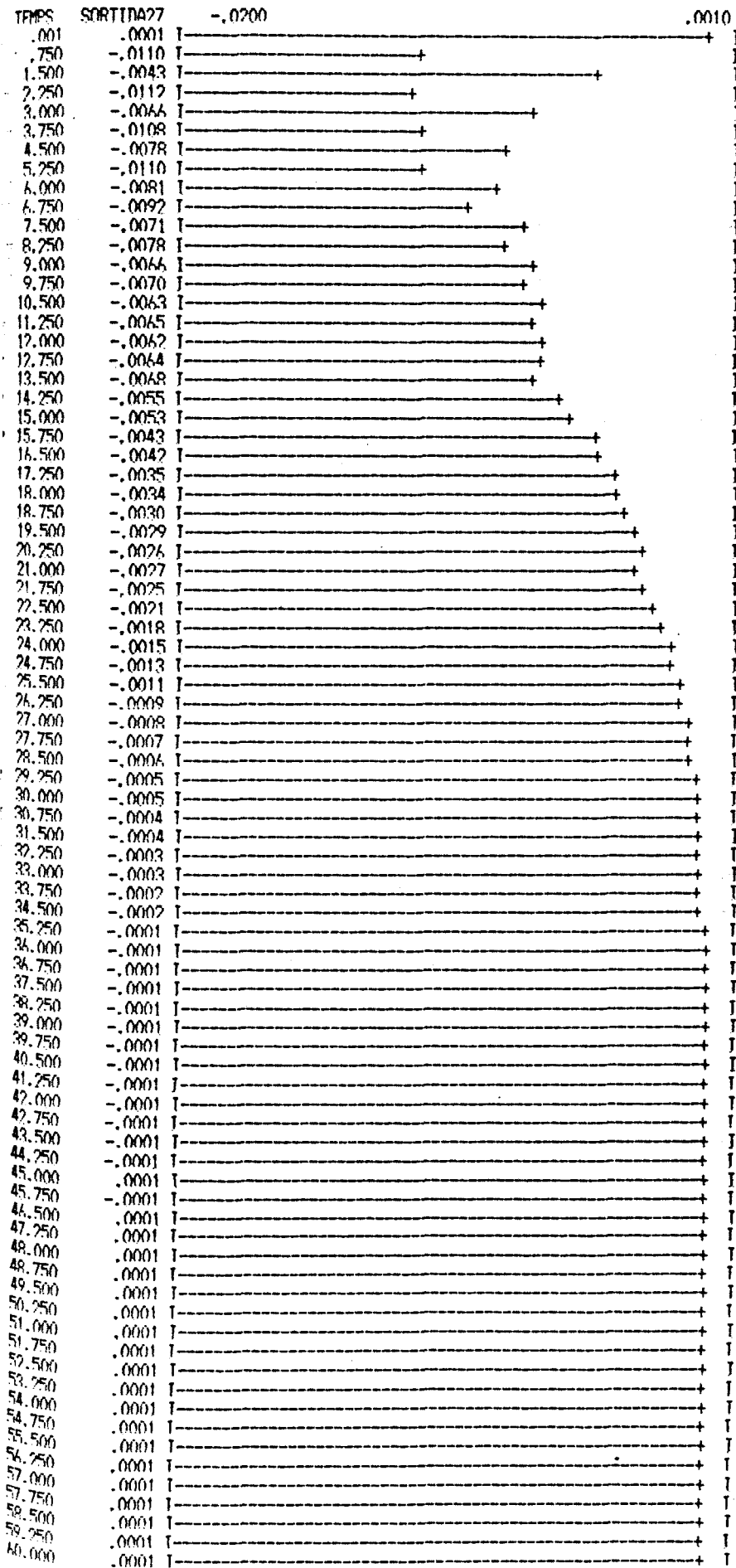
RDC FIX Y (24) MINIM (-.0600) MAXIM (.0200)

SDD2.2



RUC: FTX Y (27) MINIM (-.0200) MAXIM (.0010)

