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Transparent surfaces based on ultrathin materials with tailored optical and biological functionalities

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ABSTRACT

The properties of ultrathin materials present exciting opportunities to develop multifunctional surfaces. In addition, the use of plastic and thin glass as transparent substrates has the potential to extend the use of ultrathin materials beyond conventional substrates and provide vital advancements to existing and emerging technologies across a wide range of sectors. One of the main challenges facing next-generation transparent substrates is the substantially reduced temperature processing window which is not compatible with materials requiring high fabrication temperatures. This thesis describes the development of fabrication techniques to obtain ultrathin materials on low thermal budget transparent substrates to create surfaces with advanced optical and biological functionalities. More specifically, this thesis describes:

- A novel, low temperature transfer technique onto flexible substrates for ultrathin materials such as graphene, MoS₂ and nanostructured metals that were previously grown at a much higher temperature. The universality of the method extends the use of these ultrathin materials to a wide range of technologically relevant substrates such as cover glass for display modules and polymeric substrates for next generation foldable and bendable electronics.
- A novel approach to naturally increase electrical conductivity of transparent surfaces based on graphene, without the need of post-treatment, electrical gating or high temperatures. Notably, the method achieves a conductivity of comparable magnitude or greater than what is reported in previous studies. Furthermore, the increase in electrical conductivity is realised simply by utilizing an ion-exchanged substrate, a technologically relevant transparent glass substrate that is widely used in touch screen displays (e.g. smart phones).
- A low temperature metal dewetting technique to obtain transparent antimicrobial nanostructured coatings on a cover

glass substrate for display modules. The durability of the coatings was evaluated under conditions designed to simulate real-world use cases such as capacitive touch displays. The results show that the coatings were capable of substantially retaining optical properties of the underlying substrate, such as haze, neutral colour, and visible light transmission, as well as retaining antimicrobial properties after repeated contact with external objects such as, for example, when wiping with a towel or cloth, or touching with human fingers.

The results of this thesis demonstrate the implementation of ultrathin and nanostructured materials, such as graphene and nanostructured metals onto a wide range of technologically relevant transparent substrates, by methods that are industrially scalable and compatible with low temperature processing. At the same time, surfaces are engineered with advanced optical and biological functionalities that are relevant for applications such as transparent electrodes and antimicrobial coatings.

RESUMEN

Les propietats dels materials ultratins presenten oportunitats interessants per desenvolupar superfícies multifuncionals. A més, l'ús de plàstic i vidre fi com a substrats transparents té el potencial d'estendre l'ús de materials ultrafins més enllà dels substrats convencionals i proporcionar avenços vitals a les tecnologies existents i emergents en una àmplia gamma de sectors. Un dels principals reptes als quals s'enfronten els substrats transparents de nova generació és la finestra de processament de temperatura substancialment reduïda que no és compatible amb els materials que requereixen altes temperatures de fabricació. Aquesta tesi descriu el desenvolupament de tècniques de fabricació per obtenir materials ultrafins en substrats transparents de baix pressupost tèrmic per crear superfícies amb funcionalitats òptiques i biològiques avançades. Més concretament, aquesta tesi descriu:

- Una nova tècnica de transferència de baixa temperatura en substrats flexibles per a materials ultraprims com el grafè, MoS_2 i metalls nanoestructurats que anteriorment es conreaven a una temperatura molt més alta. La universalitat del mètode estén l'ús d'aquests materials ultratins a una àmplia gamma de substrats tecnològicament rellevants com el vidre de coberta per a mòduls de visualització i substrats polimèrics per a la propera generació electrònica plegable i doblegable.
- Un nou enfocament per augmentar de forma natural la conductivitat elèctrica de superfícies transparents basades en el grafè, sense necessitat de posttractament, portes elèctriques o altes temperatures. En particular, el mètode aconseguix una conductivitat de magnitud comparable o més gran que el que s'informa en estudis anteriors. A més, l'augment de la conductivitat elèctrica es realitza simplement mitjançant l'ús d'un substrat intercanviat d'ions, un substrat

de vidre transparent tecnològicament rellevant que s'utilitza àmpliament en pantalles tàctils (p. ex. telèfons intel·ligents).

- Una tècnica de dewetting de metall de baixa temperatura per obtenir recobriments nanoestructurats antimicrobians transparents en un substrat de vidre de coberta per mòduls de visualització. La durabilitat dels recobriments es va avaluar en condicions dissenyades per simular casos d'ús del món real com ara pantalles tàctils capacitives. Els resultats mostren que els recobriments eren capaços de retenir substancialment les propietats òptiques del substrat subjacent, com ara la boirina, el color neutre i la transmissió de llum visible, així com retenir les propietats antimicrobianes després de contacte repetit amb objectes externs com, per exemple, quan es cableja amb una tovallola o un drap, o tocar amb els dits humans.

Els resultats d'aquesta tesi demostren l'aplicació de materials ultraprims i nanoestructurats, com el grafè i els metalls nanoestructurats en una àmplia gamma de substrats transparents tecnològicament rellevants, per mètodes que són industrialment escalables i compatibles amb el processament de baixes temperatures. Al mateix temps, les superfícies estan dissenyades amb funcionalitats òptiques i biològiques avançades que són rellevants per a aplicacions com elèctrodes transparents i recobriments antimicrobians.

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C. Graham *et al.* (2023) "High and stable n-doping of graphene on ion-exchanged glass", *2D Materials*. 10 035037

Journal articles under review

C. Graham *et al.* (2023) "Durable, transparent and antimicrobial nanostructured surfaces on glass" (Under review)

Patent Applications

C. Graham, V. Pruneri, W. Senaratne, D. Thelen ID33460 "Antimicrobial surface with high transparency and durability using discontinuous metal islands"

CONTENTS

CHAPTER 1	26
1.1 Introduction	26
1.2 Thesis Outline	27
CHAPTER 2	30
ULTRATHIN MATERIALS OVERVIEW	30
2.1 Graphene and 2D materials.....	31
2.1.1 Transition metal dichalcogenides: MoS_2	35
2.1.2 hBN and layered 2D materials	37
2.2 Ultrathin metal films and nanostructures	37
2.2.1 Ultrathin Metal Film (UTMF) growth.....	38
2.2.2 Nanostructured UTMFS.....	40
2.3 Characterisation techniques.....	44
2.3.1 Optical.....	44
2.3.2 Electrical.....	48
2.3.3 Morphological.....	52
2.4 Transparent optoelectronic and biological applications.....	53
2.4.1 Transparent electrodes	54
2.4.2 Transparent antimicrobial (AM) surfaces	56
CHAPTER 3	57
LOW TEMPERATURE GROWTH AND PROCESSING TECHNIQUES FOR MoS_2 AND METAL NANOSTRUCTURES.....	57
3.1 Introduction.....	57
3.2 2D materials fabrication techniques	58
3.2.1 CVD growth	58
3.2.2 PVD techniques: Sputtering & Evaporation	60

Contents

3.3	A low temperature metal dewetting process to obtain highly transparent DNPs on low strain point glass	61
3.3.1	<i>Electromagnetic simulation of the individual DNPs</i>	62
3.3.2	<i>Discussion</i>	63
3.3.3	<i>Applications</i>	65
3.4	A transfer procedure for obtaining nanostructured and 2D materials on polymeric substrates	65
3.4.1	<i>Fabrication</i>	67
3.4.2	<i>Transfer of growth materials</i>	70
3.4.3	<i>Quality preservation of transferred nanostructured and 2D materials</i>	72
3.4.4	<i>Applications</i>	75
3.5	Conclusions and outlook	76

CHAPTER 4

TUNING ELECTRICAL FUNCTIONALITY OF A TRANSPARENT SURFACE MADE OF GRAPHENE 77

4.1	Introduction	77
4.2	Fabrication of devices.....	80
4.3	Characterisation of devices	83
4.3.1	<i>Electrical characterisation</i>	83
4.4	Applications and future work	89
4.5	Conclusions and outlook	89

CHAPTER 5

HIGHLY TRANSPARENT, ANTIMICROBIAL AND DURABLE COPPER NANO-STRUCTURED SURFACES ON GLASS

5.1	Introduction	91
5.2	State of the art AM Solutions for display and touchscreen applications.....	92
5.3	Fabrication of TANCs	100
5.3.1	<i>Antimicrobial (AM) efficacy testing</i>	102
5.3.2	<i>Calculations of log and percentage of reductions</i>	103

Contents

5.3.3	<i>Stipulated wear testing</i>	104
5.3.4	<i>ICP-MS mock testing to determine % of leached copper from TANCS</i>	106
5.3.5	<i>Morphological, Optical, Mechanical and Antimicrobial Characterizations of the coatings</i>	107
5.4	Results and discussion.....	107
5.4.1	<i>Morphological, optical and electrical properties</i> ..	107
5.4.2	<i>AM activity of TANCS</i>	109
5.5	AM durability.....	116
5.6	Conclusion	117
CHAPTER 6		118
CONCLUSIONS & OUTLOOK		118
6.1	Conclusions.....	118
6.2	Outlook.....	120

LIST OF FIGURES

- Figure 1 (a) Graphene structure showing planar hexagonal arrangement of carbon atoms. (b) Bonding scheme of graphene in which two carbon atoms contribute one electron each from each sp_2 orbital to form a σ bond. The remaining single electrons in the p_z orbitals of the two carbon atoms combine to form a π -bond. (c) 3D-graphic of graphene band structure with K and K' Dirac points. Zoom area shows the zero-bandgap of graphene where valence band (bottom) and conduction band (top) meet. The graphic has been adapted from reference [6]..... 32
- Figure 2 A typical two-probe graphene device (Graphene FET) that can be electrostatically tuned. b) Ambipolar field effect in graphene, taken from Ref[6]. The plot is resistivity as a function of gate voltage (V_G). The insets show its conical low-energy spectrum $E(k)$, indicating changes in the position of the Fermi energy E_F with changing gate voltage V_G . Positive (negative) V_G induces electrons (holes), respectively..... 34
- Figure 3 (a) Chemical structure of two layers of MoS_2 (b) Energy dispersion (energy versus wavevector k) in bulk, quadrilayer (4L), bilayer (2L) and monolayer (1L) MoS_2 from left to right, where N indicates the number of layers. The horizontal dashed line represents the energy of a band maximum at the K point. The red and blue lines represent the conduction and valence band edges, respectively. The solid arrows indicate the smallest energy transitions. There is an indirect transition for bulk and few-layer crystals that becomes a direct transition for a monolayer MoS_2 . Adapted from Reference [34] 36
- Figure 4 Schematics of three kinds of thin-film growth modes. a) Volmer-Weber mode (3D island growth). b) Stranski-Krastanov mode (layer plus island growth). c) Frank-van der Merve mode (layer-by-layer growth). 39

List of Figures

- Figure 5 Representation of the solid-state dewetting process. A uniform thin film self-assembles into isolated islands when rapidly heated. The initial UTMF thickness, annealing temperature and the duration of thermal treatment, together with the material composition of the film, will affect the distribution and size of the nanoparticles. 41
- Figure 6 (a) Illustration of electric fields of incident light and those generated by the electron oscillations near the NP. Yellow shaded region indicated M^+ ionic background. (b) Schematic drawing of the interaction of an electromagnetic radiation with a nanoparticle. It generates a dipole that oscillates in resonance with the electric field of the incident light as well as a strong confined electric field at the nanoparticle surface. 42
- Figure 7 Optical processes occurring when light interacts with a semi-transparent surface..... 44
- Figure 8 Raman vibrational modes E_{2g}^1 and A_{1g} and representative Raman spectra of bulk MoS_2 with E_{2g}^1 and A_{1g} peaks at 383 and 408 cm^{-1} . Spectra compares bulk and MoS_2 , *(experimentally obtained). 47
- Figure 9 PL spectra of ultrathin MoS_2 (experimental data). The observed absorption peaks at 1.85 eV (670 nm) and 1.98 eV (627 nm) correspond to the A1 and B1 direct excitonic transitions. Inset adapted from reference [34] 48
- Figure 10 Schematic of the Four Point probe set-up used for the R_s measurement in (a) colinear configuration and (b) Van-der-Pauw configuration with cloverleaf shaped graphene. 49
- Figure 11 Device designs fabricated in this work. In design A the graphene cloverleaf has a diameter of 300 μm . In design B, the Hall bar has dimensions 140 x 300 μm 52
- Figure 12 The schematic of a tube CVD system. (b) 2D film growth process: first, the nucleation is formed as the growth centre of grain domains; second, the growth of the 2D grain domains; third, the 2D domains coalesce to form a continuous film 59

List of Figures

- Figure 13 PVD techniques (a) sputtering; (b) thermal evaporation; (c) E-beam evaporation..... 61
- Figure 14 SEM images clearly illustrate the influence of the annealing temperature on the particle shape and size. High temperature produces separate, rounded particles with a contact angle $\approx 90^\circ$ whilst low temperature produces, flatter particles, with a contact angle $< 90^\circ$ and that are sometimes in contact. Scale bar = 100 nm. Optical spectra obtained from experiment (b) and modelling (c). Modelling reproduce qualitatively the experiments, in particular the red shift and broadening of the plasmonic resonance due to a reduction of particle's contact angle. Inset of b) shows the colour of the coatings against white background and also against a coloured text background to show transparency and colour neutrality of the dewetted CU UTMFs. The inset of c) shows the particle shape used for the modelling as determined from the SEM images in a..... 64
- Figure 15 AFM of NaCl substrate after cleaning with organic solvents (acetone and isopropanol)..... 68
- Figure 16 Fabrication of Au dewetted nano-particles (nano-caps) on NaCl by heating a sputtered Au layer of 7 nm thickness at 750°C for 90 seconds. (b) CVD growth of MoS₂ on NaCl substrates due to the reaction of MoO₃ with S powder, with the latter being introduced at 650°C using two magnets. Heating profile and N₂ flow rate for (c) Au DNPs and (d) MoS₂..... 70
- Figure 17 Transfer of Au DNPs and MoS₂ to PET using PMMA as an intermediate layer: (a) Spin-coating of PMMA at 4000 rpm for 1 minute; (b) Partial dissolution of NaCl substrate in water to afford the separation of the growth material covered with PMMA; (c) PMMA with Au DNPs and MoS₂ is located on top of the PET after which the PMMA is removed by immersion in acetone and isopropyl alcohol for 10 minutes each..... 71
- Figure 18 NaCl post-transfer conditioning Photographs (top) and AFM pictures (bottom) of (a) NaCl substrate sonicated in conventional organic solvents for 10 minutes and dried with a N₂ stream, (b) after MoS₂ removal and (c) after post-transfer

List of Figures

- rapid thermal annealing at 750°C for 135s. Scale bar: 5 μm .
..... 72
- Figure 19 SEM images of (a,d) as-grown and (b,e) transferred Au DNPs and MoS₂ respectively. Scale bar: 2 μm . Note that the different contrast in the top images (a,b) is due to different substrate charging. Figure c provides a comparison to as grown Au-DNPs on a fused silica (fs) substrate. 73
- Figure 20 Single point (a) Raman and (b) photoluminescence spectra in the range 1.6 to 2.1 eV before and after transfer. Raman maps for MoS₂ on (c) NaCl and (d) PET. Scale bar: 100 μm . 74
- Figure 21 Transmission as a function of wavelength for (a) Au DNPs and (b) MoS₂ on NaCl and PET. Inset shows photographs of Au DNPs and MoS₂ on NaCl and PET substrate..... 75
- Figure 22 Device designs fabricated in this work. In design A the graphene cloverleaf has a diameter of 300 μm . In design B, the Hall bar has dimensions 140 x 300 μm 81
- Figure 23 Procedure for the graphene device fabrication: (a) Wet graphene transfer (1) Cut PMMA/Gr/Cu foil to approx. 0.5cm² in size. (2) The foil is floated on top of ammonium persulphate for approximately 4 hours to etch the Cu from underneath the graphene. (3) The resulting PMMA/Gr stack is wet transferred onto a metalized substrate; (b) (1) Initial cleaning of substrates is by organic solvents acetone and isopropanol. (2) UV lithography and evaporation of the metal contacts (Ti 3 nm / Au 50 nm) (3) Graphene transfer onto metalized substrates by wet etching process. (4) Samples are left overnight to dry after which PMMA is removed by immersion in acetone for 15 minutes. (5) A second lithography is performed to reduce the graphene contacts area, removing the excess by reactive ion etching (RIE). (6) Hall bar devices were encapsulated with 40 nm Al₂O₃ by ALD deposition. A final lithography is performed to remove the Al₂O₃ from the top of the Au contacts by dipping the samples into a BOE solution..... 82
- Figure 24 Sketch of graphene transferred onto IOX Corning® Gorilla® glass (a) and fused silica (FS) glass (b) where blue shaded area

List of Figures

comprises the silica matrix. The top surface of the IOX Corning® Gorilla® glass contains potassium (K+) from an ion-exchange procedure, where the depth of layer can be modified from 1 to 50 μm ; (c) I-V characteristics measured for graphene on IOX20 μm Corning® Gorilla® glass (green circles) and FS (black circles) substrates. For each device, the I-V curve was measured several times to ensure repeatability, sampling at 1 mV steps, which are subsequently averaged. A linear fit was applied to the I-V curves collected for all devices on each substrate (totalling 16 IOX and 16 FS devices), with error bars representing the spread in the data. Note that the error bar for graphene/FS is not visible because of the low standard deviation. The average R_s was obtained from the slope. The inset of the graph shows an optical microscope image of a real sample. Scale bar 100 μm 84

Figure 25 Simplified three-dimensional views of the Hall bar structures, along with circuits for the Hall effect measurement. The heavy purple arrow indicates the direction of the magnetic field corresponding to the circuit diagrams shown. A constant DC current of $1\mu\text{A}$ was injected through the sample via probes “1-2” whilst and probes “3-4” or “3-5” to measure the R_s or V_{Hall} , respectively during a perpendicular magnetic field sweep (-5 T to 5 T) at 300 K . (b) V_{Hall} vs. magnetic field (B) data obtained from 16 graphene/IOX $_{1-43\mu\text{m}}$ devices (green circles) and 2 graphene/Si/SiO $_2$ devices (black circles) where the dotted line represents a linear fitting of all devices. *Note that the IOX data does not distinguish IOX layer thickness because the n_s was not influenced by the depth of exchange and, by deduction, the V_{Hall} was found to be independent of the IOX thickness. The inset of the graph shows an optical microscope image of a real sample. Scale bar 100 μm 85

Figure 26 The evolution of (a) R_s (b) μ_H and (c) n_s with IOX layer thickness. Each marker and error bars represent the average and standard deviation of D1 and D2. Samples included in the statistics are $1\times 1\ \mu\text{m}$, $1\times 5\ \mu\text{m}$, $2\times 10\ \mu\text{m}$, $2\times 20\ \mu\text{m}$ and $2\times 43\ \mu\text{m}$. In graph (a) purple markers represent the R_s for the IOX

List of Figures

devices remeasured after 5 months. The corresponding values for the Si/SiO₂ reference sample is provided in the inset of graph a. The values of μ_H and n_s for the Si/SiO₂ reference samples are indicated with blue markers in graphs b and c. In some cases, the error bars were smaller than the markers and are not visible..... 88

Figure 27 Strategies to impart AM function into transparent surfaces. Green text indicated commercial products referenced in Table 3..... 92

Figure 28 (a) Schematic illustration of the cross section of the TANC comprising 1 the glass substrate with optional adhesion layer, 2 copper or Cu₂O dewetted nanoparticles, 3 inorganic oxide embedding layer and 4 an easy to clean fluorosilane. The variation in contact angle the particle makes with the substrate is shown in the figure together with the related effects on thickness of covering layer. Dimensions are representatives but not in scale. Zoomed area shows the cross section of the coating with representative dimensions. (b) General chemical formula of ETC Optool UD509, PFPE–silane monomer, which can have variable number of silane groups, m, and variable length of PFPE chain, n. 99

Figure 29) Fabrication of transparent and AM nanostructured Cu surface (TANCS) by (1) DC sputtering of 3.5 nm Cu onto a glass substrate, (2) Low temperature annealing of Cu to form dewetted nanoparticles, (3) Evaporation of an inorganic oxide, e.g. SiO₂, embedding layer and (4) spray coating of a polymer coating, e.g. fluorosilane based easy to clean (ETC). Note that the contact angle the particle makes with the substrate is not representative and varies between 60 -100° typically for low temperature processes. 101

Figure 30 Initial and residual self-sanitising test protocols defined by the EPA for the quantification of the AM efficacy of Cu-containing surfaces. (b) Process for abrasion for residual self-sanitising test 106

Figure 31 Top down (a) and side on (b) SEM micrographs of TANCS coatings. The parameters of the SEM scan are as follows. HV

List of Figures

15.00 kV; det ETD; magnification 160,000x; WD 9.9 mm; spot 3.0; tilt 0° (a). tilt -15°(b). The scale bar is 500 nm; (c) Particle size distribution analysis using ImageJ); (d) Transmission spectra of representative TANC (blue line) as compared to the uncoated bare glass substrate (black line). Inset shows photographs of bare glass (left) and TANCs (right); (e) Finite Element Model Prediction for TANCs obtained from 3.5 nm Cu UTMF. The graph shows the alternating-current impedance ratio of an TANC in accordance with one aspect relative to an otherwise identical bare glass substrate. The lateral-surface impedance predictions demonstrate that capacitive touch performance can coexist with this dewetting antimicrobial process..... 108

Figure 32 (a) LR vs [Cu] leached. The EPA-prescribed 3-LR, corresponding to >99.99% reduction in bacterial colony counts, is marked with a black line. The blue and pink shaded regions correspond to the [Cu] concentration range above and below which a 3-LR was observed, respectively. *The comparison between LR and [Cu] leached assumes that the majority of the ions are held in the liquid phase and not consumed by the microorganisms i.e. rate of Cu dissolution due to the PBS >>> rate of consumption of Cu due to the presence of microorganisms. (b) Transmission spectra of representative TANCs. For both graphs, the circle and square markers represent TANCs from sets A and B, respectively. Inset of (b) shows photographs of Set A and Set B after mock testing where the marked central region marked shows the testing area. 112

Figure 33 Plots of LR and [Cu] leached as a function of SiO₂ thickness and fluorosilane concentration for (a) 50 W and (b) 300 W oxygen plasma treated TANCs. Error bars represent the standard deviation of two samples. Note that in some cases, the error bar is smaller than the marker and not visible... 114

Figure 34 (a) Transmission, (b) LR, (c) Haze and (d) WCA of TANCs before and after wet abrasion testing with IPA (1200 wipes) and Lysol® (730 wipes). The inset of (a) shows the TANCs after wet abrasion testing on the central region. The visual

List of Figures

appearance of the central wiping region remains close in color to the outer region, indicting a good durability of the coating to repeated wipes with cleaning sanitizers. 117

LIST OF TABLES

Table 1 Statistical Parameters for two fabricated Samples with UTMF of 3.5 nm Cu annealed at 390 and 750 °C, respectively, as extracted by SEM Image Analysis in ImageJ. Standard deviation follows the '±' symbol.	63
Table 2 Rs of graphene measured by in using the 4-point probe method in co-linear orientation.....	85
Table 3 Commercially available transparent AM coatings indicating fabrication method, coating properties.....	94
Table 4 A comparison of the present study with previous works directed towards creating transparent Antimicrobial (AM) or antiviral (AV) coatings	95
Table 5 TANCS coatings (A and B type) together with control (ctrl) samples.	102
Table 6 Water contact angle (WCA) of Set A TANCS before and after AM testing.....	115
Table 7 Staphylococcus aureus CFU results for Set A and B Figure 32 and Figure 33.....	149

NOMENCLATURE

μ H: Charge carrier mobility

2D: two dimensions

3D: three dimensions

AC: Alternating current

AFM: Atomic Force
Microscope

Ag: silver

AgNW: silver nanowire

AR: anti-reflection

Au: gold

B: Magnetic field

C1, C2: Geometrical factor for
Rs calculation

CBM: Conduction band
maximum

Cu DNPs: Copper dewetted
nanoparticles

CNP: Charge neutrality point

CNT: carbon nanotubes

CVD: Chemical Vapor
Deposition

DC: Direct Current

DI: deionized

E: Electric field

EPA: Environmental
Protection Agency

FET: Field effect transistor

F_L : Lorentz force

FWHM: Full Width at Half
Maximum

HOMO: highest occupied
molecular orbital

HTA: high temperature
annealing

I: Current

I_{12} : Current injected from
contact 1 to 2

I_{14} : Current injected from
contact 1 to 4

I_{23} : Current injected from
contact 2 to 3

I_{2D} : Intensity of the 2D Raman
peak

I_{34} : Current injected from
contact 3 to 4

I_D : Intensity of the D Raman

I_G : Intensity of the G Raman

IR: infrared

ITO: indium doped tin oxide

LED: Light emitting diodes

LUMO: Lowest unoccupied
molecular orbital

NaCl: Sodium Chloride

NA: numerical aperture

NIR: near infrared

NWs: Nanowires

n_s : Charge carrier density

PEDOT: Poly (3, 4-ethylenedioxythiophene)
PAA: Polyamic acid
PDMS: Polydimethylsiloxane
PET: polyethylene terephthalate
PI: Polyimide
PMMA: Poly(methyl methacrylate)
PS: Polystyrene
PSS: poly (styrene sulfonate)
PVD: Physical Vapor Deposition
PVP: poly(vinylpyrrolidone)
 q_e : Electron charge ($1.602 \cdot 10^{-19}$ C) xiv
R: reflection
RMS: Root Mean Square
 $R_{12,34}$: Resistance. Voltage measured in contacts 3-4. Current injected from contact 1-2
 $R_{14,23}$: Resistance. Voltage measured in contact 2-3. Current injected from contact 1-4
 $R_{23,14}$: Resistance. Voltage measured in contact 1-4. Current injected from contact 2-3
 $R_{34,12}$: Resistance. Voltage measured in contact 1-2. Current injected from contact 3-4
RS: Sheet resistance

RT: Room temperature
RTA: rapid thermal annealing
SDG: Soda lime glass
SEM: Scanning Electron Microscopy
t: Thickness
T: Transmission
 T_F : Film transmittance without substrate contribution
 T_g : Glass transition temperature
TC: Transparent conductor
TE: Transparent electrode
TCO: Transparent Conducting Oxide
 TiO_2 : titanium oxide
TS : Substrate transmission
TTC : TC transmission
TTOT : Total transmission
UTMF: ultrathin metal films
UV: Ultraviolet
V: Voltage
 V_{12} : Voltage, measured in contact 1-2
 V_{14} : Voltage, measured in contact 1-4
 V_{23} : Voltage, measured in contact 2-3
 V_{34} : Voltage measured in contact 3-4
VBM: Valence band minimum
 V_G : Charge neutrality point
 V_H : Hall voltage
WCA: Water contact angle

XPS: X-ray photoelectron
spectroscopy
ZnO: Zinc Oxide

λ : Wavelength
 ρ : Resistivity

CHAPTER 1

1.1 Introduction

The field of ultrathin materials has come a long way since the first exfoliation of graphene, oxides and metals. Thanks to improved growth and processing techniques it is now possible to obtain high quality ultrathin materials, including graphene and nanometer thick metals on a large scale, offering the possibility to create multifunctional transparent surfaces with anti-reflective, electrically conductive, self-cleaning and antimicrobial properties, to name a few. Furthermore, doping and nanostructuring techniques, provide the means to create transparent ultrathin surfaces with advanced functionalities including electrical and electro-optical tunability and tailored light-matter interactions. To this end, ultrathin materials have been used to add functionality to transparent surfaces applied towards products in the display, photovoltaic and coating industries. However, despite their impressive success, the huge potential of ultrathin materials remains to be fully realised.

One of the fundamental challenges is that existing growth and processing techniques often do not facilitate scalability at an industrial level. There is a need to develop mass-scalable methods of surface modification at the nanoscale. A second challenge concerns engineering specific material properties by methods that are reliable, repeatable, economic, stable and outperform existing solutions. For example, high electrical conductivity and optical transparency, are properties required by transparent conductors (TCs). Ultrathin materials such as graphene have been recognized as potential candidates in next generation TCs, though challenges remain in improving conductivity to levels that can compete with the existing state-of-the-art. Finally, the advent of flexible electronics has driven the need to innovate the growth, processing and transfer of ultrathin materials that traditionally require high temperatures or whose properties are not fully compatible with respect to the

substrate. This would enable a host of functional surfaces on a wide class of substrates.

In this regard, the main objective of this thesis is to design and develop transparent surfaces with advanced functionalities for optical and biological applications based on ultrathin materials. The functionalities include transparent electrodes and antimicrobial properties. The ultrathin materials include graphene, MoS₂, and nanometer thick metals which can also be nanostructured.

The specific objectives of this thesis are:

- (i) Develop scalable techniques to transfer 2D materials, such as graphene and MoS₂ and nanostructured metals onto transparent flexible substrates at low temperatures
- (ii) Find the optimum substrate-graphene combination for increasing doping and the electrical conductivity of transparent surfaces.
- (iii) Use ultrathin metals and subsequent nanostructuring for increasing the antimicrobial activity of transparent surfaces

1.2 Thesis Outline

The thesis is organised into six chapters:

Chapter 2 provides a brief review of ultrathin materials properties, including graphene, 2D transition-metal dichalcogenides, and nm scale metallic nanostructures, together with some theoretical background on the growth mechanism of 2D materials, and their electrical and optical properties. The characterization methods used to analyse and optimize the modified transparent surfaces are also included. Finally, the electrical and biological applications of 2D materials are summarised with a focus on transparent electrodes and transparent antimicrobial surfaces.

Chapter 1: Introduction

Chapter 3 is dedicated to the optimisation of low temperature fabrication and processing techniques for 2D materials and nanostructured metals. The first section describes the deposition, growth and nanostructuring techniques utilised in this work. The second section includes a study of a system of Copper dewetted nanoparticles (Cu DNPs) fabricated on low strain point transparent glass substrates. The dewetting conditions and UTMF precursor thickness were optimised for obtaining maximum transparency in the visible region. A complete theoretical and experimental analysis of the morphological and optical properties of the samples as a function of dewetting temperature is also presented. The third section describes a novel growth and processing technique which enables high thermal processing materials e.g. MoS₂ and metallic nanostructures to be obtained on low strain point substrates such as polyethylene terephthalate (PET). A full optical and morphological characterisation of the as grown and transferred materials is provided. The techniques presented in this chapter represent important innovations as they are universal and not limited by the underlying substrate. In such a way this work opens up the possibility to obtain a host of functional electrooptical and biological surfaces on flexible substrates.

Chapter 4 focuses on tuning the electrical functionality of a transparent surface made of graphene. The first section includes a review of the state-of-the-art doping techniques and the challenges regarding the implementation of doped graphene into real-world devices. The second section investigates a novel and scalable method of inducing ultrahigh n-doping of graphene by utilising a transparent ion-exchanged glass substrate. The fabrication and electrical characterisation of graphene devices is described and a doping mechanism is proposed. The innovations described in Chapter 4 and, specifically the ability to achieve high, relatively stable, and tunable graphene doping on low-cost, industry-standard materials, pave the way for the practical realization of many envisioned applications of graphene such as transparent electrodes for touch screens and organic light-emitting diodes, where the reduction of sheet resistance is crucial. The results of this work are also important for applications requiring strong and tunable n-doping, such as

Chapter 1: Introduction

microelectronics, photodetectors, photovoltaics, low work function tunable electrodes and sensors.

Chapter 5 is dedicated to the development of transparent antimicrobial (AM) surfaces on cover glass substrates for display and touchscreen applications. The first section reviews the state-of-the-art techniques to impart AM functionality into transparent substrates. This also includes an overview of the existing commercially available solutions. The second section describes the optimisation of the metallic nanostructures developed in Chapter 3 to realise transparent coatings with AM functionality that are also durable and long lasting. The coatings are easy to clean, maintain their AM functionality, optical and wetting properties over a long period of time, whilst also being fabricated in a way that is industrially scalable. A full characterisation of the samples is provided. It is anticipated that the results of this work will be useful in many applications of technological interest such as touch-enabled public displays.

Chapter 6 summarizes the main results of this thesis, and gives a brief outlook on potential future developments.

CHAPTER 2

Ultrathin materials overview

Ultrathin materials are defined as materials which have a large lateral size (up to a few micrometres and larger), but whose thickness is only single- or a few-atoms thick (typically less than 10 nm). This dimensionality confers a range of intrinsic extraordinary physical, electronic and optical properties as electrons are confined to two dimensions. Furthermore, being atomically thick, these materials have unmatched mechanical flexibility and optical transparency and large specific surface areas making them compelling for the fabrication of highly flexible and transparent electronic/optoelectronic devices. In addition to their remarkable intrinsic properties, 2D materials are also highly tunable by the application of a gate voltage, strain and external electric field. This enables material properties to be dynamically tuned to suit the application or environment. The following sections provide an overview of the fundamental properties, characterisation techniques and applications of ultrathin materials, focussing mainly on graphene, MoS₂ and nanostructured metals, their characterisation and implementation and transparent optical and biological applications.

2.1 Graphene and 2D materials

Arguably the most famous of the 2D materials is graphene, a single layer of carbon atoms arranged in a honeycomb lattice structure, as shown in [Figure 1a](#). From an optoelectronics standpoint, it is both electrically conductive and optically transparent, two properties rarely found together, making it a natural candidate for next-generation transparent conductors (TCs). Graphene first attracted significant attention after 2004, when Novoselov and Geim isolated it in monolayer form, using a scotch tape exfoliation method. They also demonstrated its electrical field effect transistor behaviour [1]. Graphene's outstanding properties were further outlined in later studies [2–4], including the demonstration of the room temperature quantum Hall effect [5] and high room temperature carrier mobility [6] which eventually led to Novoselov and Geim being awarded the Nobel Prize in Physics in 2010 [7,8].

These remarkable phenomena arise due to the unique bonding structure of graphene. The sp^2 hybridised orbitals of the carbon atoms support sigma (σ) and pi (π) bonding components as shown in [Figure 1b](#). The σ bond is formed in the x-y plane when two sp^2 hybridised orbitals of adjacent carbon atoms overlap. The π bond is formed in the z plane where two p_z orbitals of two adjacent carbon atoms overlap. The electrons in the σ bonds are held strongly and give graphene its mechanical strength, whilst electrons in π bonds are held weakly, and delocalise above and below the plane of bonded carbon atoms and are responsible for its excellent thermal and electrical conductivities.

The hexagonal arrangement of carbon atoms gives rise to a unique band structure where the valence and conduction bands touch each other at the so-called Dirac point or charge neutrality point (CNP) [9], [Figure 1c](#). At the Dirac point the density of states (DOS) is zero and by this definition, graphene is referred to as a zero-band gap semiconductor or a zero-overlap semimetal. Under neutral conditions, when graphene is undoped the Fermi level (E_F) lies at the meeting point of the bands and the intrinsic charge carrier concentration (n_S) is, in principle, zero. Close to the Dirac point, the charge carriers have a linear relationship between energy and

momentum. This linearity considers the charge carriers as massless Dirac fermions [2,10], which are described by the relativistic Dirac equation rather than the non-relativistic Schrodinger equation. The carriers travel at a relativistic Fermi velocity, $v_F = c/300$, where c is the speed of light in vacuum. The injection of charge carriers, denoted n_s (electrons or holes), through, for example electrical gating or chemical doping, results in a square-root shift in the Fermi energy with respect to the value at the Dirac point according to Eq. 2.1

$$E_F = \hbar v_F k_F = \hbar v_F \sqrt{\pi n_s} \quad (2.1)$$

where \hbar is the reduced Planck constant and $k_F = \sqrt{\pi n_s}$ is the Fermi wave vector. Moreover, given the linear dispersion and vanishing density of states at the Dirac point, only a moderate increase in n_s is required to induce substantial changes in E_F . This is in contrast to other semiconductor materials whose band structure can be considered parabolic for very low energies and $E_F \propto n_s$.

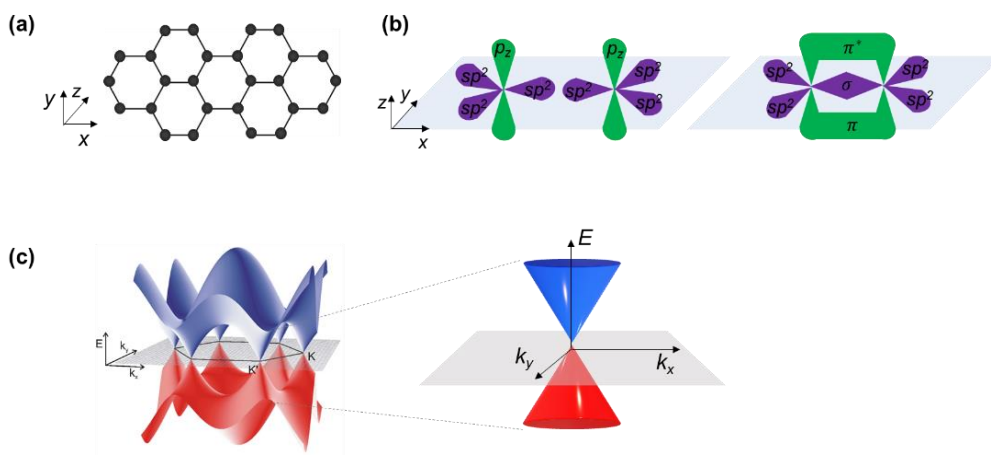


Figure 1 (a) Graphene structure showing planar hexagonal arrangement of carbon atoms. (b) Bonding scheme of graphene in which two carbon atoms contribute one electron each from each sp_2 orbital to form a σ bond. The remaining single electrons in the p_z orbitals of the two carbon atoms combine to form a π -bond. (c) 3D-graphic of graphene band structure with K and K' Dirac points. Zoom area shows the zero-bandgap of graphene where valence band (bottom) and conduction band (top) meet. The graphic has been adapted from reference [6].