SDD2.3

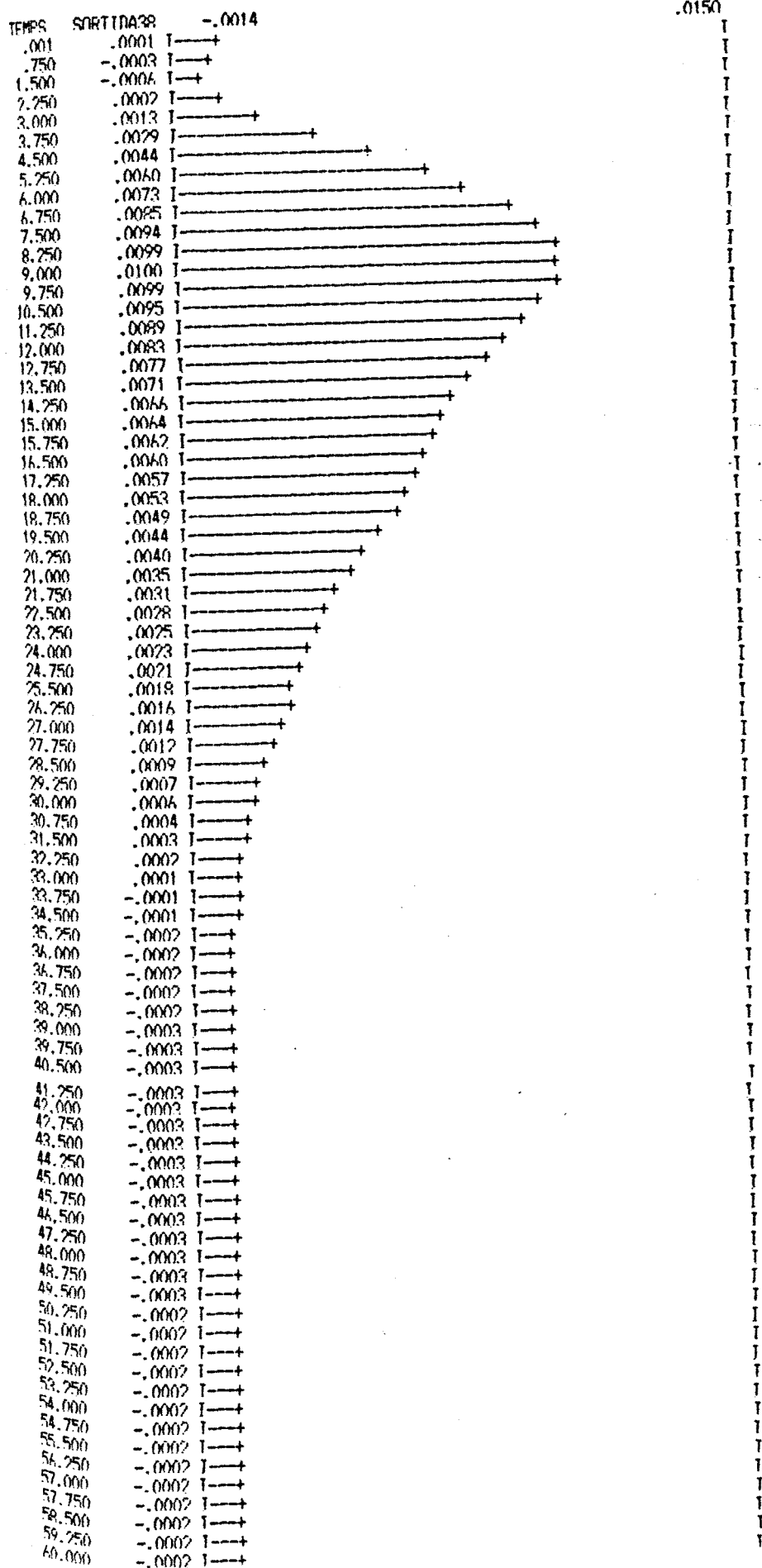


RUC FTY Y (20) MINIM (-.0007) MAXIM (.0150)

SDD2.4

TEMPS	SOBTIDA20	-.0007	.0150
.001	.0001	I+	I
.750	-.0003	I+	I
1.500	.0001	I+	I
2.250	.0004	I+	I
3.000	.0010	I+	I
3.750	.0015	I+	I
4.500	.0019	I+	I
5.250	.0014	I+	I
6.000	.0026	I+	I
6.750	.0035	I+	I
7.500	.0040	I+	I
8.250	.0042	I+	I
9.000	.0041	I+	I
9.750	.0040	I+	I
10.500	.0038	I+	I
11.250	.0036	I+	I
12.000	.0035	I+	I
12.750	.0029	I+	I
13.500	.0032	I+	I
14.250	.0043	I+	I
15.000	.0053	I+	I
15.750	.0060	I+	I
16.500	.0065	I+	I
17.250	.0068	I+	I
18.000	.0070	I+	I
18.750	.0071	I+	I
19.500	.0072	I+	I
20.250	.0073	I+	I
21.000	.0071	I+	I
21.750	.0075	I+	I
22.500	.0080	I+	I
23.250	.0084	I+	I
24.000	.0086	I+	I
24.750	.0089	I+	I
25.500	.0090	I+	I
26.250	.0092	I+	I
27.000	.0093	I+	I
27.750	.0093	I+	I
28.500	.0094	I+	I
29.250	.0095	I+	I
30.000	.0095	I+	I
30.750	.0096	I+	I
31.500	.0096	I+	I
32.250	.0097	I+	I
33.000	.0098	I+	I
33.750	.0098	I+	I
34.500	.0099	I+	I
35.250	.0099	I+	I
36.000	.0100	I+	I
36.750	.0100	I+	I
37.500	.0100	I+	I
38.250	.0100	I+	I
39.000	.0100	I+	I
39.750	.0100	I+	I
40.500	.0100	I+	I
41.250	.0100	I+	I
42.000	.0100	I+	I
42.750	.0100	I+	I
43.500	.0100	I+	I
44.250	.0100	I+	I
45.000	.0100	I+	I
45.750	.0100	I+	I
46.500	.0100	I+	I
47.250	.0100	I+	I
48.000	.0100	I+	I
48.750	.0101	I+	I
49.500	.0101	I+	I
50.250	.0101	I+	I
51.000	.0101	I+	I
51.750	.0101	I+	I
52.500	.0101	I+	I
53.250	.0100	I+	I
54.000	.0100	I+	I
54.750	.0101	I+	I
55.500	.0101	I+	I
56.250	.0101	I+	I
57.000	.0101	I+	I
57.750	.0101	I+	I
58.500	.0101	I+	I
59.250	.0101	I+	I
60.000	.0101	I+	I

PLANE FIX Y (38) MINIM (-.0014) MAXIM (.0150)



SDD3

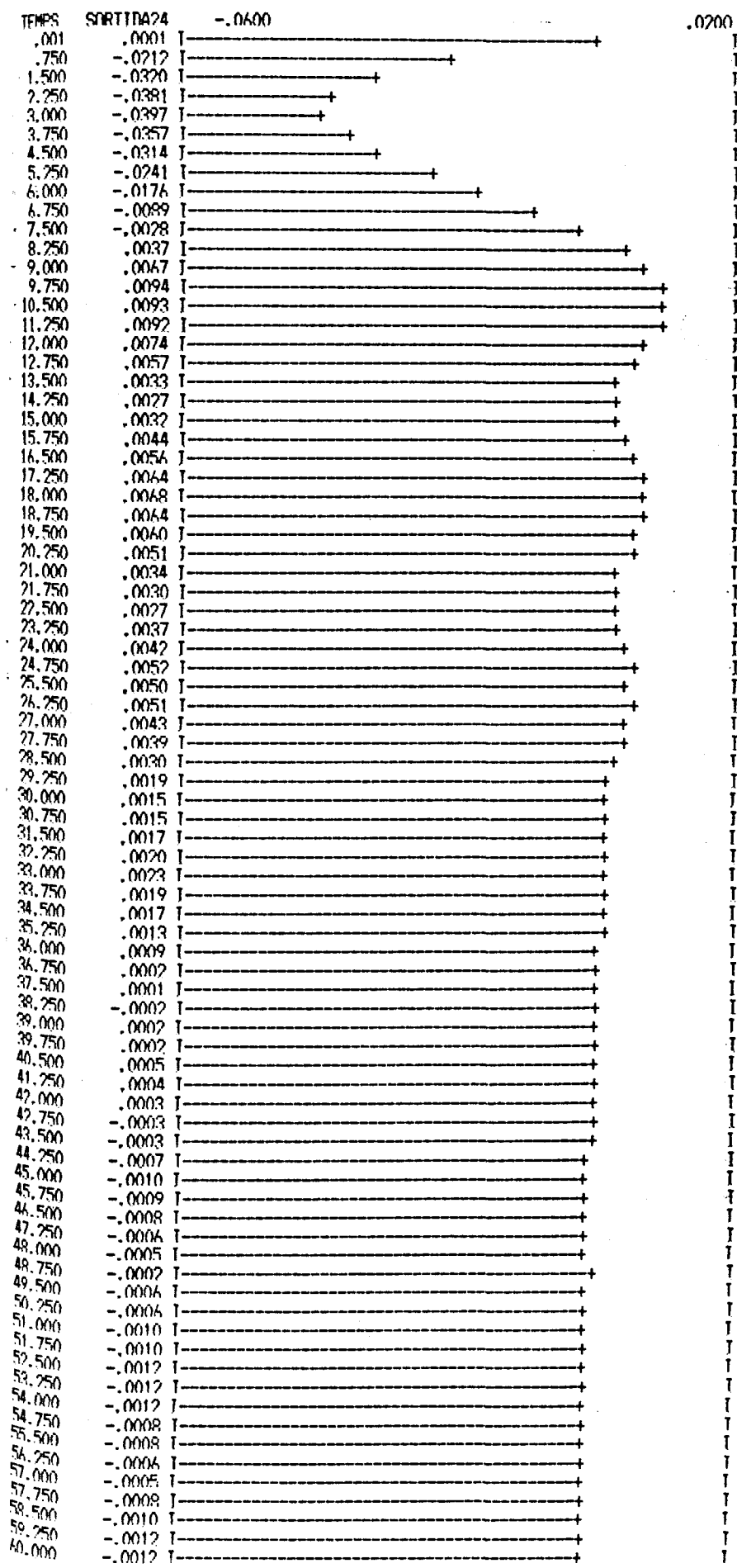
RLO de doble acción ($\mathcal{U} = 4$, $T = 8$).

Penalización continua, importando tanto el esfuerzo en kT como en $kT + \mathcal{U}$.

(simulación con un retardo de cálculo de 1 segundo).

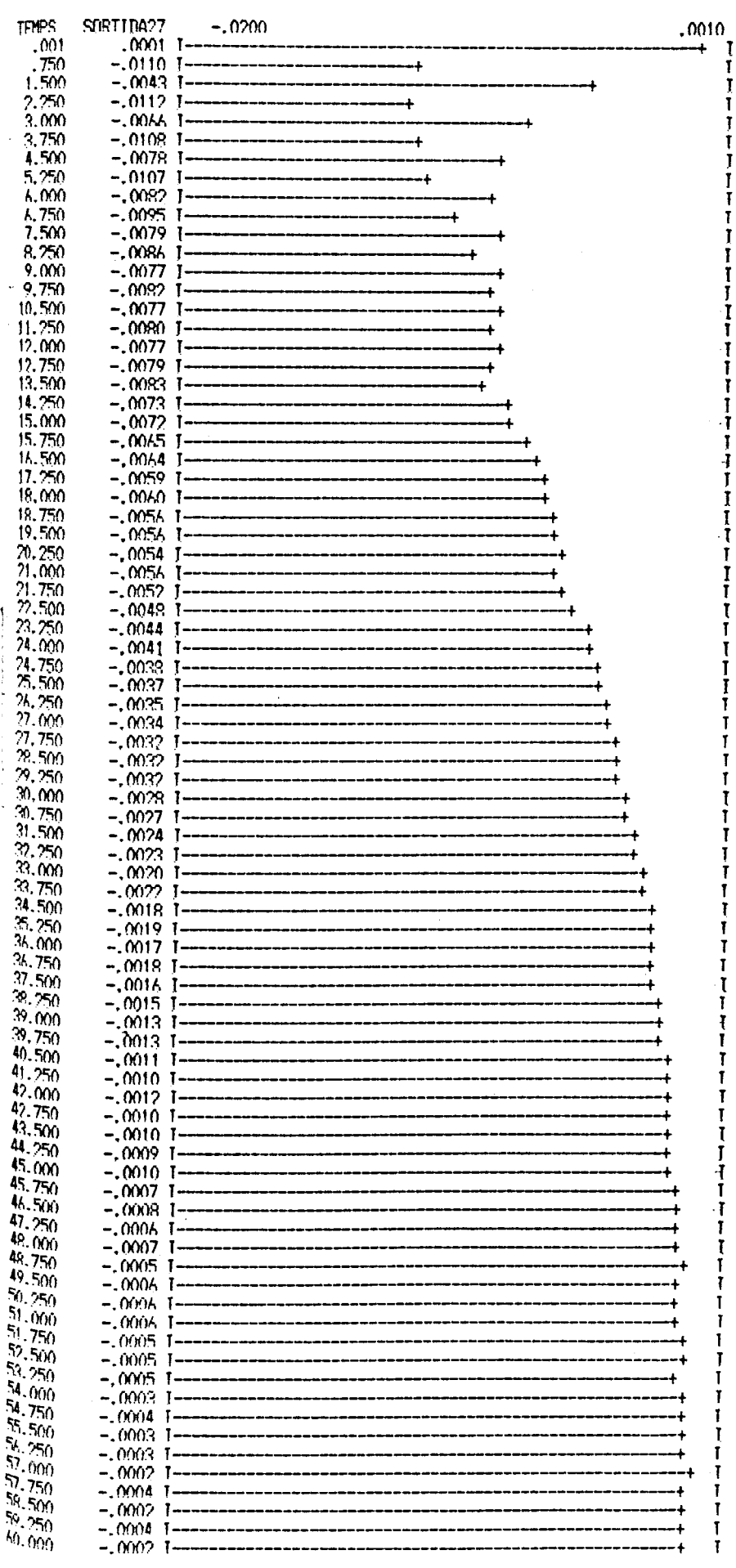
RUC FIX Y (24) MINIM (-.0600) MAXIM (.0200)