Tunable electronic properties of graphene

Charge carriers can be induced into graphene by the electrostatic field effect or by chemical means. For electrostatic doping, an electrical bias is applied to the graphene. The typical device structure for achieving the field effect is the field effect transistor (FET). Recently, transparent Graphene FET devices have been demonstrated in which the graphene channel is patterned on a transparent substrate, such as quartz or borosilicate, and is surrounded by the source and drain electrodes, made of another transparent conducting material or graphene [11]. The gate electrode is separated from the graphene channel by a thin insulating layer, typically made of silicon dioxide (SiO_2), aluminium oxide (Al_2O_3), hafnium dioxide (HfO_2), silicon nitride (Si_3N_4) or hexagonal boron nitride (hBN). This configuration resembles a capacitor with the gate electrode and the graphene acting as the two plates of the capacitor. The application of voltage to the gate electrode induces an electric field in the insulating layer that causes charges to accumulate on the graphene as a function of the applied gate voltage (V_G). The carrier density, n_s , is tuned electrostatically with the application of a gate voltage. The change in n_s as a function of V_G translates to a change in the resistance of the graphene device (as shown in [Figure 2](#)) and can be measured across the source and drain contacts. With the applied gate voltage (V_G), the resistance of the graphene changes as the number and type of charge carriers change from p-type at negative voltages to n-type at positive voltages. When n_s approaches zero, graphene shows a finite maximum resistance at the charge neutrality point (CNP), due to the absence of a band gap. At the Dirac Point, graphene exhibits a minimum conductivity, which is approximately on the order of magnitude $4e^2/\hbar$. The charge carrier density is related to the electrical conductivity (σ) by the [Eq. 2.2](#):

$$\sigma \approx \mu e n_s \tag{2.2}$$

where μ is the carrier mobility and e is the elementary charge. n_s is determined by the doping level. The carrier mobility is affected by the electron scattering by lattice vibrations, lattice defects for example holes, impurities, wrinkles and grain boundaries. Whilst suspended graphene

has a mobility in the order of $\sim 10^6$ cm²/V·s [4,12], the mobility of supported graphene is limited by several factors including its interaction with substrate phonons, charged impurities and lattice defects. Nonetheless, graphene still exhibits a room temperature mobility that far surpasses most conventional semiconductors, recently reaching values up to 350,000 cm²/V·s [13] for a hexagonal boron nitride (hBN) encapsulated device.

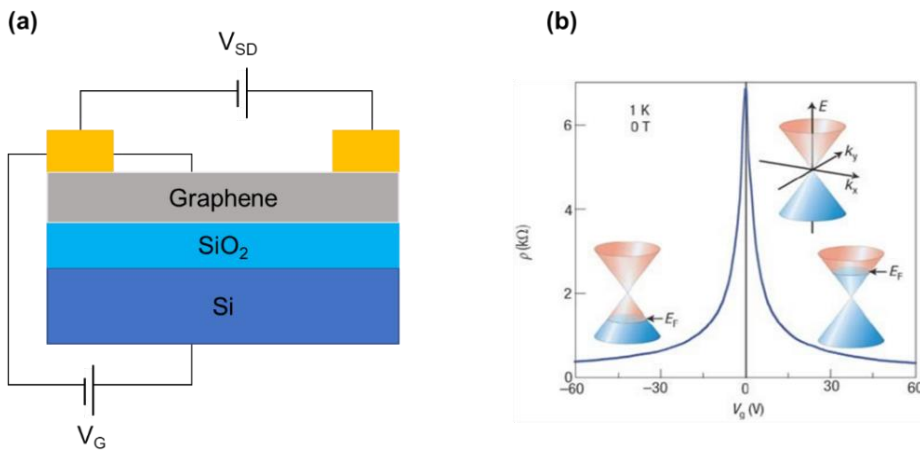


Figure 2 A typical two-probe graphene device (Graphene FET) that can be electrostatically tuned. b) Ambipolar field effect in graphene, taken from Ref[6]. The plot is resistivity as a function of gate voltage (V_G). The insets show its conical low-energy spectrum $E(k)$, indicating changes in the position of the Fermi energy E_F with changing gate voltage V_G . Positive (negative) V_G induces electrons (holes), respectively.

Optical properties of graphene

The zero-band gap nature of graphene gives it exceptional optical properties [14–16]. In the undoped state, graphene is characterized by its universal optical conductivity, $\sigma_{uni} = \pi e^2/2h$, where e is the electronic charge and h is Planck's constant. This gives rise to the well-known universal absorption of 2.3 % in the region from visible to near-IR frequencies. When electrically doped, an optical gap opens up which is proportional to the applied bias voltage [17–19].

2.1.1 Transition metal dichalcogenides: MoS₂

Beyond graphene, one group of 2D materials that has amassed great attention is transition metal dichalcogenides (TMDs). These materials combine the ultrathin nature of graphene with exceptional semiconductor properties. In Chapter 3 of this thesis, MoS₂ was chosen as a prototypical 2D material for the development of a novel transfer process that enables high thermal processing materials to be obtained on low strain point flexible substrates. The following section describes the structural, electrical and optical properties of MoS₂ and its applications.

Structure

Bulk TMDs, with the general formula MX₂, consist of vertically stacked sheets where each 3-atom thick sheet consists of a layer of transition metal atoms, M, such as molybdenum (Mo) or tungsten (W), between two planes of chalcogen atoms, X, such as sulphur (S) or selenium (Se), as shown in [Figure 3a](#). The atoms within each layer of TMDs are held together by covalent bonds, while vertical layers are held together by weaker van der Waals interactions. The layers can be arranged in a variety of polytypes, which vary in stacking orders and metal atom coordination, the most energetically favourable being the 2H phase.

Optical and vibrational properties

In the 2H-polytype, both bulk and few layer MoS₂ exhibit semiconducting behaviour, with an indirect band gap transition in which the valence band maximum (VBM) and conduction band minimum (CBM) are located at the Γ point and Λ points of the Brillouin zone, respectively. With decreasing layer number, both the CBM and VBM shift toward the K point, resulting in a direct band gap of 1.9 eV for monolayer MoS₂ [20] as shown in [Figure 3b](#). The change in the band structure with layer number is due to quantum confinement and the resulting change in hybridization between p_z orbitals on S atoms and d orbitals on Mo atoms [21].

This transition to a direct band gap is significant as photons with an energy higher than the bandgap can be efficiently absorbed and emitted, and is therefore able to reach significantly higher quantum yields than bilayer and bulk devices [20]. TMD monolayers are also extraordinary light

absorbers. MoS₂ can absorb up to 5–10% incident light at visible frequencies in a thickness of less than 1 nm, thus achieving one order of magnitude higher visible light absorption than GaAs.

Moreover, compared with classical direct-bandgap semiconductors, MoS₂ can offer additional advantages in the context of optoelectronics because of its optical transparency (~ 91% for monolayer in the visible range) and mechanical flexibility [22–24].

Together these outstanding properties make MoS₂ an ideal candidate for optoelectronic applications with primary progress demonstrated in field-effect transistors [25,26], light-emitting diodes [27], sensing [28], atomically thin photodetection platforms [29,30] and flexible electronics [31,32]. Most notable examples have included the demonstration of up to a 10% absorption of sunlight for monolayer MoS₂ [33]. Chapter 3 of this thesis demonstrates the growth of MoS₂ on a novel substrate that enables its subsequent transfer to flexible substrates.

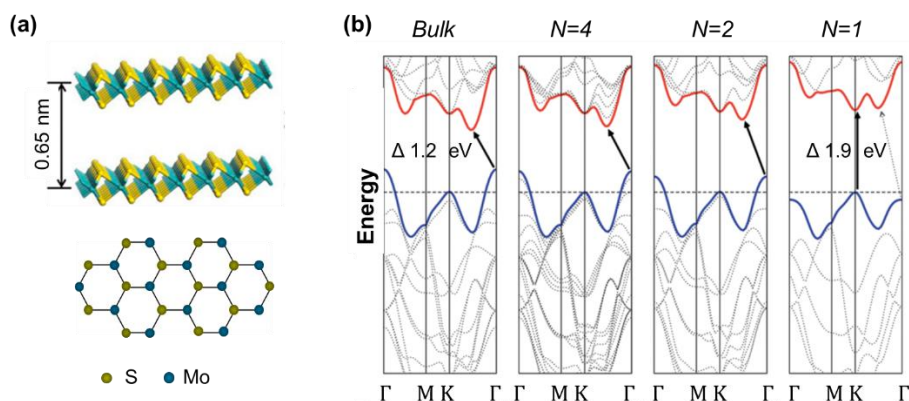


Figure 3 (a) Chemical structure of two layers of MoS₂ (b) Energy dispersion (energy versus wavevector k) in bulk, quadrilayer (4L), bilayer (2L) and monolayer (1L) MoS₂ from left to right, where N indicates the number of layers. The horizontal dashed line represents the energy of a band maximum at the K point. The red and blue lines represent the conduction and valence band edges, respectively. The solid arrows indicate the smallest energy transitions. There is an indirect transition for bulk and few-layer crystals that becomes a direct transition for a monolayer MoS₂. Adapted from Reference [34]

2.1.2 hBN and layered 2D materials

Among other 2D materials, hexagonal boron nitride (hBN) is notable. It shares the same honeycomb structure as graphene, but with a distinction where the sublattice symmetry is disrupted by the substitution of boron and nitrogen atoms at the A and B sublattice positions, respectively. It has a wide band gap (5–6 eV) making it an insulator [35]. It has good thermal conductivity (751 /m·K) and is regarded as a good candidate for dielectric layer in conjunction with Si/SiO₂ substrate or direct growth substrate because of its atomically flat surface and the lack of dangling bonds and charge impurities at the surface [36–39]. hBN is also used as an encapsulation layer for other 2D materials due to its impermeability, chemical inertness, and thermal stability [40–42]. In addition to the extraordinary fundamental properties that arise at low dimensions, the ability to combine or stack isolated 2D materials into multilayer heterostructures gives rise to artificial materials which often reveal unusual properties and new physical phenomena [43,44].

2.2 Ultrathin metal films and nanostructures

Similarly, ultrathin metal films (UTMFs), with thicknesses below 10 nm, are another class of materials which produce interesting electrical and optical properties (e.g. high optical transmittance, high conductivity and low sheet resistance and strong plasmons [45]) at low thickness. Moreover, their deposition on a wide variety of substrates (e.g. rigid and flexible) [46,47] makes them attractive in a number of optoelectronics applications including transparent conductors [48,49], photovoltaics [50], low emissivity windows [51], infrared absorbers [52], plasmonic metasurfaces [53], and point-of-care biosensors [54] to name a few. This thesis is concerned with nanostructured UTMFs, which are obtained after thermal annealing treatments of UTMFs < 5 nm thickness. The following sections describe the processes of UTMF growth, their subsequent nanostructuring and applications.

2.2.1 Ultrathin Metal Film (UTMF) growth

The ultrathin films (UTMFs) in this thesis were grown by sputtering, a technique which will be described in [Section 3.2.2](#). The growth of ultrathin films follows three stages (1) nucleation, (2) coalescence (3) thickness accumulation. During nucleation, incoming particles interact and adhere to the substrate forming nucleation sites. During coalescence, the nucleation sites grow to form interconnected islands. At this stage the film shows a high roughness and inhomogeneity. Further deposition increases the thickness of the material until a uniform film is obtained. The interaction energy between the incoming particles and the uncovered substrate surface and existing particles determines the growth mechanism, which determines the final properties of the film such as surface roughness and electrical conductivity.

According to the criteria developed by Bauer [55], there are three different growth modes that can be observed in the nucleation stage. The modes, presented in [Figure 4](#), depend on the surface free energy of the substrate ($\gamma_{\text{substrate}}$), the free energy of the interface ($\gamma_{\text{interface}}$), and the free energy of the film (γ_{film}). Under equilibrium conditions, the growth mode is determined by the so-called wetting factor, Φ , which is influenced by the competition between the surface and interface energies:

$$\Phi = \gamma_{\text{film}} + \gamma_{\text{interface}} - \gamma_{\text{substrate}} \quad (2.3)$$

If the interaction between the deposited atoms and the substrate is stronger than the interaction between the adjacent deposited atoms ($\Phi < 0$), a complete wetting of the substrate is observed leading to the formation of a uniform, layer-by-layer (or Frank-Van der Merwe) growth ([Figure 4c](#)). In most cases, the free energy of the interface is larger than the substrate free energy ($\Phi > 0$). Under these conditions, the adjacent incoming particles interact more strongly with each other than with the substrate leading to a 3D island like (or Volmer-Weber) growth ([Figure 4a](#)). A third hybrid growth mode, known as the Stanski-Krastanov mode, arises during the crossover from 2D to 3D growth, which occurs above a critical

thickness when the free energy relation switches from: $\gamma_{\text{film}} + \gamma_{\text{interface}} \leq \gamma_{\text{substrate}}$ to $\gamma_{\text{film}} + \gamma_{\text{interface}} > \gamma_{\text{substrate}}$. This is shown in Figure 4b.

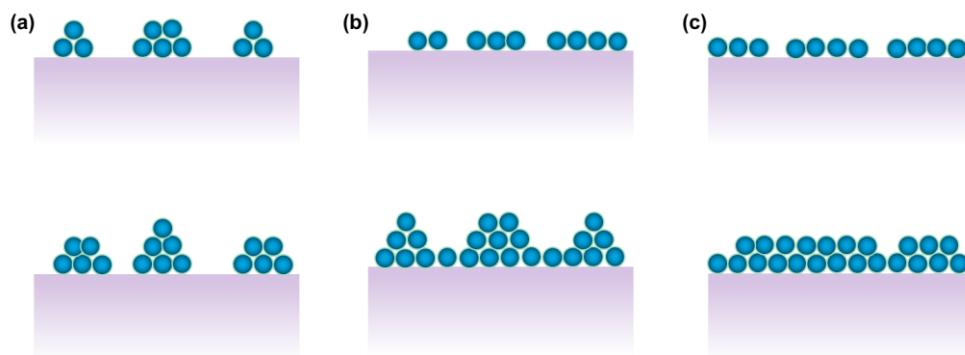


Figure 4 Schematics of three kinds of thin-film growth modes. a) Volmer-Weber mode (3D island growth). b) Stranski-Krastanov mode (layer plus island growth). c) Frank-van der Merwe mode (layer-by-layer growth).

The efficient adhesion of the UTMF on dielectric or semiconductor substrates is essential in applications and research within plasmonics, metamaterials, 2D materials and nano-electronics. Noble metals such as gold, silver and copper are often used for these applications, however they adhere poorly to the substrate, leading to phenomena like island-formation, delamination, peeling, and time-dependent device performance deterioration.

A technique widely employed to improve adhesion and suppress the 3D growth modes of UTMFs is seeded growth. This relies on the deposition of an ultrathin seed layer onto the growth substrate that dramatically changes the wetting factor (Φ) and subsequent growth of UTMFs thereby reducing their percolation thickness, that is the thickness at which the UTMF becomes physically connected and electrically conductive [56–59]. Seeded growth is particularly useful for improving the adhesion between metals and oxide substrates such as glass. In this thesis, titanium (Ti) is used for the seed layer for the deposition of gold contacts and Cu UTMFs in Chapter 4 and Chapter 5, respectively.

From a thermodynamics point of view a criterion for good adhesion between a metal film and an oxide substrate is that the metal must be oxygen negative to react chemically with the oxide surface, to form a strong covalent oxide bond. In other words, when the enthalpy of formation (ΔH_f^\ominus) for the metal oxide is less than that of SiO_2 , it indicates a favorable condition for the formation of a covalent oxide bond between the metal and the oxygen atoms in the glass. In this context, enthalpy of formation (ΔH_f^\ominus) for titanium oxide (TiO) $<$ ΔH_f^\ominus silicon dioxide (SiO_2) $<$ ΔH_f^\ominus copper oxide (CuO) and therefore, Ti would favorably form an oxide layer with the glass while Cu would not due to the improved oxide forming ability of the Ti seed layer with the glass [60]. In this thesis, 1-3 nm of Ti is deposited as a seed in order to achieve the optimum gradation from TiOx at the glass interface to fully metallic at the Ti/Cu or Ti/Au interface such that a good adhesion between Ti and metal is obtained.

2.2.2 Nanostructured UTMFS

UTMFs deposited through physical vapour deposition are generally unstable or metastable in the as-deposited state. When provided with sufficient thermal energy, the activation barrier for atomic diffusion is overcome and mass transport and capillary forces drive the film to agglomerate (dewet) into nanoparticles, [Figure 5](#) [61]. This process can occur well below the metal's melting temperature, which maintains the dewetted material in the solid-state and permits the use of various materials as a substrate. Dewetting typically starts on defects, holes, contamination sites or directly from the edges of the substrate. From there, it expands over the hole formation until it breaks up into nanoparticles. By changing the dewetting process parameters including for example, time and temperature, initial UTMF thickness or chamber atmosphere, it is possible to tailor the resulting dewetted nanoparticles' shape, size and coverage of the underlying substrate. The kinetics and thermodynamics of the metal dewetting process is described in detail in reference [62]. The tunable properties of dewetted UTMFs are demonstrated in Chapter 3 for a transparent surface.

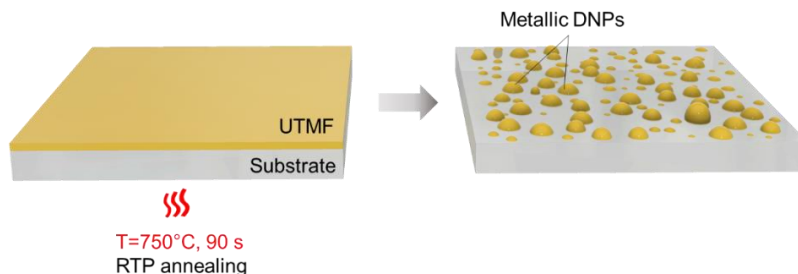


Figure 5 Representation of the solid-state dewetting process. A uniform thin film self-assembles into isolated islands when rapidly heated. The initial UTMF thickness, annealing temperature and the duration of thermal treatment, together with the material composition of the film, will affect the distribution and size of the nanoparticles.