SDD3.1



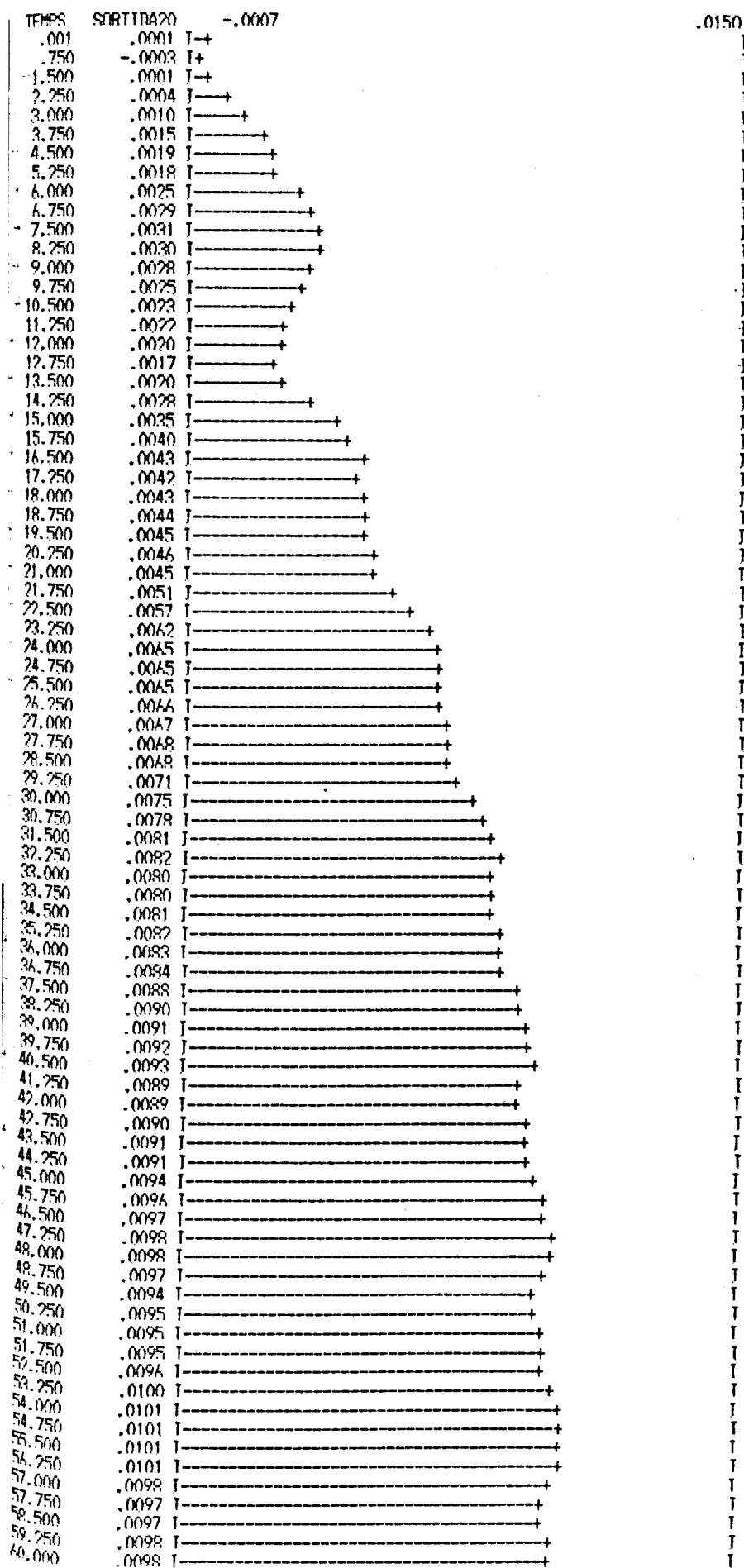
R:DC:FIX Y (??) MINIM (-.0200) MAXIM (.0010)

SDD3.2



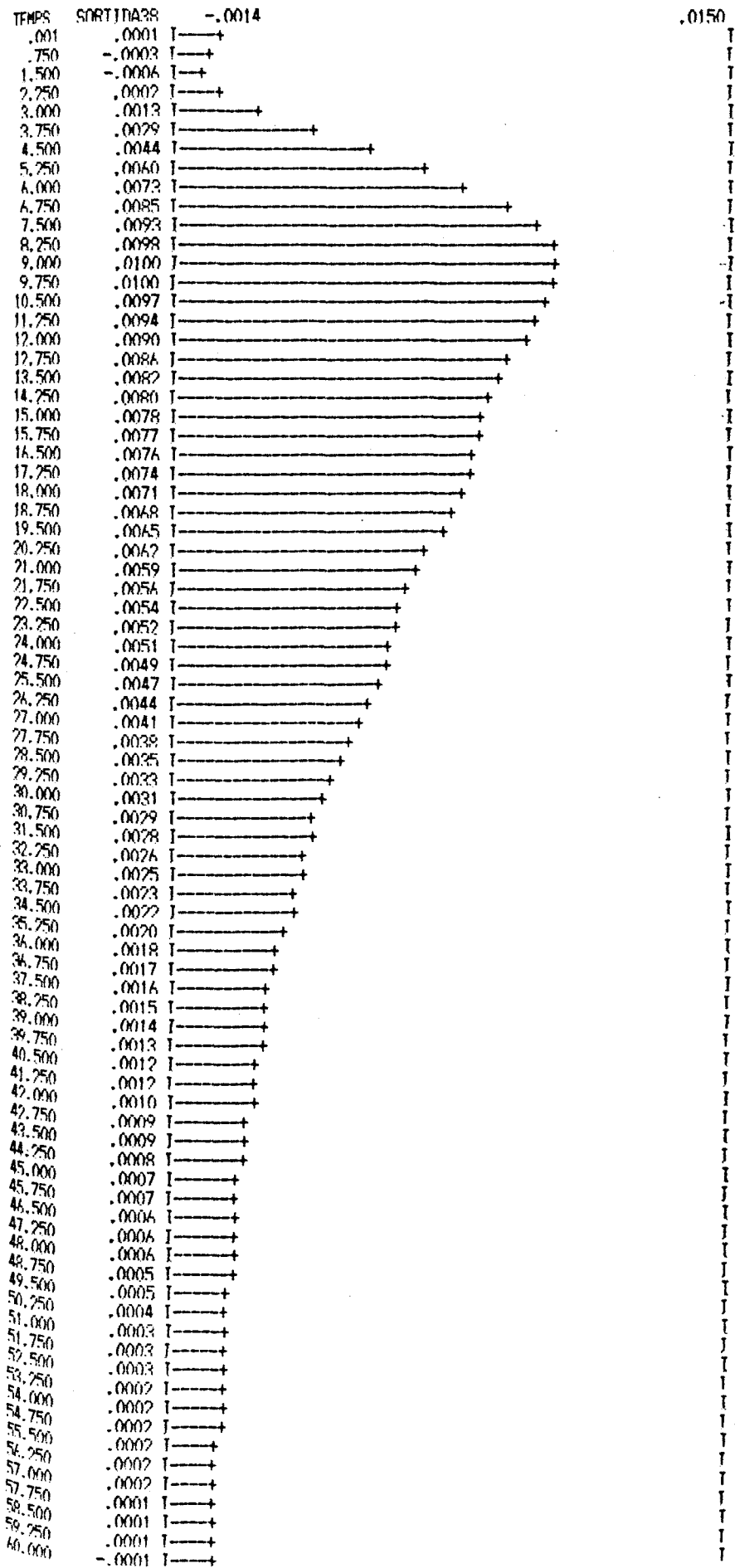
PLC ETX Y (20) MINIM (-.0007) MAXIM (.0150)

SDD3.3



R OF FIX Y (38) MTNTM (-.0014) MAXTM (.0150)

SDD3.4



SDD3.5

TEMPS	SRRTDA4A	SRRTDA30	SRRTDA55	SRRTDA56
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0656	-.0167	.0057	.0005
8.00	-.0842	.0016	.0059	.0006
10.00	-.0991	.0089	.0060	.0008
12.00	-.1130	.0079	.0062	.0009
14.00	-.1281	.0021	.0062	.0010
16.00	-.1414	.0047	.0062	.0011
18.00	-.1525	.0064	.0063	.0012
20.00	-.1625	.0053	.0064	.0013
22.00	-.1726	.0023	.0064	.0013
24.00	-.1809	.0042	.0064	.0014
26.00	-.1875	.0048	.0065	.0014
28.00	-.1933	.0035	.0065	.0014
30.00	-.1990	.0013	.0065	.0014
32.00	-.2038	.0018	.0065	.0014
34.00	-.2076	.0017	.0065	.0014
36.00	-.2109	.0008	.0065	.0014
38.00	-.2142	-.0001	.0065	.0015
40.00	-.2168	.0003	.0065	.0015
42.00	-.2189	.0001	.0065	.0015
44.00	-.2208	-.0006	.0065	.0015
46.00	-.2227	-.0008	.0065	.0015
48.00	-.2241	-.0005	.0065	.0015
50.00	-.2252	-.0008	.0065	.0015
52.00	-.2263	-.0011	.0066	.0015
54.00	-.2274	-.0010	.0066	.0015
56.00	-.2281	-.0007	.0066	.0015
58.00	-.2287	-.0010	.0066	.0015
60.00	-.2294	-.0012	.0066	.0015
62.00	-.2301	-.0009	.0066	.0015
64.00	-.2304	-.0006	.0066	.0015
66.00	-.2307	-.0009	.0066	.0015
68.00	-.2312	-.0011	.0066	.0015
70.00	-.2315	-.0008	.0066	.0015
72.00	-.2317	-.0005	.0066	.0015
74.00	-.2318	-.0008	.0066	.0015
76.00	-.2321	-.0010	.0066	.0015
78.00	-.2324	-.0006	.0066	.0015
80.00	-.2324	-.0003	.0066	.0015
82.00	-.2324	-.0007	.0066	.0015
84.00	-.2326	-.0009	.0066	.0015
86.00	-.2328	-.0005	.0066	.0015
88.00	-.2328	-.0002	.0066	.0015
90.00	-.2327	-.0006	.0066	.0015
92.00	-.2329	-.0008	.0066	.0015
94.00	-.2330	-.0003	.0066	.0015
96.00	-.2330	-.0001	.0066	.0015
98.00	-.2329	-.0005	.0066	.0015
100.00	-.2331	-.0007	.0066	.0015
102.00	-.2331	-.0002	.0066	.0015
104.00	-.2331	-.0001	.0066	.0015
106.00	-.2330	-.0004	.0066	.0015
108.00	-.2332	-.0005	.0066	.0015
110.00	-.2333	-.0001	.0066	.0015
112.00	-.2332	.0001	.0066	.0015
114.00	-.2331	-.0003	.0066	.0015
116.00	-.2333	-.0005	.0066	.0015
118.00	-.2333	-.0001	.0066	.0015
120.00	-.2332	.0002	.0066	.0015
122.00	-.2332	-.0003	.0066	.0015
124.00	-.2333	-.0004	.0066	.0015
126.00	-.2334	.0001	.0066	.0015
128.00	-.2333	.0002	.0066	.0015
130.00	-.2332	-.0003	.0066	.0015
132.00	-.2334	-.0004	.0066	.0015
134.00	-.2334	.0001	.0066	.0015
136.00	-.2333	.0003	.0066	.0015
138.00	-.2333	-.0002	.0066	.0015
140.00	-.2334	-.0004	.0066	.0015
142.00	-.2334	.0001	.0066	.0015
144.00	-.2333	.0003	.0066	.0015
146.00	-.2333	-.0002	.0066	.0015
148.00	-.2334	-.0004	.0066	.0015
150.00	-.2334	.0001	.0066	.0015
152.00	-.2333	.0003	.0066	.0015
154.00	-.2333	-.0002	.0066	.0015
156.00	-.2334	-.0004	.0066	.0015
158.00	-.2334	.0002	.0066	.0015
160.00	-.2333	.0003	.0066	.0015