Optical properties of nanostructured metals

For noble metals, such as Au and Cu, the Drude model [63,64] gives a good description of the dielectric constant in the near-IR region, but it breaks down in the visible to near-UV due to the onset of interband transitions from lower-lying d-bands to the sp-hybridized conduction bands. The onset of the interband transitions is at ~ 2.1 eV for Cu [65]. The interband transitions give a frequency dependent damping, and can be included in the dielectric function by adding additional Lorentzian terms. The Lorentz–Drude dielectric model is then given by the combination of the Drude component and Lorentzian contribution. Sub-wavelength sized NPs also have additional damping effects that arise from scattering of electrons with the surface of the NP.

Localised surface plasmon resonance

Localised surface plasmon resonance (LSPR) is an outstanding optical property of metallic nanoparticles. When light is incident on a metal nanoparticle that has a size smaller or comparable to the incident light wavelength, it exerts a force on the conduction electrons. This causes them to move towards the NP surface. This movement of negative charge induces an electric dipole and creates an electric field inside the NP (also known as the restoring field) [68]. LSPR is the resonant collective oscillation of conduction electrons with respect to immobilized positive ion cores, as depicted in Figure 6a. The resonance frequency of metallic NPs corresponds typically to UV–Vis light and consequently, the LSPRs

lead to absorption bands in this region of the spectrum. At the LSPR wavelength, due to the charge separation at the surface of the nanoparticle a strongly enhanced electric field is generated locally around the nanoparticle (Figure 6b). There are large regions where the electric field generated by the NP is opposite to that of the light, leading to destructive interference and light extinction beyond the NP volume.

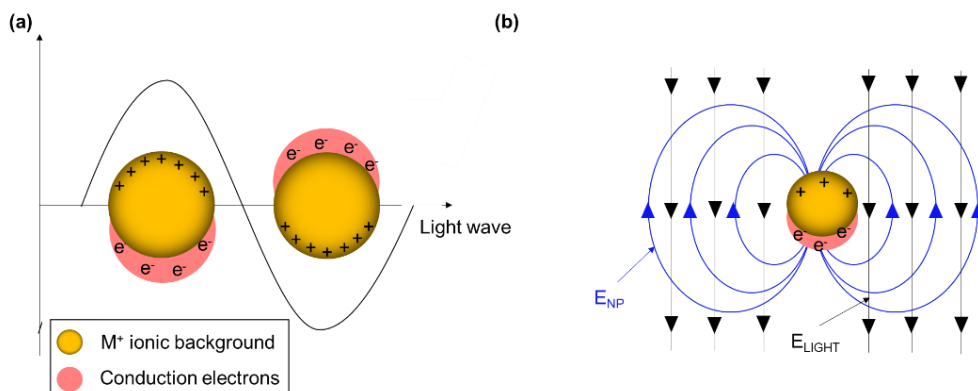


Figure 6 (a) Illustration of electric fields of incident light and those generated by the electron oscillations near the NP. Yellow shaded region indicated M^+ ionic background. (b) Schematic drawing of the interaction of an electromagnetic radiation with a nanoparticle. It generates a dipole that oscillates in resonance with the electric field of the incident light as well as a strong confined electric field at the nanoparticle surface.

The efficiency with which NPs extinguish light is given by the extinction cross section, σ_{ext} , which is the sum of the absorption and scattering cross sections. Light absorption has an exponential dependence with σ meaning that a small increase in σ leads to a huge light extinction. A light beam propagating through a medium containing NPs decays in intensity according to Eq. 2.4:

$$I(x) = I_0 \cdot \exp(-C \cdot \sigma_{ext} \cdot x) \quad (2.4)$$

where C is the number of NPs per unit volume, σ_{ext} is the extinction cross section and x is the distance travelled. This underpins the advantage of LSPR since the cross sections are much larger (up to 10 times their diameter of the NP) than compared with other optical transitions, for example interband transitions.

Effects of NP size, shape, dispersion and surrounding medium on the LSPR

The number, position, shape and intensity of LSPR of metallic nanoparticles can be tuned over wide spectral range by varying the size, shape, dispersion and surrounding medium of the nanoparticles.

Increasing the NP size induces a broadening and red-shift of the LSPR peak. This effect is attributed to a weakening of the restoring force because as the distance between charges on opposite sides of the particle increases, their interaction decreases.

The intensity of the LSPR is reduced by damping interactions induced by scattering mechanisms. Electron oscillations are damped by scattering off the ionic cores and with the NP surface. Whilst scattering with the ionic cores is a constant and independent of NP size, the scattering with the NP surface is highly size dependent.

The geometry of the metallic nanoparticles is also important in shaping the LSPR. The system studied in this thesis take a nanocap shape, having a flat base and rounded hemispherical cap. The asymmetry induces multiple polarisation axes, giving rise to transverse and longitudinal plasmons. As the restoring force is proportional to the charge accumulation at the NP surface, the LSPR of nanocaps is tunable by the aspect ratio (height to diameter) of the nanocaps.

Finally, the dielectric constant of the surrounding medium, ϵ_{medium} , affects the LSPR. The electric field that is induced in the region of the NP during the SP excitation, also induces a polarization of the surrounding media, that scales with ϵ_{medium} . This results in charge accumulation at the interface between the metallic NP and the dielectric media. This charge partially screens the charge accumulation due to the movement of conduction electrons in the NP, resulting in a net reduction in charge at the NP surface, and thereby a reduction in the restoring force. Reduced restoring force implies a reduced resonance frequency, therefore leading to a red shift with increasing ϵ_{medium} . In Chapter 3, this effect is demonstrated for Cu dewetted systems, in which a reduction in charge at the NP surface due to the interaction with the dielectric media (SiO_2) leads

to a decreased restoring force and, consequently, a red shift in resonance frequency as ϵ_{medium} increases.

2.3 Characterisation techniques

The optical, electrical and morphological properties of the ultrathin materials and nanostructured surfaces fabricated in this thesis were evaluated with a number of techniques. In this section, the methods and equipment used are described and divided into four different categories: optical, morphological, wetting and mechanical. The techniques are discussed by chapter.

2.3.1 Optical

When light is incident on a material, the fraction that is transmitted (T), reflected (R), absorbed (A) or scattered (S) depends on the materials' properties (dielectric constant and refractive index) and surface structure. The total contributions of T , R , A and S sum to 1. The optical properties are determined with several techniques explained briefly in the following sections.

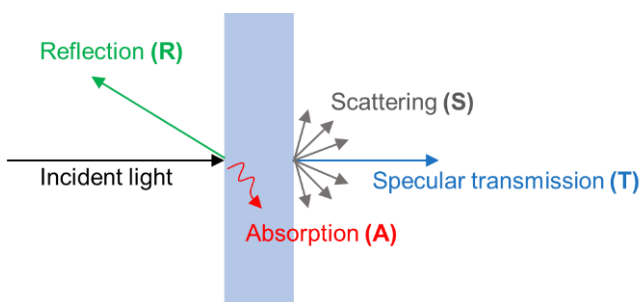


Figure 7 Optical processes occurring when light interacts with a semi-transparent surface

Transmission, reflection and absorption

A PerkinElmer Lambda 950 spectrometer in the UV–Visible region was used to measure the transmission and reflection of samples. The total transmission (%) = $(I/I_0) \times 100$, in which I is transmitted light intensity at a given wavelength or wavelength range, and I_0 is incident light intensity at

a given wavelength or wavelength range. In some aspects, the transmission is averaged over the wavelength range of 380-750 nm. The absorption (A) was calculated according to $A=100 - T - R$ (in the case of negligible scattering). Note that the substrate's contribution is always considered in optical transmittance measurements.

Haze

As used herein, the term “haze” refers to the percentage of transmitted light that is scattered so that its direction deviates more than 2.5 degrees from the direction of the incident beam. The haze should be kept as low as possible for applications requiring high transparency, for example touch display screens such as those proposed in Chapter 5. In this thesis, a Haze-Guard iPro system from BYK instruments was used to measure the haze. The sample is illuminated and all the transmitted light is measured by an integrating sphere. Only light scattered or dispersed at an angle greater than 2.5° is detected, as all forward directed light is excluded by a light trap.

Raman spectroscopy

Raman spectroscopy is a non-destructive optical measurement technique that enables chemical and structural characterisation of a sample. The underlying principle of Raman spectroscopy lies in the coupling of incident photons with the phonon modes of bonds within a material. Incident light can be scattered elastically (Rayleigh scattering) or inelastically (Raman scattering). Elastic scattering implies that the frequency of the emitted photon is the same as the frequency of the incident light. For inelastic scattering, the frequency of the scattered light is larger (anti-Stokes scattering) or smaller (Stokes scattering) than that of the incident light, which is called Raman scattering phenomenon. The majority of phonons within materials experience elastic scattering (around 10^{-3} times the intensity of the incident light) whilst only a fraction undergoes Raman scattering (around 10^{-6} times the intensity of the incident light). Light scattered from the material is passed through a filter which allows only the Raman scattered light to reach the detector. A spectrograph is placed in-between the filter and the detector in order to separate the Raman

Chapter 2: Ultrathin Materials Review

scattered light by frequency and thus acquire a fingerprint of the vibrational modes within a material.

In this thesis a, Renishaw InVia instrument was used with 532 nm laser. A reduction in the power radiation was selected in order to avoid heat damage on the samples. 50X lenses (with a numerical aperture of 0.75) were used throughout. In addition to single-point spectra, Raman maps of up to $1 \mu\text{m}^2$, were also acquired to enable a statistical analysis of larger samples areas. All Raman single-point spectra and maps presented in this thesis were treated by a custom MATLAB® code that combines ten or more spectra obtained from different areas of the sample and fits a single average Lorentzian peak to the relevant peaks, after a linear background subtraction.

Raman spectroscopy of MoS₂

In Chapter 3, Raman spectroscopy measurements are performed to determine the number of layers and quality of as-grown MoS₂, before and after performing the transfer from the growth substrate (NaCl) to the target substrate (PET). MoS₂ has two Raman active phonon modes, depicted in [Figure 8](#). The in-plane vibration (E_{2g}^1) provides information on the in-plane strain, while the out-of-plane mode (A_{1g}) depends on the interaction with its neighbouring material. The frequencies, peak widths and intensities of both Raman modes depend highly on the number of layers of MoS₂ [66]. As the number of layer increases, the E_{2g} vibration observed at $\sim 383 \text{ cm}^{-1}$ shows a red-shift (shifts to lower frequency) whereas A_{1g} vibration observed at $\sim 408 \text{ cm}^{-1}$ shows a blue-shift (shifts to higher frequencies) [67].

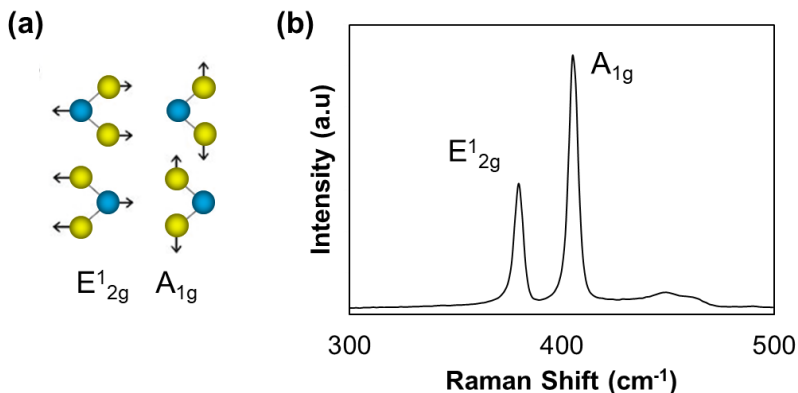


Figure 8 Raman vibrational modes E_{12g} and A_{1g} and representative Raman spectra of bulk MoS₂ with E_{12g} and A_{1g} peaks at 383 and 408 cm⁻¹. Spectra compares bulk and MoS₂, *(experimentally obtained).

Photoluminescence spectroscopy

Photoluminescence (PL) spectroscopy, similar to Raman spectroscopy, is a contactless fast and non-destructive optical technique to probe the electronic energy structure of materials. When the sample is excited, electron-hole pairs are produced. The electron is excited from the valence band to the conduction band and then relaxes to the band edge before recombining with the hole in a radiative emission process. As photons of particular energy are absorbed by the sample, the energy of the photons emitted can provide evidence of the electronic structure. In the case of MoS₂, where the band structure is layer dependent, PL can be used to determine thickness. Secondly PL spectra can also indicate material quality. If impurities are present in semiconductor materials, the defect energy levels would form near the conduction band or valence band. Depending on the type of impurities introduced, they could act as donor or acceptor of electrons in crystals and thus change the energy of the emitted photons.

In Chapter 3, single-point photoluminescence spectroscopy was performed using the Renishaw InVia instrument in order to obtain information regarding the quality of the MoS₂. The photoluminescence spectrum for monolayer MoS₂, (see [Figure 9](#)), shows two direct excitonic transitions, the so-called A1 and B1 excitons which appear at 1.85 eV (670

nm) and 1.98 eV (627 nm) and correspond to direct-gap transitions at the K-point of the Brillouin zone between the maxima of split valence bands and the minimum of the conduction band [34]. The ratio of intensities of the peaks is a quality indicator where a low B/A ratio indicates low defect density and high-quality growth and a large B/A ratio signals a high defect density and poor-quality growth [68].

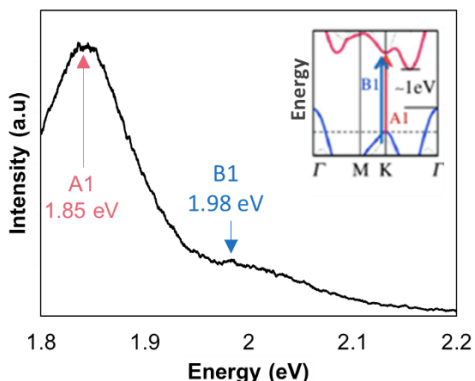


Figure 9 PL spectra of ultrathin MoS₂ (experimental data). The observed absorption peaks at 1.85 eV (670 nm) and 1.98 eV (627 nm) correspond to the A1 and B1 direct excitonic transitions. Inset adapted from reference [34]

2.3.2 Electrical

The following section provides the methodology used for the electrical characterisation of graphene samples and devices fabricated in Chapter 4.

Measurement of sheet resistance

The electrical properties of graphene films are typically described in terms of their sheet resistance, R_s , which for a film with resistivity, ρ , and thickness, t , is defined as,

$$R_s = \frac{\rho}{t} \tag{2.5}$$

As ρ is a measure of the resistance per unit volume of the bulk material, R_s is a scaling independent unit, meaning that it does not depend on the film's lateral dimensions (only on its thickness), and is typically denoted in units of Ohms per square ($\Omega/\text{sq.}$). R_s can be directly measured using a

four-point probe set-up. This technique is the most common approach for determining the DC electrical properties of films since it is not affected by parasitic resistances, such as contact resistance, probe resistance or resistances under the probes [69]. There are several configurations in which the measurement can be performed.

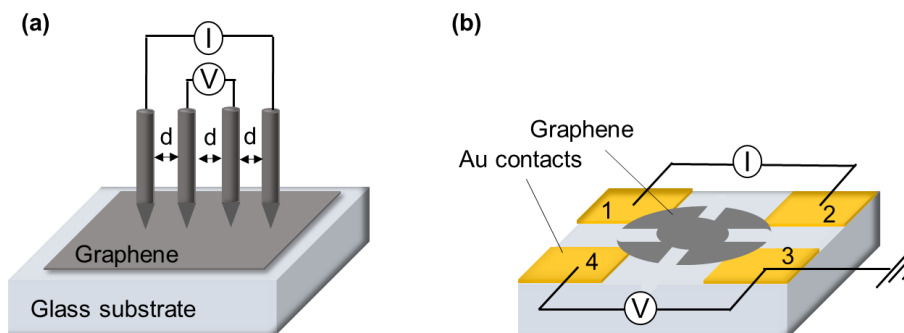


Figure 10 Schematic of the Four Point probe set-up used for the R_s measurement in (a) colinear configuration and (b) Van-der-Pauw configuration with cloverleaf shaped graphene.

For large area graphene samples, in the order of 1cm^2 , a fixed Cascade Microtech 44/7S 2791 linear four-point probe set-up connected to a Keithley 2001 was used, as shown in Figure 10a. The tips are brought into contact with the graphene surface, a test current (I) is injected through the outer tips while the inner tips measure the voltage drop (V), as shown in Figure 10a. In this case, R_s is calculated as,

$$R_s = C_1 * C_2 * R_m \quad (2.6)$$

where R_m is the measured resistance value, and C_1 and C_2 are corrective coefficients which are related to the ratio between the distance between tips (d) and the graphene thickness (t), and the ratio between ' d ' and the sample lateral sizes, respectively (for more details see Ref.[69]). In our case C_1 is approximated to be 1 as the thickness of the graphene is (0.345 nm) is much smaller than the tip separation, $d = 1\text{mm}$, and the area of the graphene (typically 1 cm^2) is much larger than the tip separation. $C_2 = \pi/\ln(2) = 4.4364$.

For precise measurements of the sheet resistance, a Van der Pauw configuration was used, which allows the electrical conductivity of thin samples with arbitrary shapes to be determined. In this configuration, samples were prepared with 50 nm thick Au rounded contacts 1-4, as shown in [Figure 10b](#). A voltage is applied between two parallel contacts and the current is measured between the remaining two. The area of contact between the metallic pads and the graphene must be infinitesimally small in order to avoid measurement errors [70]. A cloverleaf structure with rounded corners was chosen as it has been shown to be more robust against possible sample defects. In this case, the R_s values are

$$R_s = \frac{\pi}{\ln(2)} * R_m \quad (2.7)$$

where R_m is the measured resistance value.

Measurement of the carrier density

The quantum Hall effect in graphene allows for a direct measurement of the graphene carrier density, when it is exposed to a perpendicular external magnetic field, B . The underlying principle of the Hall effect arises from the Lorentz force (F_L), which describes the force exerted on a charged particle, such as an electron, when moving through a magnetic field (B).

$$\vec{F}_L = q_e(\vec{E} + \vec{v} \times \vec{B}) \quad (2.8)$$

Where q_e is the elementary charge (1.602×10^{-19} C), v is the particle velocity and E is the electric field. When B is oriented perpendicular to the direction of the applied electric field, the electron experiences a force that is perpendicular to both the direction of motion and the orientation of the B . The result is that a certain number of charge carriers (n_s) will accumulate at the edge of the device and a transversal Hall voltage (V_H) will appear ([Eq. 2.9](#)), where I is the current injected.