SDD4

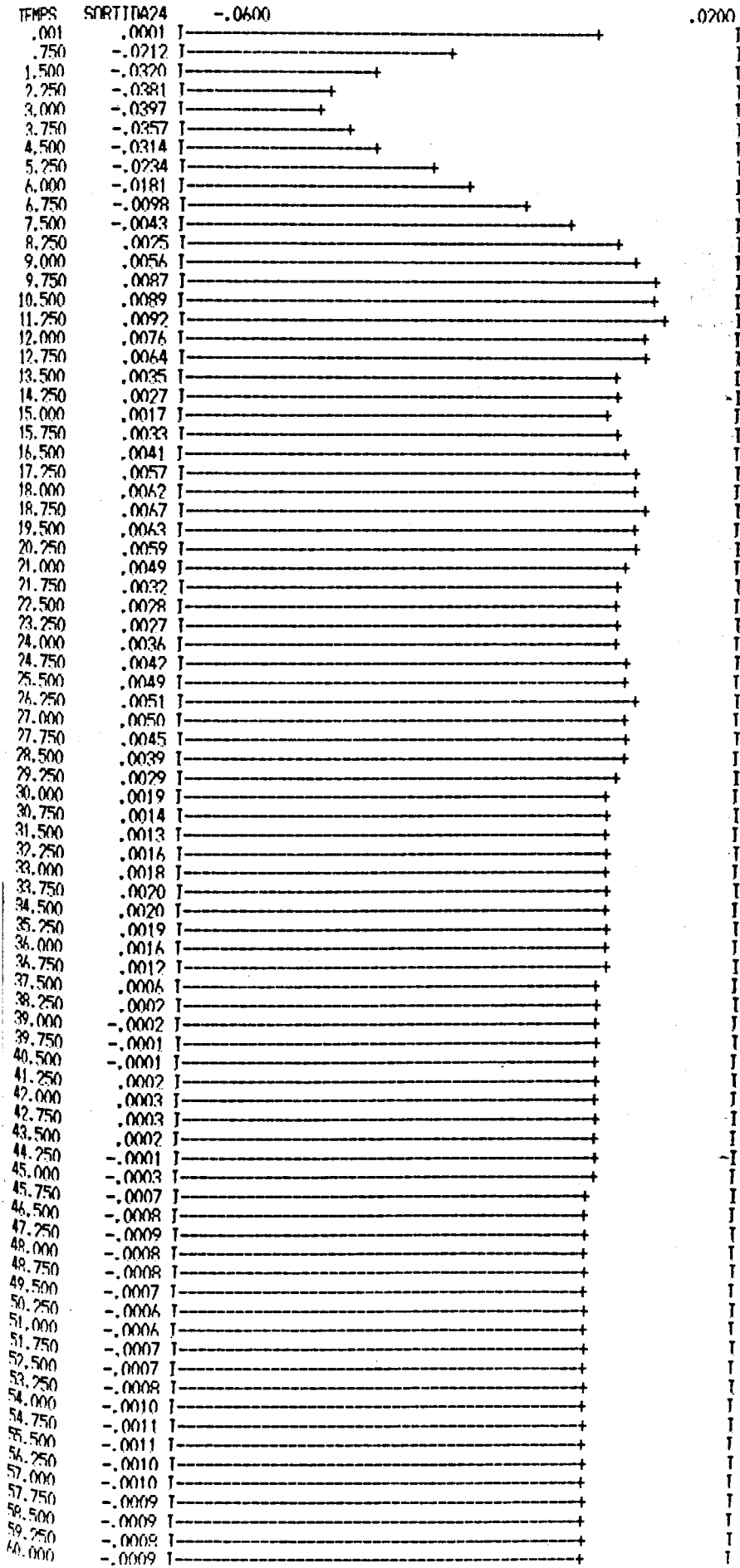
RLO de doble acción ($\mathcal{Z} = 4, T = 8$).

Penalización de las desviaciones y del esfuerzo de control solamente en kT (penalización discreta).

(simulación con un retardo de cálculo de 1 segundo).

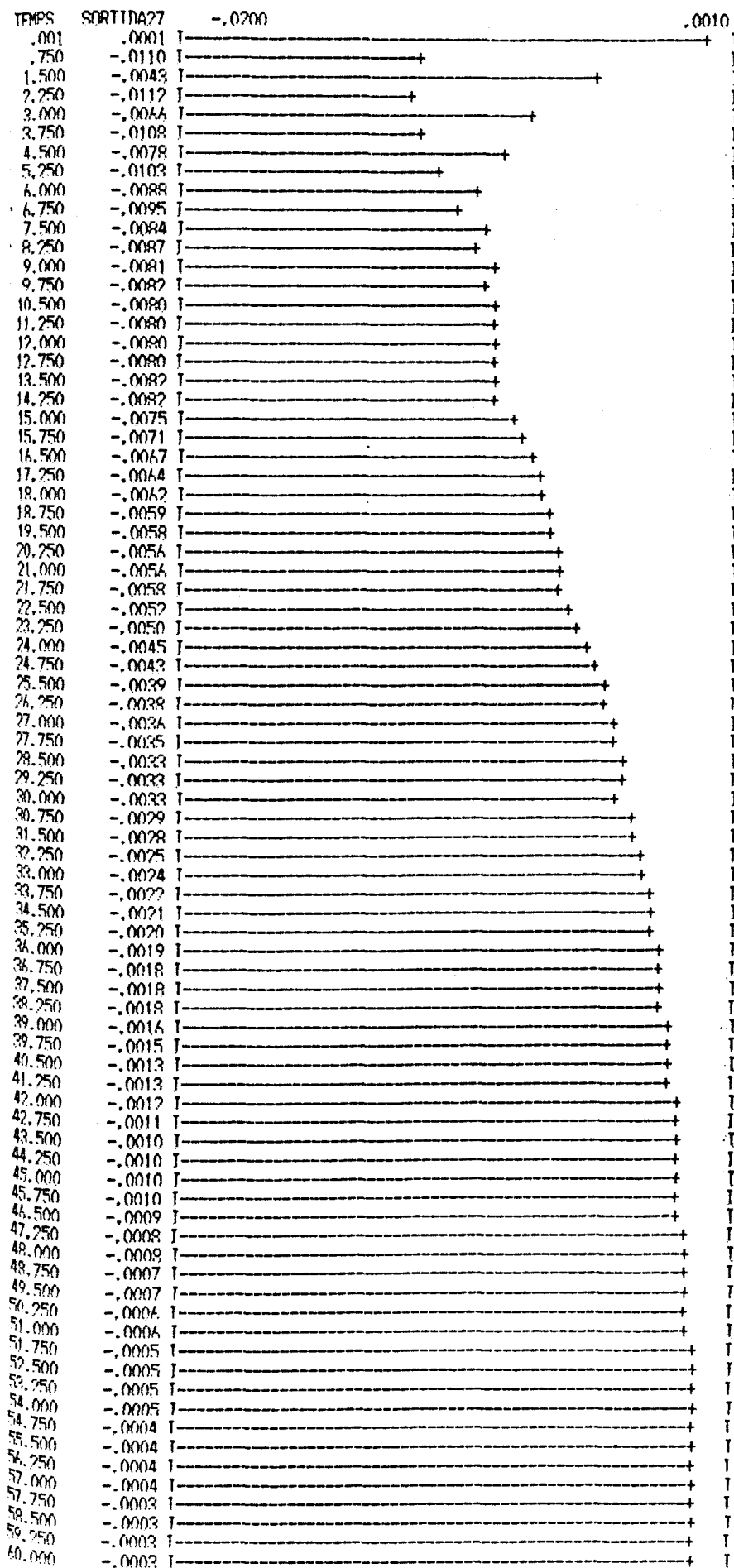
BLOC FIX Y (24) MINIM (-.0600) MAXIM (.0200)

SDD4.1



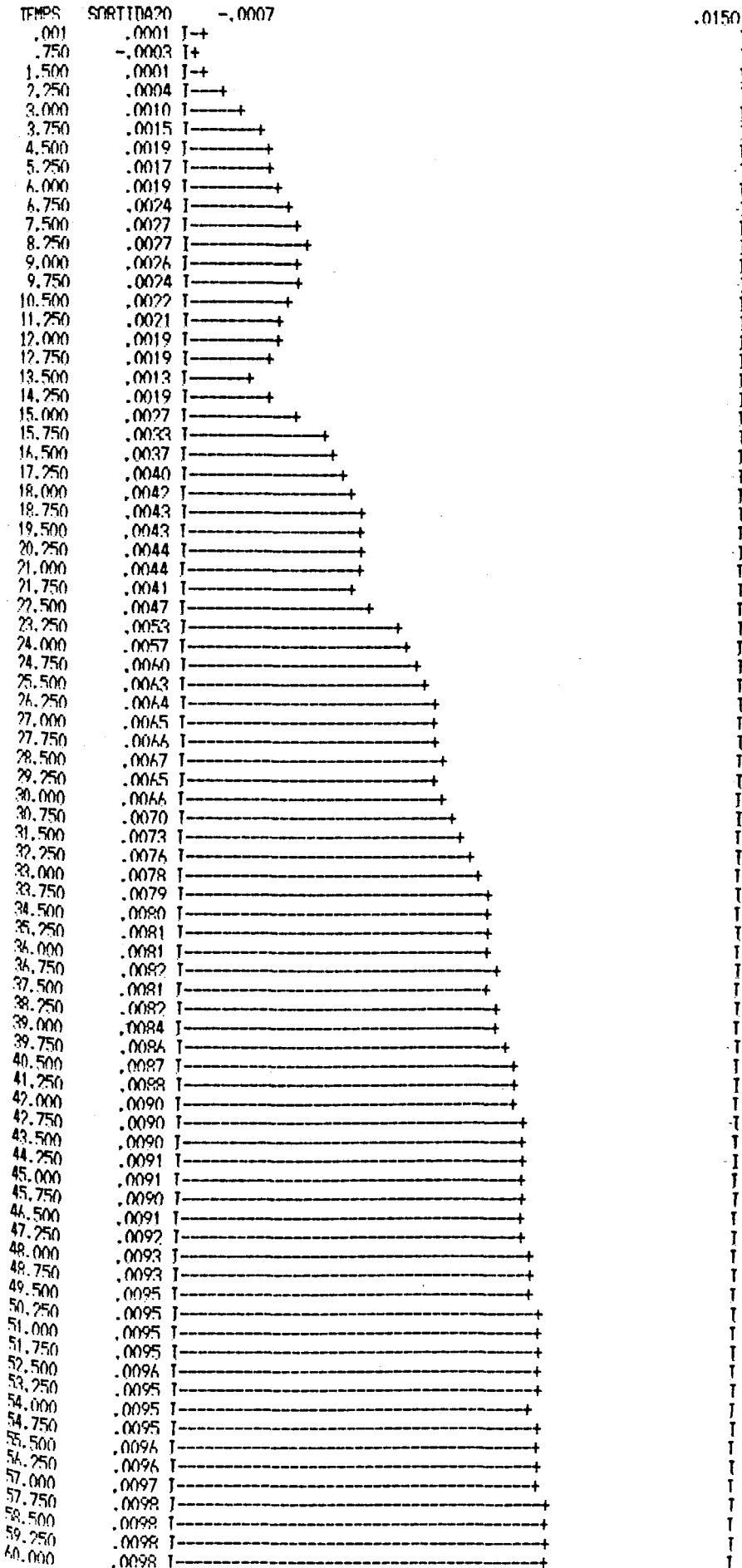
BI DE FIX V (27) MINIM (-.0200) MAXIM (.0010)

SDD4.2



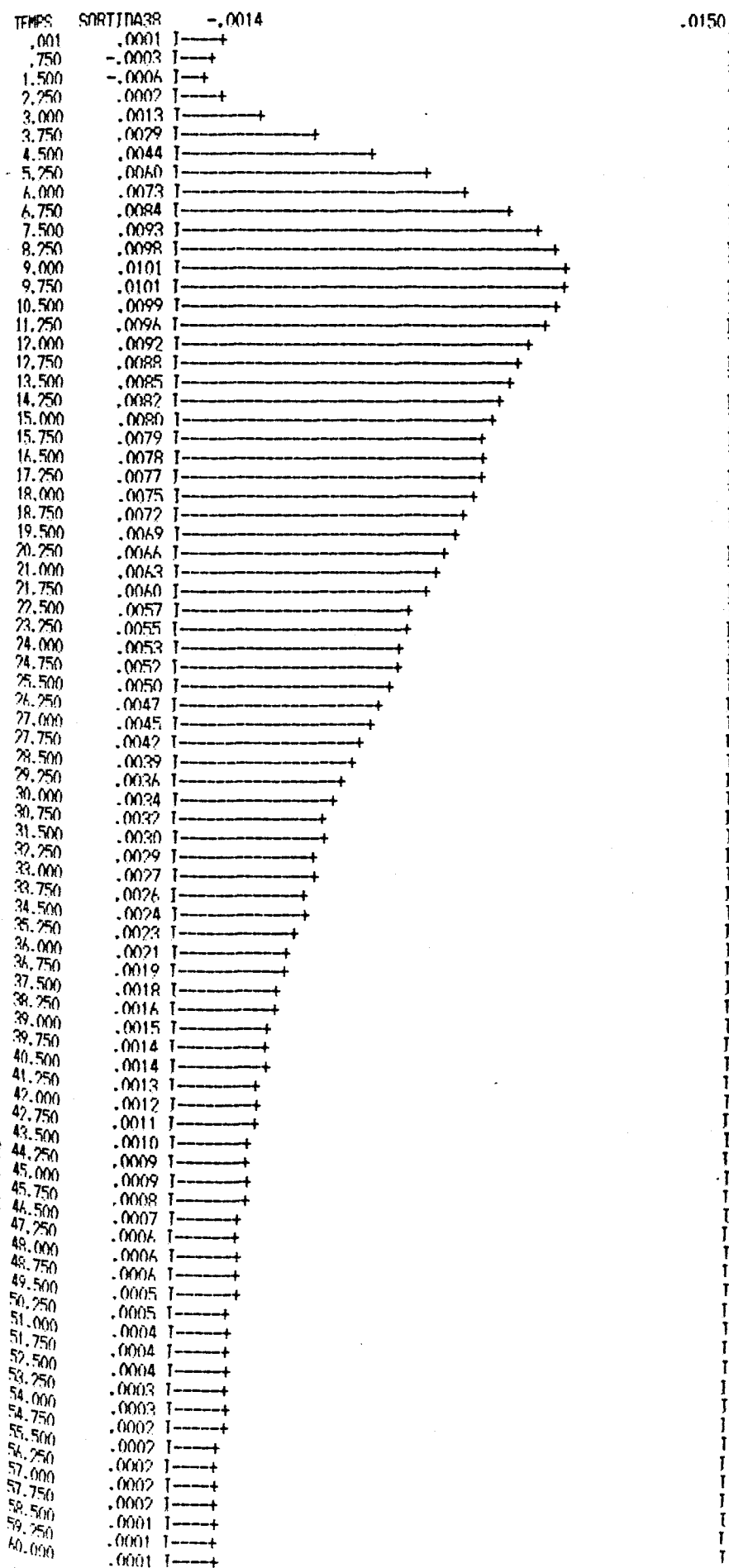
BLDC FIX Y (20) MINIM (-.0007) MAXIM (.0150)