In this work R_s , n_s and μ of the Hall bar devices shown in design B of [Figure 11](#) was carried out at 300 K in a Physical Property Measurement System by Quantum Design as follows. A constant DC current of 1 μ A was injected into the sample via probes 1-2 whilst probes 3-4 and 3-5 measured the

longitudinal (V_{34}) and transverse ($V_{35 \text{ (Hall)}}$) voltage, respectively, during a perpendicular magnetic field sweep (-5 T to 5 T) at 300 K . The subscripts indicate the contact pads shown in [Figure 11b](#). From the longitudinal voltage (V_{34}), the sheet resistance (R_s) was determined at zero magnetic field by Ohms law according to [Eq. 2.10](#), where ‘W’ and ‘L’ correspond to the width ($140 \text{ }\mu\text{m}$) and length ($300 \text{ }\mu\text{m}$) of the graphene area, respectively. The n_s was obtained from the slope of the linear fit between the transversal voltage (V_{Hall}), and the magnetic field (B), according to [Eq. 2.11](#) where q_e is the electron charge ($1.6 \times 10^{-19} \text{ C}$) and I_{DC} is the constant DC current, ($1 \text{ }\mu\text{A}$). If the slope is negative, the graphene is n-type doped (excess of electrons), while if the slope is positive, it is p-type doped (excess of holes). Assuming the Drude model of conductivity [71], the mobility (μ) was calculated by [Eq. 2.12](#). Finally, the Fermi level, E_F , was calculated from the n_s according to [Eq. 2.13](#), where \hbar is reduced Planks constant, v_F is the Fermi velocity, k_F is Fermi wave vector which is equal to $\sqrt{\pi n_s}$ and $n_s =$ number of additional charge carriers.

$$V_H = I \cdot B / q_e \cdot n_s \quad (2.9)$$

$$R_s = V_{3,4} / I_{1,2} \quad (2.10)$$

$$n_s = I_{\text{DC}} / q_e \cdot (\Delta V_H / \Delta B) \quad (2.11)$$

$$\mu_H = 1 / q_e \cdot n_s \cdot R_s \quad (2.12)$$

$$E_F = \hbar v_F k_F = \hbar v_F \sqrt{\pi n_s} \quad (2.13)$$

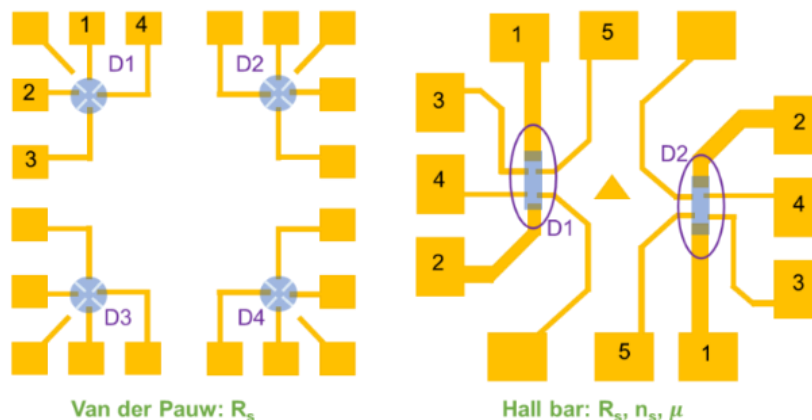


Figure 11 Device designs fabricated in this work. In design A the graphene cloverleaf has a diameter of $300\ \mu\text{m}$. In design B, the Hall bar has dimensions $140 \times 300\ \mu\text{m}$.

2.3.3 Morphological

SEM

SEM was used in this thesis to investigate properties and structure of materials (MoS_2 , dewetted nanoparticles). In this thesis, a SEM (FEI Inspect F) was used for the imaging of CVD grown MoS_2 and dewetted silver nanoparticles in Chapter 3 and for embedded Cu dewetted nanoparticles in Chapter 5.

AFM

Atomic force microscopy (AFM) enables a visualisation of the surface topography at the atomic scale. This technique was used in Chapter 3 to measure the surface roughness of substrates after post-treatment. The principle relies on measuring a mechanical frequency change of an oscillating micron-scale cantilever due to interactions with the surface, such as Van der Waals, capillary or electrostatic forces. In this work an AFM Bruker/Veeco Dimension 3100 was used for topography measurements.

2.4 Transparent optoelectronic and biological applications

The properties of 2D and ultrathin materials, such as large specific surface area, flexibility, electrical conductivity, optical transmittance and reflectance, and tunability together with their unique sensitivity to changes in the environment make them compelling materials for the active components or supporting substrate in applications across a broad range of sectors from electronics, to energy harvesting, storage and conversion, optical displays, biomedicine and health. This thesis is dedicated to the development of low temperature fabrication and processing techniques to obtain 2D materials on substrates of technological interest. Two promising applications are demonstrated: the first is increasing the electrical conductivity of transparent surfaces made of graphene while the second is increasing the antimicrobial functionality of transparent surfaces made of nanostructured copper. The following provides a brief summary of applications of 2D and nanostructured materials that could benefit from the low temperature processing and transfer techniques before reviewing in detail the applications developed in Chapter 4 and Chapter 5.

UTMFs are widely used in transparent optoelectronic applications as transparent conductors (TCs) [48,49] in photovoltaic cells and low emissivity windows [51] as well as plasmonic meta-surfaces [57]. On the other hand, metallic dewetted nanoparticles (DNPs) can be used as a mask to pattern glass surfaces (SiO_2) via reactive ion etching (RIE), allowing the fabrication of large area nanopillars and nanoholes, which have shown unprecedented optical properties such as anti-reflection [72] and increased transparency, as well as self-cleaning properties [73]. Moreover, when large nanopillars are fabricated, surface phonon-polaritons on glass can be excited i.e. increase the optical emissivity in the infrared (IR) optical range, allowing the use of these surfaces for passive radiative cooling [74]. In another example, DNPs can be fabricated with the right dimensions to promote visible light scattering for the fabrication of antiglare surfaces [75]. Finally, antimicrobial metals, for example copper or silver, could be

nanostructured on glass substrates for the fabrication of transparent antimicrobial, self-cleaning, anti-viral and antifouling surfaces.

2.4.1 Transparent electrodes

The first application of this thesis is developing highly conductive transparent surfaces that could be used as transparent electrodes. A transparent electrode (TE) is a key component of any optoelectronic or transparent device. With an increasing number of large area applications, there is growing demand to replace the conventional oxide based transparent conducting films with nanomaterials, primarily to reduce the cost. When light photons have to pass through an active material, the electrode(s) hosting the active material must be transparent to light photons. Display screens, for example, use TEs to carry electrical signals while rendering the display visible. Touchscreens, on the other hand, use TEs both to keep the display visible and also to convert touch into electrical signals [76]. Solar cells utilise TEs to collect photons and extract charge carriers generated due to the photovoltaic effect [77]. TEs are also used as transparent heaters in defogging and defrosting applications [78].

In many cases, electrical conductivity and optical transmittance are the most important performance indicators for TEs. Currently, the state of art TEs are large bandgap semiconductors heavily doped with metals, known as transparent conductive oxides (TCOs). TCOs show high transparency in the visible (VIS) range together with excellent electrical properties. Among the TCOs, indium tin oxide (ITO) is the most widely used with a sheet resistance, R_s around $10 \Omega/\text{sq.}$ at an optical transmittance, $T_r = 85\%$ [79]. However, the use of ITO as a transparent electrode suffers from several drawbacks: 1) it contains Indium, which is a high cost scarce material, 2) it requires complex fabrication and high annealing temperatures to reduce its resistivity making it difficult to integrate at an industrial scale, 3) it is incompatible with certain organic materials (active components of e.g. solar cells) due to indium and/or oxygen migration from In_2O_3 [80], 4) it is brittle which makes it unsuitable material for flexible applications where bending is desired, and, 5) ITO has a band gap of 3.75 eV (331 nm) which results in absorption of radiation at ultraviolet (UV) wavelengths. In

addition, due to plasmon resonances, ITO becomes reflective in near infra-red region (NIR) [77]. Thus, the poor, transparency in UV and IR region of the spectrum precludes the use of ITO in certain applications such as (IR) pyroelectric detectors, solar cells for space applications and (UV) photodiodes and LEDs. In this regard, the search for 2D material-based TEs has been developed with primary progress achieved with thin (< 10 nm) metal films [48,81–83], silver nanowire films [84,85], conductive polymers [86–88] carbon nanotube films [89–91] and graphene [92–98].

Pristine graphene has an optical absorption of $\pi\alpha = 2.3\%$ per layer. Thus, three layers of pristine graphene could theoretically achieve the industrially competitive standard of $10\Omega/\text{sq.}$ at 94% transmittance (equivalent to ITO) [99]. Unfortunately, in practice, the R_s of large area graphene is typically much higher, in the order of ~ 1 -2 k Ω , due to a high scattering rate resulting from wrinkles, defects and domain boundaries. As a result, real graphene films used in devices are not nearly as conductive. The best values reported in the literature are: $R_s = 30 \Omega/\text{sq.}$ at $Tr = 90\%$ for graphene multilayers [100,101], $R_s = 125 \Omega/\text{sq.}$ at $Tr = 97.7\%$ [102,103] and $8.8 \Omega/\text{sq.}$ at $Tr = 84\%$ [104], for chemically doped graphene.

Despite these practical challenges, graphene is still recognised as a promising TE material as it offers superior thermal conductivity and mechanical flexibility enabling more efficient heat dissipation and compatibility with flexible substrates. Furthermore, for some applications such as touchscreens, photodetectors which carry little current, obtaining an ultralow conductivity is less important.

In addition, with recent developments in doping techniques, highly n-doped graphene is promising as low work function electrodes for energy conversion and electron emission applications such as solar cells [105,106] and touchscreens [100]. In Chapter 4, we demonstrate a method of obtaining highly conductive n-doped graphene on glass, while, in Chapter 3 we provide a growth and processing technique for ultrathin materials at low temperatures. This can enable the incorporation of ultrathin materials based TEs on low strain point flexible substrates for a

range of emerging flexible optoelectronic and photonic devices in the health, electronics and energy related industry.

2.4.2 Transparent antimicrobial (AM) surfaces

The second application developed in this thesis are transparent AM surfaces. Transparent touch screen applications is increasingly in demand. Whilst only a decade ago, only smartphones bore touchscreens, nowadays touchscreens can be found in a variety of settings, from train station ticketing machines to self-service kiosks. In parallel, the recent COVID19 pandemic has changed the world attitude towards the hygienic use shared surfaces, which are used by many people in a short space of time and therefore have an increased potential to harbour harmful bacteria. The demand for safer screens has motivated a surge of intense and recent efforts towards imparting antimicrobial functionality into glass, this being the most widely used substrate for touch screens [107].

Whilst historically metals such as copper and silver have been used for their inherent antimicrobial properties [108–111], these metals are not suitable for applications requiring a high level of transparency. In this regard several strategies have been developed with primary progress being achieved by metallic nanoparticle coatings, antimicrobials polymers and photoactivated metal oxide coatings. One market leader in the field is Kastus® Technologies who uses the latter method for AM coatings range. However, due to the high temperature (>600 °C) used for fabrication of the coatings, this option is not suitable for some substrates. Thus, challenges remain in low temperature fabrication for low strain point (glass transition temperature) plastics and thin glass. Chapter 5 provides a full review of the current state-of-the art solutions for transparent AM surfaces and describes the method developed in this thesis to obtain highly durable transparent antimicrobial coating at temperatures <400°C using metal dewetting techniques.

Chapter 3

Low temperature growth and processing techniques for MoS₂ and metal nanostructures

The information, text and figures in this chapter have been adapted, under the terms of the Creative Commons Attribution-Non-Commercial license, from the original publications: C. Graham et al. ‘‘NaCl substrates for high temperature processing and transfer of ultrathin materials’’ Scientific Reports (10)1 7253 (2020) & C. Graham et al. (2023) ‘‘Durable, transparent and antimicrobial nanostructured surfaces on glass’’ (Under Review).

3.1 Introduction

Ultrathin materials and nano-structures are key elements in developing functional surfaces for, e.g. electronic and optoelectronic devices, display screens, light emitting diodes, smart windows and photovoltaic cells. However, their deposition and processing often necessitate high temperatures, which are not compatible with a direct fabrication onto the target substrate. For example, polymers are widely used as a supporting layer but unfortunately have low strain-point temperatures. In this chapter we develop low temperature growth and processing techniques for ultrathin and nanostructured materials including graphene, MoS₂ and nanostructured metals. In [Section 3.2](#), we overview the fabrication techniques. In [Section 3.3](#) we demonstrate a low temperature fabrication

of Copper (Cu) dewetted nanoparticles (DNPs) by a metal dewetting process in order to obtain a coating with a transparency independent of wavelength. The coating is fabricated directly on a low strain point glass substrate that is relevant for use in cover glass for display applications. In [Section 3.4](#) we introduce a novel, simple and fast technique to obtain thin materials and nano-structures requiring high temperature processing onto low strain-point (glass transition temperature) substrates. The innovations presented in this chapter mark progress towards the realisation of functional transparent surfaces on flexible substrates.

3.2 2D materials fabrication techniques

Since the exfoliation of graphene in 2004, and subsequent expansion of the 2D materials family, several techniques have been developed in order to produce high quality 2D materials on a large scale. These techniques are briefly summarized below, focusing mainly on Chemical and Physical Vapor Deposition (CVD and PVD, respectively) processes that also feature in this thesis.

3.2.1 CVD growth

CVD is a chemical process in which the deposition of the target material onto the substrate is controlled by a chemical reaction between powdered and/or gaseous precursors which are heated inside a furnace at high temperatures (>500 °C). Most CVD material growth relies on the pyrolytic decomposition of precursors on the substrate surface after adsorption. The decomposition of the precursor results in the generation of new surface adsorption sites and enables thereby a continuous growth of the desired material. The reaction is performed at temperatures greater than the pyrolytic decomposition threshold of the precursor in order to enable continuous film growth. [Figure 12](#) shows a schematic of the CVD which takes place in the following 3 stages i) adsorption, decomposition, and desorption of precursor molecules on the substrate surface; ii) diffusion and reaction of atoms or molecules from the decomposed precursor on the substrate surface; iii) the nucleation and

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

growth of the 2D material templated by the substrate. The thermodynamics and kinetics of growth, and the resulting material thickness, quality and morphology, is highly dependent on parameters such as precursors used, the carrier gas flow rate, temperature, pressure, and type of substrate.

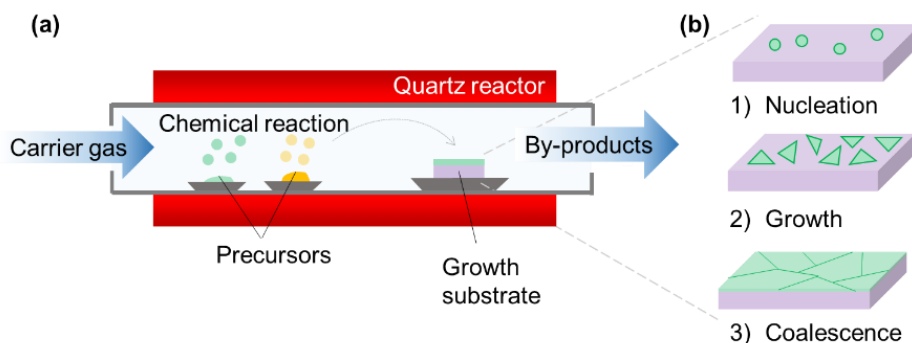


Figure 12 The schematic of a tube CVD system. (b) 2D film growth process: first, the nucleation is formed as the growth centre of grain domains; second, the growth of the 2D grain domains; third, the 2D domains coalesce to form a continuous film

To date, CVD has been employed to grow a range of large-area high quality 2D materials. The most prominent examples include transition metal dichalcogenides, including several to monolayer MoS₂ [112], and graphene [100] where lateral dimensions of up to 6 and 30-inches, have been demonstrated. The development of transfer techniques (detailed in [Section 3.4](#)) has enabled the growth materials to be transferred onto a range on functional substrates. Furthermore, with CVD it is possible to directly grow materials on substrates with complex and patterned geometries. Besides the parameters of precursors, temperature and time, CVD techniques have witnessed further advancements with the use of seeding promoters [113], sacrificial layer catalysts [114] and magnets [115] to precisely control the growth and quality of the materials obtained.

3.2.2 PVD techniques: Sputtering & Evaporation

Sputtering is a PVD technique that uses electrical energy to release a material from a source and deposit it onto the substrate. The target material goes from a solid to vapour phase and then back again to a solid phase, as a thin film. The basic operation of sputtering consists of introducing a process gas (Ar in this thesis) into a high vacuum ($\sim 10^{-8}$ Torr) chamber. Then an electric field is applied between the target, which contains the material to be sputtered, and the substrate, as shown in [Figure 13a](#). This electric field ionizes the Ar gas, creating a plasma of Ar⁺ ions. These positive charges are accelerated towards the target placed at the bottom of the chamber and collide with the target, detaching particles, which are then deposited on the substrate. The quality of thin films obtained by this method is governed by a number of parameters, including deposition rate, pressure of the process gas, initial vacuum level, and substrate material and temperature, to name a few. In this thesis, we used a computer controlled, automatic RF/DC magnetron sputtering system from AJA International Incorporation.

Thermal and electron beam (e-beam) evaporation are also physical vapour deposition (PVD) techniques. In thermal evaporation, [Figure 13b](#), a solid target is heated to a temperature beyond its melting point, producing the vapor phase of the material, which is then coated onto the substrate in the solid phase. In this thesis, films were thermally evaporated under high vacuum ($\sim 10^{-8}$ Torr) in a system from Kurt J Lesker. In e-beam evaporation, [Figure 13c](#), a high voltage source produces a stream of electrons which bombard and melt the target material producing the vapor phase which is subsequently deposited on the substrate as a solid film. The deposition rate is controlled by the voltage applied to the target material where the voltage is proportional to the thermal energy produced.

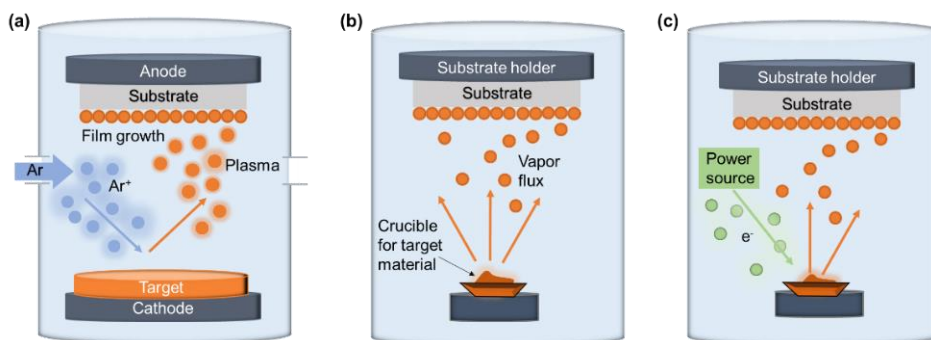


Figure 13 PVD techniques (a) sputtering; (b) thermal evaporation; (c) E-beam evaporation

3.3 A low temperature metal dewetting process to obtain highly transparent DNPs on low strain point glass

Metal dewetting is a low-cost technique to create nanostructured metals on transparent silica surfaces without the need of complicated multistage lithographic techniques [75,116,117]. The dewetted nanoparticles (DNPs) are typically obtained by a rapid thermal annealing process at temperatures in excess of 600°C, as explained in [Chapter 2, Section 2.2.2](#). The resulting DNP array carries a signature extinction (absorbance and reflectance) associated with the plasmonic resonance of the particles. For some applications, it is desirable to reduce the absorption and/or reflection in order to obtain a surface with a high transparency independent of wavelength; i.e. reduce colour. The light absorption, reflection, transmission and colour by the nanoparticles is tunable by the size (diameter) and shape (contact angle) of the DNPs [47]. These parameters can be controlled by the dewetting temperature, the duration of the thermal treatment used to induce dewetting, the initial UTMF thickness and substrate type [118].