SDD4.3



RUC FIX Y (38) MINIM (-.0014) MAXIM (.0150)

SDD4.4



SDD4.5

TEMPS	SORTINA44	SORTINA30	SORTINA55	SORTINA54
.00	.0001	.0001	.0001	.0001
2.00	-.0175	-.0334	.0014	.0002
4.00	-.0428	-.0369	.0043	.0003
6.00	-.0655	-.0168	.0057	.0005
8.00	-.0849	-.0001	.0059	.0006
10.00	-.1004	.0085	.0060	.0008
12.00	-.1147	.0080	.0061	.0009
14.00	-.1299	.0022	.0062	.0010
16.00	-.1444	.0029	.0062	.0012
18.00	-.1564	.0062	.0063	.0012
20.00	-.1670	.0059	.0063	.0013
22.00	-.1773	.0027	.0064	.0014
24.00	-.1867	.0031	.0064	.0014
26.00	-.1941	.0049	.0064	.0015
28.00	-.2003	.0042	.0065	.0015
30.00	-.2063	.0017	.0065	.0015
32.00	-.2118	.0012	.0065	.0015
34.00	-.2161	.0019	.0065	.0015
36.00	-.2197	.0015	.0065	.0015
38.00	-.2231	.0002	.0065	.0015
40.00	-.2262	-.0003	.0065	.0015
42.00	-.2287	.0002	.0065	.0015
44.00	-.2307	-.0001	.0065	.0016
46.00	-.2326	-.0007	.0065	.0016
48.00	-.2344	-.0009	.0065	.0016
50.00	-.2358	-.0007	.0065	.0016
52.00	-.2369	-.0007	.0065	.0016
54.00	-.2380	-.0010	.0065	.0016
56.00	-.2390	-.0011	.0065	.0016
58.00	-.2398	-.0010	.0065	.0016
60.00	-.2404	-.0008	.0065	.0016
62.00	-.2410	-.0010	.0065	.0016
64.00	-.2416	-.0011	.0065	.0016
66.00	-.2420	-.0010	.0065	.0016
68.00	-.2424	-.0008	.0065	.0016
70.00	-.2427	-.0008	.0065	.0016
72.00	-.2430	-.0009	.0065	.0016
74.00	-.2433	-.0008	.0065	.0016
76.00	-.2435	-.0007	.0065	.0016
78.00	-.2436	-.0007	.0065	.0016
80.00	-.2438	-.0008	.0065	.0016
82.00	-.2440	-.0007	.0065	.0016
84.00	-.2441	-.0005	.0065	.0016
86.00	-.2441	-.0005	.0065	.0016
88.00	-.2443	-.0006	.0065	.0016
90.00	-.2444	-.0006	.0065	.0016
92.00	-.2444	-.0004	.0065	.0016
94.00	-.2444	-.0004	.0065	.0016
96.00	-.2445	-.0005	.0065	.0016
98.00	-.2446	-.0005	.0065	.0016
100.00	-.2446	-.0003	.0065	.0016
102.00	-.2446	-.0003	.0065	.0016
104.00	-.2446	-.0004	.0065	.0016
106.00	-.2447	-.0004	.0065	.0016
108.00	-.2447	-.0002	.0065	.0016
110.00	-.2447	-.0002	.0065	.0016
112.00	-.2447	-.0003	.0065	.0016
114.00	-.2447	-.0003	.0065	.0016
116.00	-.2447	-.0001	.0065	.0016
118.00	-.2447	-.0001	.0065	.0016
120.00	-.2447	-.0003	.0065	.0016
122.00	-.2448	-.0003	.0065	.0016
124.00	-.2448	-.0001	.0065	.0016
126.00	-.2447	-.0001	.0065	.0016
128.00	-.2448	-.0002	.0065	.0016
130.00	-.2448	-.0002	.0065	.0016
132.00	-.2448	-.0001	.0065	.0016
134.00	-.2447	-.0001	.0065	.0016
136.00	-.2448	-.0002	.0065	.0016
138.00	-.2448	-.0002	.0065	.0016
140.00	-.2448	.0001	.0065	.0016
142.00	-.2447	.0001	.0065	.0016
144.00	-.2448	-.0002	.0065	.0016
146.00	-.2448	-.0002	.0065	.0016
148.00	-.2448	.0001	.0065	.0016
150.00	-.2447	.0001	.0065	.0016
152.00	-.2448	-.0002	.0065	.0016
154.00	-.2448	-.0002	.0065	.0016
156.00	-.2448	.0001	.0065	.0016
158.00	-.2447	.0001	.0065	.0016
160.00	-.2448	-.0002	.0065	.0016