In this Section, we utilise a low temperature annealing of Cu UTMFs i.e. sufficiently close to the temperature at above which dewetting of the

continuous film is observed and below the glass strain point of the substrate (580°C). By doing so we intentionally introduce a degree of inhomogeneity into the contact angle, size and morphology of the particles obtained such that the plasmonic resonance effect on the colouring of the coating is kept within acceptable values. To provide a comparison and demonstrate the advantage of low temperature dewetting, electromagnetic simulations of the high (750°C) and low (390°C) temperature dewetting cases were performed together with a comparison to the experimental optical spectra. Cu is chosen as the precursor UTMF, but the technique could also be applied to metals such as silver and gold.

3.3.1 Electromagnetic simulation of the individual DNPs

The optical response of individual nanocaps is simulated using the Finite Element Method with commercial COMSOL Multiphysics® software [119]. A 2-D array of nanoparticles was chosen as physical model, considering periodic boundary conditions on the edges of a unit cell. The unit cell is then composed by the substrate, i.e. fused silica, 1-nm thin layer of metallic Ti and a single Cu nanoparticle in air properly shaped. For the nano particles obtained at higher dewetting temperature the period of the system is set to 120 nm. For the lower dewetting temperature case, 230 nm has been used for the periodic condition. The geometric parameters of the unit cell, including particle geometry, particle base diameter and contact angle were considered according to a statistical analysis of the representative sample SEM images [Figure 14c](#), using the Fiji distribution of ImageJ software [120]. The model input parameters are listed in [Table 1](#). The particles were described as spherical nanocaps and assume fixed and average values of the copper-on-silica contact angle and base diameter for high and low temp dewetting cases, respectively. For the high temperature samples, the nanoparticle shape was made to be more rounded and the nanoparticles density lower while the model for the low temperature samples is composed by flattened nanoparticles and higher density. The metal dielectric function for Cu is taken from McPeak et al. [121], the one for Ti from Johnson and Christy [122] while for air we

set fixed values of the refractive index ($n=1$) and extinction coefficient ($k=0$) and for the substrate $n=1.45$ and $k=0.0001$. The mesh chosen is a free-triangular mesh that is finer at the boundaries between different materials with the smallest domain equal to 3nm in the nanoparticle and at the interface between the substrate and air. The wavelength range used for the simulation is 380 – 750 nm with a step of 35 nm. Note that since the theoretical model is based on a simplified 2D array of Cu nanoparticles, it enables a qualitative rather than quantitative comparison to experimental data, whilst still reproducing the experimental trends.

Table 1 Statistical Parameters for two fabricated Samples with UTMF of 3.5 nm Cu annealed at 390 and 750 °C, respectively, as extracted by SEM Image Analysis in ImageJ. Standard deviation follows the '±' symbol.

Annealing temperature (°C)	Average base diameter (nm)	Average particle height (nm)	Average particle contact angle (°)
390	117 ± 38	64 ± 20	35 ± 12
750	62 ± 24	42 ± 21	74 ± 23

3.3.2 Discussion

Experimentally we observed that: (i) low temperature produces flatter particles with a lower contact angle, (ii) particles are much closer together, and in some cases, in contact with each other (Figure 14a), (iii) high temperature annealing produced the typical narrowband resonance centred around 580 nm with pinkish colour while the same process at low temperature produces a broader resonance at longer wavelength with paler bluish colour (Figure 14b). The simulated optical spectra (Figure 14c) are in good agreement to the experimental observations. Without wishing to be bound by theory, it is believed that the broadening and red-shift of the plasmonic resonance in the low temperature annealing case may arise from a combination of two effects: the first may be that low temperature produces flatter particles with a lower contact angle; the second may be that particles are much closer together or in some cases touching (Figure 14a), this being consistent with previous work [47].

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

The change in particles' structure and associated optical response give the coating a transparency without strong dependence on wavelength. We have also measured low scattering (haze) < 1%. Thus, the colour of the Cu UTMFs as a whole remains visually close to the neutral colour of the substrate against white and coloured text backgrounds and has a transmission between 70-80% that is substantially independent of wavelength in the visible range. The inset of [Figure 14b](#) demonstrates that the visual appearance is such that the functionality of transparent devices would be retained.

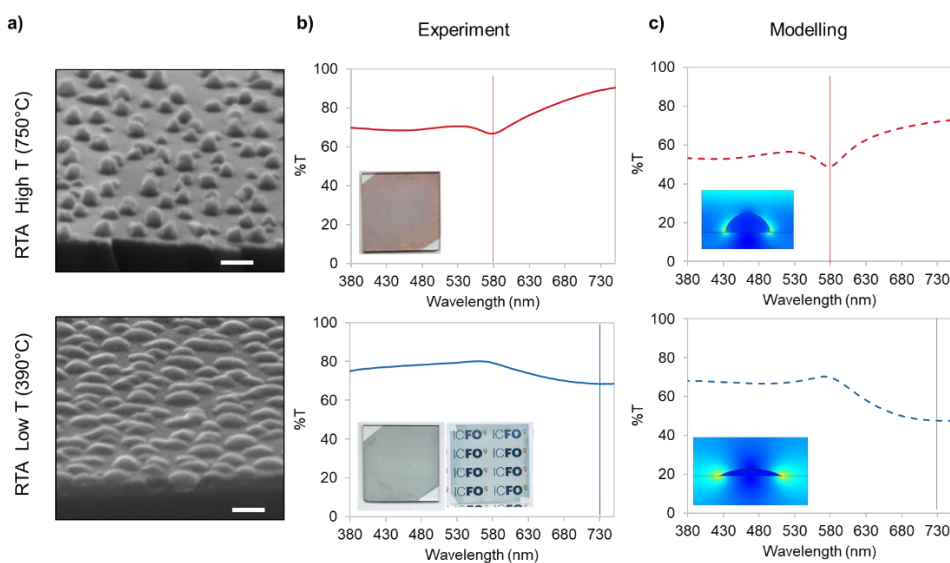


Figure 14 SEM images clearly illustrate the influence of the annealing temperature on the particle shape and size. High temperature produces separate, rounded particles with a contact angle $\approx 90^\circ$ whilst low temperature produces, flatter particles, with a contact angle $< 90^\circ$ and that are sometimes in contact. Scale bar = 100 nm. Optical spectra obtained from experiment (b) and modelling (c). Modelling reproduce qualitatively the experiments, in particular the red shift and broadening of the plasmonic resonance due to a reduction of particle's contact angle. Inset of b) shows the colour of the coatings against white background and also against a coloured text background to show transparency and colour neutrality of the dewetted CU UTMFs. The inset of c) shows the particle shape used for the modelling as determined from the SEM images in a.

3.3.3 Applications

The techniques developed in this section would enable the implementation of nanostructured metals onto transparent flexible substrates at low temperatures. Substrates of interest are thin cover glass, typically used for display screens, or plastic substrates for emerging flexible electronics applications. For example, by tuning the metal and additional dielectric thickness and additional function coatings, one can engineer the dimensions of the nanoparticles and the refractive index of the embedding material to create transparent antiglare, antireflection, self-cleaning coatings for display applications on substrates that cannot withstand high temperatures. Other applications can be in transparent sensors and solar cells where, for example, the use of metal nanostructures on the front and rear surfaces or in the bulk of a cell can be used to enhance their light collection efficiency through surface plasmon resonances [123,124]. Finally, an application that is elaborated in Chapter 5, is the use of dewetted Cu UTMFs for transparent antimicrobial coatings for touch-activated displays.

3.4 A transfer procedure for obtaining nanostructured and 2D materials on polymeric substrates

The field of flexible electronics stands to greatly benefit from advances in 2D materials, as the unmatched combination of device physics accessible on flexible polymeric or plastic substrates would enable long sought after large-area high-performance flexible devices. One of the main challenges facing plastic as a next-generation substrate is the substantially reduced processing temperature window. The maximum fabrication temperature is related to the glass transition temperature (strain point) above which plastic deformation takes place and the substrate no longer retains its original dimension. For example, polyethylene naphthalate (PEN) and polyethylene terephthalate (PET) satisfy the requirements for flexible substrates in that they are highly transparent, light, deformable, have low

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

roughness, are inexpensive and highly resistant to chemical/environmental corrosion. However, they can tolerate maximum temperatures of only 160 and 120 °C, respectively. Due to this limitation, high thermal processing materials are typically grown on SiO₂ or sapphire substrates, which can withstand high temperatures, after which they can be transferred onto a flexible substrate.

To this aim, a number of techniques have been developed to delaminate the 2D film from the growth substrate, each with varying degrees of cleanliness, uniformity and transfer related damage. In the following we briefly summarize; (i) etchant based, (ii) dry-transfer, (iii) water-assisted and (iv) salt-assisted techniques, in particular, the processes, advantages, and drawbacks of various transfer methods are discussed. A detailed summary is provided in [125]. Chemical-etchants e.g. hydrofluoric acid (HF), hydrochloric acid (HCl), or nitric acid (HNO₃) or strong bases such as NaOH or KOH, act by etching the substrate from underneath the 2D film, after which it can be transferred to the target substrate. Unfortunately, these etchants are non-environmentally friendly, highly corrosive and often damage or unintentionally dope the transferred film, ultimately leading to reduced device performance [126–130]. Dry-transfer techniques involve the use of adhesive supporting layers e.g. PDMS stamps, metals or other 2D materials to peel-off and separate the 2D material from its growth substrate [131–134]. These techniques unfortunately suffer from lack of control over contamination from the adhesion layer or stress induced film damage upon lift-off or transfer steps. Water-assisted transfer approaches rely on ultrasonication or capillary action to force water into the interface between 2D material and growth substrates [135–137]. This technique is prone to generate cracks and wrinkles in the transferred film [138–140]. Finally, water-soluble sacrificial layers such as NaCl [141–143], PTAS [144], and Na₂S/Na₂SO₄ [145,146] have been reported for the transfer of metals, metal nanostructures, graphene and TMDs. In this technique, the sacrificial material is deposited on the growth substrate prior to the target material. Whilst being etchant- and polymer support-layer-free, the sacrificial layers may not always be suitable for high-quality defect-free growth,

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

potentially causing undesired chemical or catalytic reactions which degrade the material quality. Previously, NaCl has been used as the growth substrate for the semiconducting materials [147], metal oxides [148], magnetic materials [149], metallic films [150,151], nanostructures [152] and graphene [153].

In this work, we develop a novel technique to obtain ultrathin and nanostructured materials requiring high temperature processing onto low strain-point (glass transition temperature) substrates. Our technique utilizes polished NaCl substrates, a well-known material that can stand the high temperatures involved during the growth – up to about 1000 °C - and can provide a fast and clean transfer onto the flexible target substrate due to the easy dissolution of the salt in water. We demonstrate two model systems including thermal dewetting of Au ultrathin metal films and growth of MoS₂ on NaCl at 750 and 650 °C, respectively, and subsequent transfer onto PET film substrates, after which the salt is easily dissolved by water.

3.4.1 Fabrication

NaCl substrates from International Crystal Laboratories with a size of 1 × 1 inches and of 5 mm thickness were used for the Au DNPs, meanwhile for MoS₂, the substrate was diced to 0.5 × 0.5 inches in order to fit the furnace dimension. PET films of 125 μm thickness from Goodfellow Inc. were used as the flexible target substrate. All substrates were sonicated in conventional organic solvents for 10 minutes and dried with a N₂ stream. As it can be observed in the AFM in Figure 15, NaCl substrates were purchased polished, which translates into a low roughness (RMS (root mean square) = 2.42 nm).

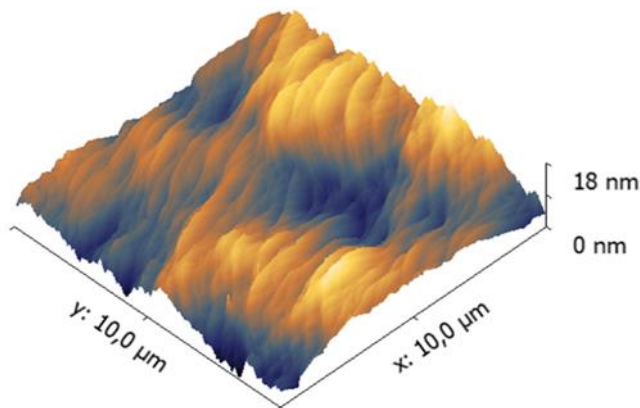


Figure 15 AFM of NaCl substrate after cleaning with organic solvents (acetone and isopropanol).

The substrates were treated in a way that minimises exposure to air as much as possible. If not kept under vacuum, the surface may become rough due to the reaction with humidity. A rougher surface will lead to poorer growth quality. This was avoided by keeping the NaCl in vacuum and properly evacuating the air from the CVD growth chamber.

Ag dewetted nanoparticles (Ag DNPs)

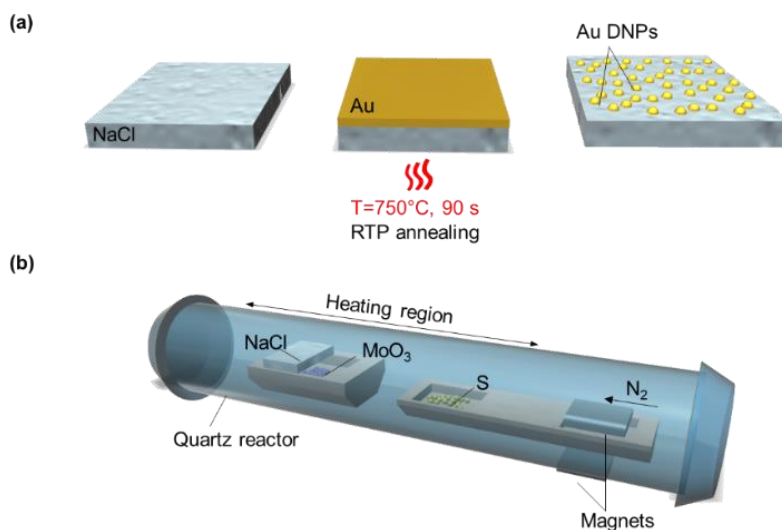
Gold (Au) thin films of 7 nm thickness were deposited onto NaCl substrates using a Lesker thermal evaporator with a deposition rate of 1 Å/s. The continuous films were subsequently dewetted by a rapid thermal annealing (RTP) (TSUNAMI™ RTP-600S) at 750 °C for 90 seconds. The temperature profile and gas flow rate are shown in [Figure 16c](#). A description of the dewetting procedure was explained in Chapter 2 and is elaborated in reference [62].

CVD growth of MoS₂

MoS₂ was grown as the main product from the reaction between powdered molybdenum trioxide (MoO₃) and sulphur (S) precursors by a chemical vapor deposition (CVD) process illustrated in [Figure 16b](#). The NaCl substrate was mounted facing down above a ceramic boat containing 6 milligrams of MoO₃ precursor (Sigma-Aldrich, 99.97% purity) and then loaded into the CVD furnace (MTI GSL-1100X-NT-LD). Another boat containing 300 milligrams of sulphur (Sigma Aldrich, 99.98% purity)

Chapter 3: Low temperature growth and processing techniques for MoS_2 and metal nanostructures

and a magnet was placed upstream, 18 centimetres from the boat of MoO_3 , in order to control the rate of sublimation. Once the substrates and precursors were mounted, a cycle of pumping until 0.1mbar and N_2 flow (10 ml/min) is repeated at least 3 times to remove oxygen from the reactor. The furnace was firstly heated to 300 °C with a rate of 20 °C/min after which the rate was reduced to 10 °C/min to prevent overshooting of the target temperature. Upon reaching a growth temperature of 650 °C, an external magnet was used to push the sulphur containing boat into the reaction zone where the temperature was held at 650 °C for 5 minutes. During the process, nitrogen (99.999% purity) was used as the carrier gas, with a flow rate of 50 ml/min. After 5 minutes, the furnace was left to cool down slowly. Atmospheric pressure was maintained throughout the experiment. The temperature profile and gas flow rate are shown in [Figure 16d](#).



Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

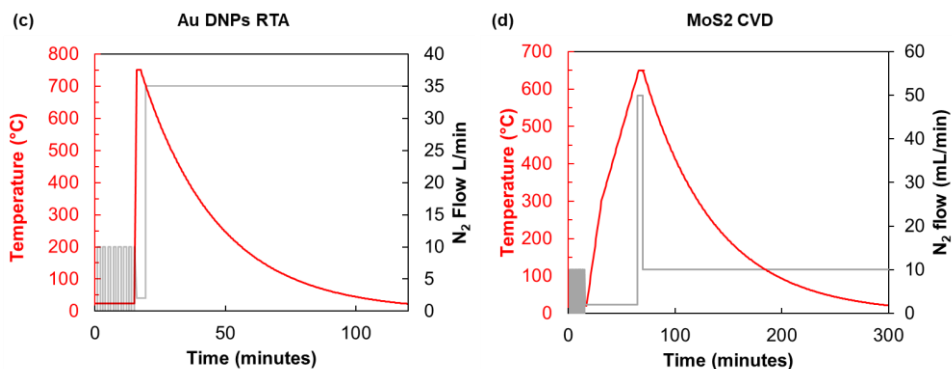


Figure 16 Fabrication of Au dewetted nano-particles (nano-caps) on NaCl by heating a sputtered Au layer of 7 nm thickness at 750 °C for 90 seconds. (b) CVD growth of MoS₂ on NaCl substrates due to the reaction of MoO₃ with S powder, with the latter being introduced at 650 °C using two magnets. Heating profile and N₂ flow rate for (c) Au DNPs and (d) MoS₂

3.4.2 Transfer of growth materials

A polymer assisted wet transfer method was used to transfer the MoS₂ film and the Au DNPs onto a flexible substrate, PET. Figure 17 illustrates the common transfer process using a PMMA as an intermediate layer. Firstly, a PMMA film was spin-coated at 4000 rpm for one minute onto the sample surface as a support to avoid the disaggregation of both growth materials, MoS₂ and Au DNPs respectively, during the transfer. The PMMA layer, with the adhered growth material, is afforded by water intercalation in between the growth material and substrate due to the high solubility of NaCl in water. The substrate is first located on the base of the beaker after which deionised water is slowly added. Once the water level reaches the top surface of the substrate, the release of the growth material occurs gently without inducing cracks or wrinkles. After that, the growth material remains floating on the water surface and it is then located onto the PET substrate. The high surface energy of the free standing MoS₂ or Au affords a strong interfacial Van der Waals adhesion between the transferred MoS₂ and the PET substrate, preventing the wash out or detachment of the transferred material during the subsequent PMMA removal process. The process was performed at room temperature and was complete within minutes for the samples of 1×1-inch size. After locating the growth material on top of the PET, the PMMA is removed by immersion in

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

acetone and isopropyl alcohol for 10 minutes each. In case of removing PMMA residues, cleaning could be improved by a low power oxygen plasma treatment.

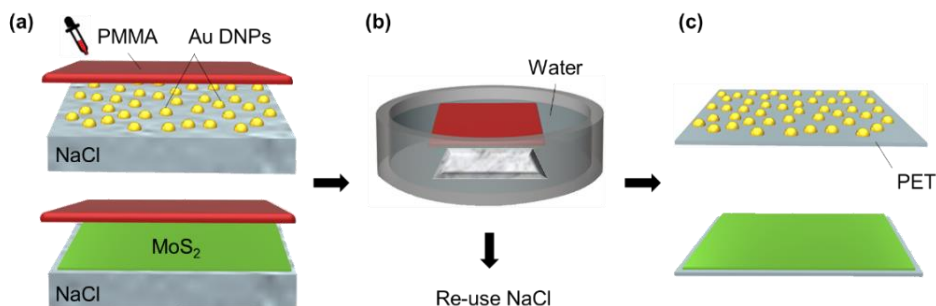


Figure 17 Transfer of Au DNPs and MoS₂ to PET using PMMA as an intermediate layer: (a) Spin-coating of PMMA at 4000 rpm for 1 minute; (b) Partial dissolution of NaCl substrate in water to afford the separation of the growth material covered with PMMA; (c) PMMA with Au DNPs and MoS₂ is located on top of the PET after which the PMMA is removed by immersion in acetone and isopropyl alcohol for 10 minutes each

Thus, our method guarantees easy, fast transfer and, given the 5 mm thickness of the NaCl substrate, there is the potential to re-use the growth substrate by performing a post-transfer surface conditioning procedure.

Figure 18 provides optical images and AFM pictures of the NaCl substrate as received after cleaning, immediately after MoS₂ transfer, and following a rapid thermal annealing surface conditioning treatment at 750 °C for 135 seconds, where it can be observed that the surface roughness is markedly improved to approaching that of the as received substrate.

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

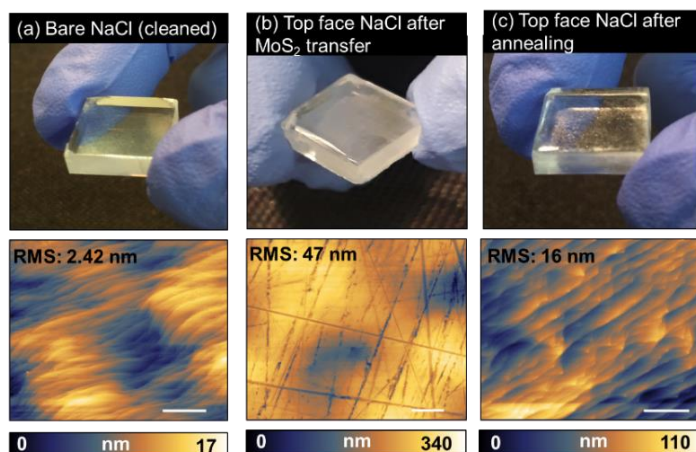


Figure 18 NaCl post-transfer conditioning Photographs (top) and AFM pictures (bottom) of (a) NaCl substrate sonicated in conventional organic solvents for 10 minutes and dried with a N₂ stream, (b) after MoS₂ removal and (c) after post-transfer rapid thermal annealing at 750°C for 135s. Scale bar: 5 μm.

3.4.3 Quality preservation of transferred nanostructured and 2D materials

For the transfer to be successful, the coverage, morphology, thickness and quality of the material should be well preserved. In this section, we provide the SEM, Raman and transmittance characterisations before and after the transference of Au DNPs and MoS₂ films.

SEM imaging was performed to evaluate the morphology and uniformity of the Au DNPs and MoS₂ films. Figure 19 shows a top view SEM of the Au DNPs and MoS₂ before, Figure 19a&d, and after, Figure 19b&e, the transfer onto PET. In both cases, the structure, coverage and morphology of the materials is preserved. In the case of Au DNPs, Figure 19a&b confirm that the transfer did not significantly affect their size or distribution. Moreover, Figure 19c provides an SEM comparison of Au DNPs on NaCl and fused silica where it is demonstrated that the morphology of the DNPs remains unchanged in each case, differing only in size due to the difference in interfacial energy between the Au and the substrate surfaces, respectively. Regarding MoS₂, the variation in domain

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

size and shape as a function of precursor ratio has been well documented in the literature [154–156] and can vary between hexagonal, triangular flakes and circular truncated and vertical stacks for more supersaturated conditions. In saturated conditions, as in our case where the Mo:S ratio is 1:50, the flakes have coalesced to form larger overlapping regions. This can be seen clearly in [Figure 19d&e](#), which show a continuous film with areas of overlapping domains.

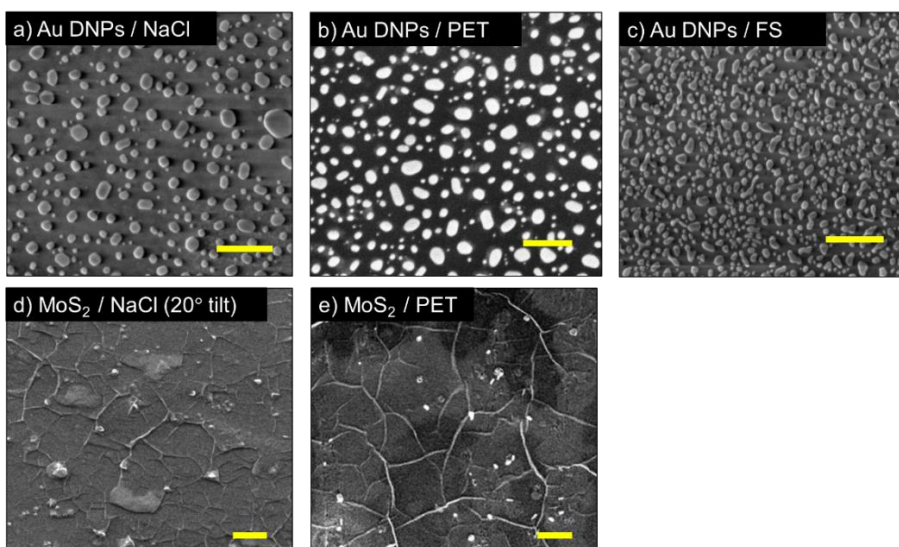


Figure 19 SEM images of (a,d) as-grown and (b,e) transferred Au DNPs and MoS₂ respectively. Scale bar: 2 μm . Note that the different contrast in the top images (a,b) is due to different substrate charging. Figure c provides a comparison to as grown Au-DNPs on a fused silica (fs) substrate.

Raman spectroscopy measurements were performed to identify the quality and layer structure of the as-grown MoS₂, as described in [Chapter 2, Section 2.3.1](#). Single point Raman spectra, [Figure 20a](#), displays the two signature peaks corresponding to the in-plane vibrations of the Mo and S atoms (E_{2g}^1) at $\sim 385\text{ cm}^{-1}$ and the out of plane vibration of the S atoms (A_{1g}) at $\sim 407\text{ cm}^{-1}$ [66]. Raman maps, shown in [Figure 20c-d](#), of $500\text{ }\mu\text{m} \times 500\text{ }\mu\text{m}$ were obtained. For both the MoS₂/NaCl and MoS₂/PET maps, a relatively uniform distribution and intensity were found with an average $E_{2g}^1 - A_{1g}$ peak distance of 22 cm^{-1} , therefore confirming that the MoS₂ film

Chapter 3: Low temperature growth and processing techniques for MoS₂ and metal nanostructures

was cleanly transferred with perfect preservation of the coverage, morphology, and thickness. The average peak separation of between 22 and 23 cm⁻¹ is indicative of 2–3 layers of MoS₂, in agreement with the SEM micrographs of [Figure 19d-e](#), which indicate several layer-overlapping domains.

Single-point photoluminescence spectra, see [Figure 20b](#), show the characteristic peak of A1 excitonic emission at 1.87 eV for both the pristine and transferred MoS₂ samples, again indicating a damage-free transfer with a good preservation of the sample. Note the absence of the B-exciton peak at 1.98 eV, whose absence has previously been associated with high quality samples [68].

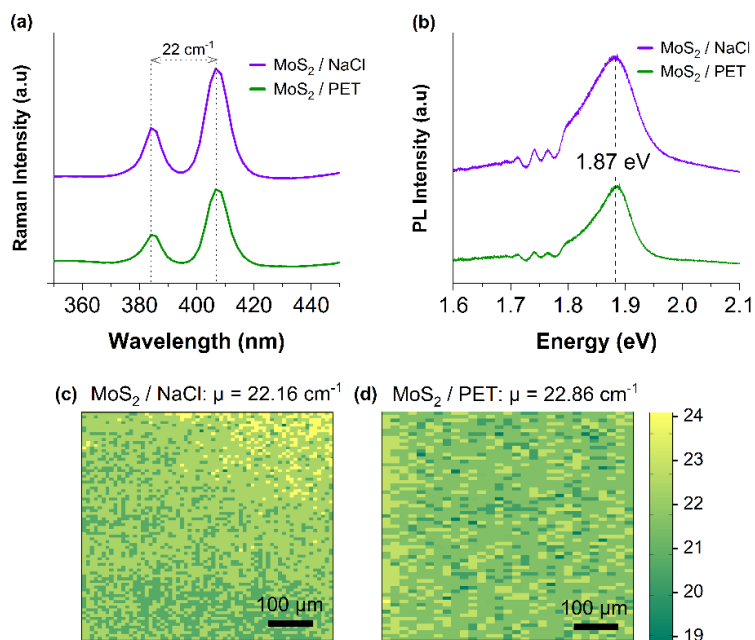


Figure 20 Single point (a) Raman and (b) photoluminescence spectra in the range 1.6 to 2.1 eV before and after transfer. Raman maps for MoS₂ on (c) NaCl and (d) PET. Scale bar: 100 μm.

The transmission of the films was measured in the range 400 – 2200 nm. The results are collected in [Figure 21a](#) and [Figure 21b](#) for Au DNPs and MoS₂, respectively. All graphs include the transmittance of the bare NaCl

(black line) and PET substrate (red line). Transmittance of the samples is preserved in both cases differing slightly due to the transmittance of the respective substrates. In the case of Au DNPs, see Figure 21a, a transmission dip at 600 nm wavelength is present due to surface plasmon resonances [47]. Note that the reduced transmission is compared to Au DNPs on NaCl, which correlates to the reduced transparency of NaCl in the region 500-600 nm. The insets of the Figure 21 show the aspect of Au DNPs and MoS₂, respectively, before and after transfer. The transferred films were completely removed from the growth substrate, leaving no visible PMMA residues and were deposited continuously, as confirmed by Raman mapping.

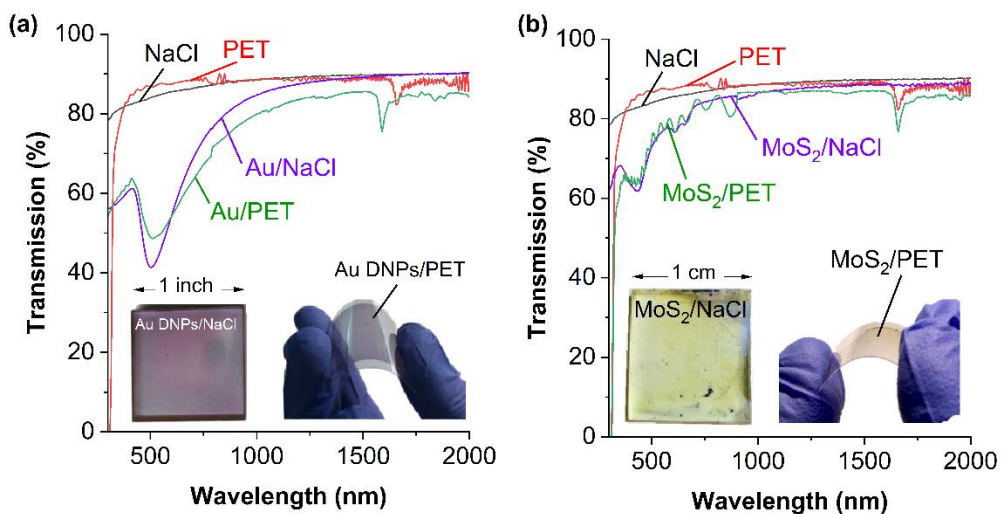


Figure 21 Transmission as a function of wavelength for (a) Au DNPs and (b) MoS₂ on NaCl and PET. Inset shows photographs of Au DNPs and MoS₂ on NaCl and PET substrate.

3.4.4 Applications

The clean transfer of large-area (centimeter scale) CVD-grown MoS₂ and dewetted Au nanoparticles onto arbitrary substrates, including flexible substrates such as PET demonstrates the versatility of the transfer method, allowing for the fabrication of flexible devices. The transfer method will be of interest to the research community working toward the

manufacturing of devices based on 2D materials for electronics, optoelectronics and flexible electronics.

3.5 Conclusions and outlook

The techniques presented in this chapter represent important innovations as they can be applied to different material combinations and are not limited by the underlying substrate. In such a way, we open up the possibility to obtain a host of functional, optical and biological surfaces on flexible substrates. Specifically, we demonstrate for the first time the growth of high thermal processing materials, Au DNPs and MoS₂, on NaCl substrates. Additionally, we show a new fast and easy way to transfer the growth materials to low strain point and flexible substrates, such as PET, whilst preserving the film quality. The technique is scalable, easily implemented and etching free. For the case of fabricating metallic nanostructures, increased scalability only requires a larger sacrificial substrate when compared to existing methods such as nano-lithography which is always limited to less than micron size dimensions. Similarly, up-scaling the growth of MoS₂ may be achieved with the use of a larger CVD chamber and consequent optimization of the reactive compounds.

In the future work, this technique could be readily extended to other ultrathin and 2D materials, such as graphene, or for the assembly of vertical hetero-structure systems, thereby offering extended functionality and performance for both fundamental studies and various existing and emerging applications.

The method could also be extended on other growth water-soluble crystalline substrates, such as ZnO. It is well known that, lattice constant matching between the 2D material and the growth substrate is very important for achieving high quality material growth; when the constants differ, strains are introduced into the layer, which leads to defected growth. Due to closer lattice matching of MoS₂ ($a=3.212\text{\AA}$) with ZnO ($a=3.2495\text{\AA}$) compared with NaCl ($a=5.6413\text{\AA}$), ZnO would promote higher quality growth of MoS₂, but since the cost of ZnO substrates is far greater, for this basic study we demonstrated the proof of principle using NaCl.

Chapter 4

Tuning electrical functionality of a transparent surface made of graphene

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4.1 Introduction

Engineering the doping level in graphene is essential to realizing functional electronic and optoelectronic devices. While achieving strong p-doping is relatively straightforward, electrostatic or chemical approaches to negatively dope graphene have yielded electron densities (n_s) of $-9.5 \times 10^{12} \text{ cm}^{-2}$ or below. This Chapter presents a method of achieving a very high n_s (-10^{13} to -10^{14} cm^{-2}) in graphene, on an ion-exchanged (IOX) glass substrate, which is widely used in touch screen displays (e.g. smart phones). Moreover, the proposed method, which is easy to implement and scalable, leads to relatively stable graphene doping, with about a 40% increase in sheet resistance over 5 months at ambient conditions. The results presented in this work could enable a route towards a host of previously inaccessible applications of graphene where the reduction of sheet resistance and strong and tunable n-doping is important, such as low work function transparent electrodes for energy

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

conversion and electron emission applications such as OLED, LEDs, solar cells and photonic devices operating in the NIR/VIS wavelength range.

Broadly speaking, graphene doping techniques can be classified in three categories: *i)* substitutional, *ii)* chemical and *iii)* electrostatic. Substitutional doping involves the replacement of one or more carbon atoms with atoms with a different number of valence electrons, e.g boron or nitrogen. It is typically achieved by introducing precursor gases containing boron (HBO_3 , H_2B) or nitrogen (NH_3) during the CVD synthesis of graphene [157,158]. Boron has one less valence electron than carbon and p-dopes graphene. Nitrogen, has one more valence electron than carbon, and so is used for n-doping. A drawback of this method is the difficulty in controlling the number of heteroatoms introduced into the graphene lattice, which can compromise the accuracy and repeatability of the doping level achievable by this method [159]. Additionally, the incorporation of heteroatoms can induce lattice strain effects and structural defects, which can eventually compromise the conductivity of graphene thus limiting its use in electronic devices [160]

Chemical doping techniques refer to the adsorption to the graphene surface of strong electron withdrawing or electron donating groups [161]. The technique relies on the charge transfer process taking place at the adsorbate/graphene interface. Some examples of chemical doping are the adsorption of HNO_3 (p-doping) [162], NO_2 (p-doping) [163], H_2O (p-doping) [163], ethanol (n-doping) [161] and NH_3 (n-doping) [164]. One drawback related to this method of doping is that it is difficult to control the surface coverage and reactivity of the chemical species adsorbed onto the graphene (e.g., HNO_3 and AuCl_3). This can lead to difficulty in controlling the doping level and instability of the doping over time [165].

Electrostatic doping is a technique in which the graphene doping level is modulated by application of a gate voltage where the polarity and value of the gate voltage determines the type and strength of doping. This technique allows for a degree of reversible and accurate control of the doping. This is typically performed in back or top gated device configurations depending on the nature of the substrate. One drawback

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

is the relatively low reachable n_s - maximum 10^{13} cm^{-2} due to the limited capacitance of the available solid-state thin film or electrolyte capacitors (e.g. 300 nm-thick SiO_2 grown on Si). The capacitance can be increased by reducing the thickness of the SiO_2 dielectric [166]. However, SiO_2 is prone to dielectric breakdown at gate voltages required for achieving high doping. In this respect, the use of thinner or higher dielectric constant materials (e.g. MoS_2 , h-BN), oxides (e.g. HfO_2 , ZrO_2 , Al_2O_3), ionic liquids or polymers have been considered for achieving high doping [167–169]. However, there remains challenges to reduce the influence of the target substrate or dielectric on the doping of graphene.

Moreover, while achieving strong p-doping is relatively straightforward, accessing high and stable n-type doping in graphene is challenging on two fronts. The first is that it is difficult to prevent graphene from process related p-doping that can arise from its reaction with chemical resists, metal etchants and polymer residues [170–172]. The second concerns the stability of n-type doping as graphene reacts with moisture and oxygen in the atmosphere causing it to become p-doped. Despite these challenges, significant efforts are being made towards engineering high levels of n-type doping in graphene as it would provide a route towards a host of previously inaccessible applications, including photonic devices operating in the NIR/VIS wavelength range, low work function transparent electrodes for energy conversion and electron emission applications such as Organic Light Emitting Diodes (OLEDs) [173–175], Light Emitting Diodes (LEDs) [97], solar cells [105,106,164] and touchscreens [100].

Electrostatic and chemical doping techniques have so far yielded electron densities (n_s) of $-9.5 \times 10^{12} \text{ cm}^{-2}$ or below. In light of this limitation, several works have demonstrated graphene doping after its transfer onto appropriately treated substrates. For example, the deposition of ammonia or aluminium on the surface onto SiO_2 substrates led to formation of positive (NSiO^+) and negative (AlSiO^-) surface charge layers on the substrate which were shown to induce the electrostatic n- and p-doping of graphene, with n_s of -8.62×10^{12} and $2.17 \times 10^{12} \text{ cm}^{-2}$, respectively [176].

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

More recently, n-doping of graphene has been demonstrated on multicomponent glass where the ions are exploited to n-dope graphene to a level sufficient to reverse environmental and process related p-doping [177]. Similarly, sodalime glass (SLG) has been used to obtain highly n-doped graphene, in the order of $-1.33 \times 10^{13} \text{ cm}^{-2}$, where it was proposed that the high surface density of Na in SLG dopes the graphene via electron transfer [178].

This Chapter describes, for the first time, a method to obtain highly n-doped graphene with carrier densities (n_s) in the order of -10^{13} to -10^{14} cm^{-2} by transferring graphene (e.g., pristine graphene) onto ion-exchanged (IOX) CORNING® GORILLA® GLASS substrates, widely used in touch screen displays (e.g. smart phones). This glass contains potassium ions (K^+) from an ion exchange process in which some of the sodium ions (Na^+) at the glass surface are replaced by K^+ . The depth of the exchange layer (referred herein as 'IOX thickness') can be modified from 5 to 50 μm .

4.2 Fabrication of devices

Two types of devices were fabricated on IOX Corning® Gorilla® glass, fused silica (FS) and Si/SiO₂ substrates for electrical measurements. Van-der-Pauw devices, shown in [Figure 22](#) (left), features four identical devices (D1 - D4) with the typical cloverleaf geometry for performing sheet resistance measurements. Hall bar devices, shown in [Figure 22](#) (right), features two identical devices (D1 and D2) with Hall bar geometry for performing transport measurements. To allow for statistical descriptions, multiple samples of each design were fabricated. Both devices follow the same fabrication procedure outlined in the following, with the addition of Al₂O₃ device encapsulation for the Hall bar structures.

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

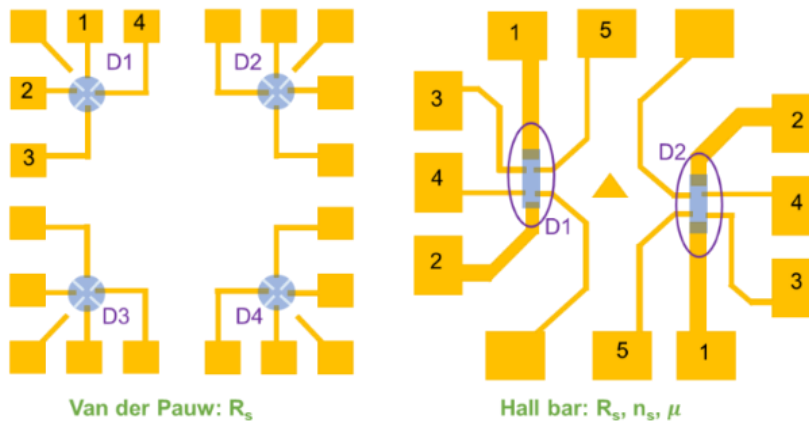


Figure 22 Device designs fabricated in this work. In design A the graphene cloverleaf has a diameter of 300 μm . In design B, the Hall bar has dimensions 140 x 300 μm .

All experiments have been carried out with graphene grown by chemical vapor deposition (CVD) purchased from Graphenea. The graphene sheets were transferred using a wet-transfer technique [179] onto FS, Si/SiO₂ or IOX Corning® Gorilla® glass substrates. Prior to graphene transfer, the substrates were cut to a size of 1 cm² and cleaned in an ultrasonic bath using acetone and isopropyl alcohol for 5 minutes in each solvent. Then, Ti/Au (3/50 nm) contacts were fabricated with Van-der-Pauw or Hall bar geometry by photolithography and lift-off processes. CVD graphene was transferred to the metallized substrates which were subsequently dried under atmospheric conditions for 12 h and later immersed in a bath of acetone to remove the PMMA residues. A photolithography process and subsequent Argon/Oxygen etching step was performed to reduce the area of the graphene to a 300 μm diameter cloverleaf in Van-der-Pauw devices and a 140 x 300 μm rectangle in the Hall bar devices, respectively. Remaining photoresist was removed by immersing the samples in acetone for 2 minutes. Finally, the Hall bar devices were encapsulated with 40 nm Al₂O₃ by atomic layer deposition and a final photolithography and subsequent etching process were performed to remove the excess Al₂O₃. The etching was performed by dipping the samples in a buffered HF oxide etchant solution (BOE, HF: NH₄F, 1:7) for 1 minute.

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

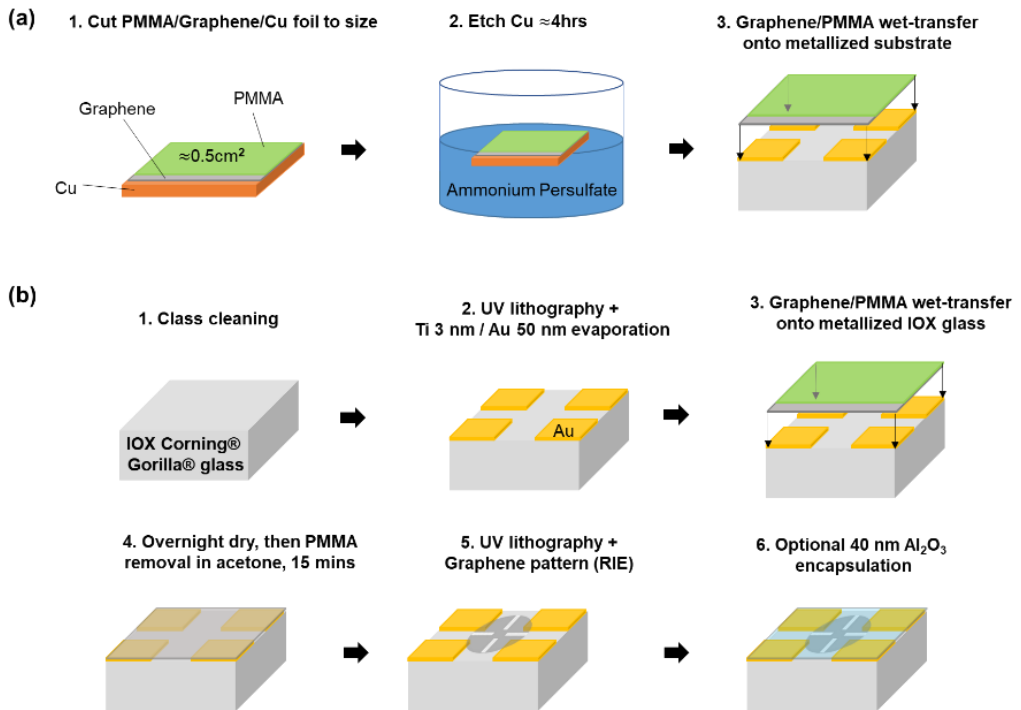


Figure 23 Procedure for the graphene device fabrication: (a) Wet graphene transfer (1) Cut PMMA/Gr/Cu foil to approx. 0.5cm^2 in size. (2) The foil is floated on top of ammonium persulfate for approximately 4 hours to etch the Cu from underneath the graphene. (3) The resulting PMMA/Gr stack is wet transferred onto a metallized substrate; (b) (1) Initial cleaning of substrates is by organic solvents acetone and isopropanol. (2) UV lithography and evaporation of the metal contacts (Ti 3 nm / Au 50 nm) (3) Graphene transfer onto metallized substrates by wet etching process. (4) Samples are left overnight to dry after which PMMA is removed by immersion in acetone for 15 minutes. (5) A second lithography step is performed to reduce the graphene contacts area, removing the excess by reactive ion etching (RIE). (6) Hall bar devices were encapsulated with 40 nm Al₂O₃ by ALD deposition. A final lithography step is performed to remove the Al₂O₃ from the top of the Au contacts by dipping the samples into a BOE solution.

4.3 Characterisation of devices

4.3.1 Electrical characterisation

The electrical measurements have been previously explained in [Section 2.3.2](#). Figure 24 shows a sketch of the graphene transferred onto IOX Corning® Gorilla® glass (a) and fused silica (FS) glass (b) where blue shaded area comprises the silica matrix.

Sheet resistance measurements

The four-point R_s of all Van-der-Pauw devices (comprising 16 on IOX and 16 on FS) was measured. For each device, the I-V curve was measured several times to ensure repeatability, sampling at 1 mV steps, which were subsequently averaged. A linear fit was applied to the I-V curves collected for all devices on each substrate, from which the average R_s was obtained.

[Figure 24c](#) compares the I-V characteristics for Van-der-Pauw devices prepared on IOX_{20µm} Corning® Gorilla® glass and FS substrates, where the difference in slope confirms the strong influence of the supporting substrate on the sheet resistance of graphene. The corresponding average R_s (obtained from the slope of the linear fit of the I-V curve) of the graphene/FS devices was 1.22 ± 0.353 kΩ/sq. which is similar to those values previously reported [180], thus confirming the reliability of our transfer technique and characterization method. On the other hand, the R_s for the graphene/IOX_{20µm} devices was consistently 3-5 times lower with an average of 0.245 ± 0.069 kΩ/sq. The results were quite repeatable across all devices fabricated by independent runs. The low R_s is in and of itself of great interest, as it supports the use of graphene on IOX substrates as a transparent conductor [181] and other applications requiring low R_s such as low work function electrodes [182].

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

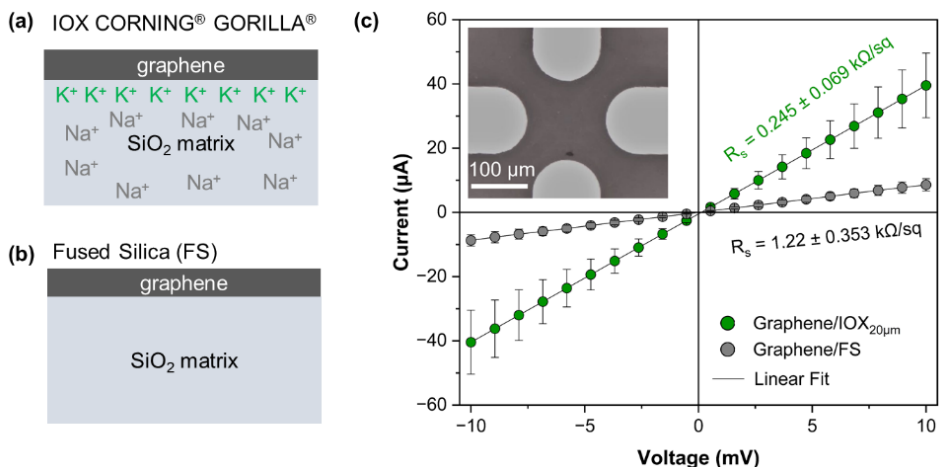


Figure 24 Sketch of graphene transferred onto IOX Corning® Gorilla® glass (a) and fused silica (FS) glass (b) where blue shaded area comprises the silica matrix. The top surface of the IOX Corning® Gorilla® glass contains potassium (K⁺) from an ion-exchange procedure, where the depth of layer can be modified from 1 to 50 µm; (c) I-V characteristics measured for graphene on IOX20 µm Corning® Gorilla® glass (green circles) and FS (black circles) substrates. For each device, the I-V curve was measured several times to ensure repeatability, sampling at 1 mV steps, which are subsequently averaged. A linear fit was applied to the I-V curves collected for all devices on each substrate (totalling 16 IOX and 16 FS devices), with error bars representing the spread in the data. Note that the error bar for graphene/FS is not visible because of the low standard deviation. The average R_s was obtained from the slope. The inset of the graph shows an optical microscope image of a real sample. Scale bar 100 µm.

R_s measurements were also performed on graphene transferred onto bare (i.e. with no pre-defined Au contacts) substrates. For this experiment, graphene was wet transferred onto bare 1x1cm² IOX Corning® Gorilla® Glass or fused silica (FS) substrates as described in the fabrication methods, Section 4.2. The sheet resistance of the graphene (R_s) was measured with a four-probe point probe in colinear configuration, as described in Section 2.3.2. Four samples on IOX Corning® Gorilla® Glass and four samples on FS were prepared. Several measurements were taken per sample to ensure repeatability. The value of R_s reported in Table 2 is the average for all samples of each substrate.

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

Table 2 R_s of graphene measured by in using the 4-point probe method in co-linear orientation.

	R_s k Ω /sq.	Standard deviation
IOX 20 μ m	1.32	0.7
FS	1.39	0.4

Interestingly, and in contrast to Au-contacted graphene devices (Figure 24c), no difference in R_s was found, irrespective of the underlying substrate with both IOX and FS systems measuring between 1-2k Ω /sq., Table 2. This result was repeated several times by independent fabrication processes.

Hall measurements

Eight samples on IOX_{1-43 μ m} were fabricated with a Hall bar design, Figure 11b, where each sample contains two identical devices (D1 and D2) for gathering statistics. The Hall measurement was previously explained in Section 2.3.2 Figure 25a-b show the measurement scheme and the evolution of Hall voltage (V_{Hall}) as a function of perpendicular magnetic field sweep (B) between -5 and 5 Tesla at 300 K.

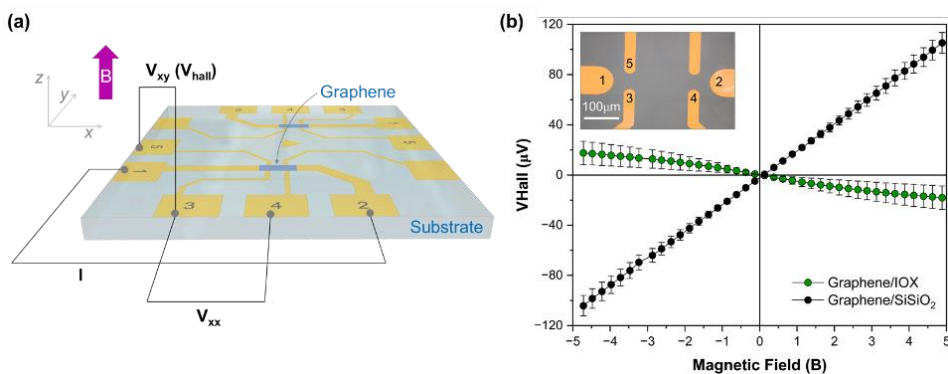


Figure 25 Simplified three-dimensional views of the Hall bar structures, along with circuits for the Hall effect measurement. The heavy purple arrow indicates the direction of the magnetic field corresponding to the circuit diagrams shown. A constant DC current of 1 μ A was injected through the sample via probes “1-2” whilst probes “3-4” or “3-5” were used to measure the R_s or V_{Hall} , respectively during a perpendicular magnetic field sweep (-5 T to 5

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

T) at 300 K. (b) V_{Hall} vs. magnetic field (B) data obtained from 16 graphene/IOX_{1-43 μm} devices (green circles) and 2 graphene/Si/SiO₂ devices (black circles) where the dotted line represents a linear fitting of all devices. *Note that the IOX data does not distinguish IOX layer thickness because the n_s was not influenced by the depth of exchange and, by deduction, the V_{Hall} was found to be independent of the IOX thickness. The inset of the graph shows an optical microscope image of a real sample. Scale bar 100 μm .

A negative slope indicates n-type doping (excess of electrons), while a positive slope indicates p-type doping (excess of holes) where the magnitude of the gradient correlates to the strength of the doping. Comparing the slope of the devices fabricated on IOX_{1-43 μm} to that of the Si/SiO₂ reference, it is found that V_{Hall} induced by the charge carriers in the graphene on IOX substrates is lower in amplitude and of opposite sign, for a fixed current and magnetic field.

Figure 26a-c shows the evolution of R_s , μ_H and n_s respectively, for the eight graphene/IOX samples, comprising of IOX thicknesses: 1x1 μm , 1x5 μm , 2x10 μm , 2x20 μm and 2x43 μm . Each marker and corresponding error bar represent the average and standard deviation of D1 and D2. Identical measurements on the Si/SiO₂ reference sample are indicated with blue markers. Note that the low R_s (and high n_s) is reproduced with a comparable magnitude irrespective of the IOX thickness.

The sheet resistance measurements shown in Figure 26a show an average R_s value of 0.318 ± 0.078 k Ω /sq. for the graphene/IOX_{1-43 μm} devices. This is in close agreement with the R_s statistics obtained with the Van-der-Pauw structures (0.245 ± 0.069 k Ω /sq.) and confirms that the effect of the underlying substrate is significant and independent of the slight processing differences between the two designs e.g. encapsulation with Al₂O₃. Furthermore, the R_s for the Si/SiO₂ reference, 2.32 ± 0.690 k Ω /sq., is of the same order of that for graphene/FS devices fabricated with Van-der-Pauw geometry (1.22 ± 0.353 k Ω /sq.).

The room temperature (RT) carrier mobility (μ) measurements, in Figure 26b, show a mobility between 80 – 800 and 150-160 cm²/V·S for graphene on IOX and Si/SiO₂ substrates, respectively. Graphene wet-transferred onto Si/SiO₂ substrates typically produces mobility values in the range of 10^2 - 10^3 cm²/V·s at 300 K for a carrier concentration, $n_s \sim 10^{12}$ cm⁻²

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

[180,183,184]. In the future, we will perform studies and evaluate previous techniques to reduce the spread of the mobility we have observed toward the highest values observed in the literature for glass [185–187].

The carrier density measurements (n_s) shown in Figure 26c show a moderate p-doping (average $n_s +3.9 \times 10^{13} \text{ cm}^{-2} \pm 1.3 \times 10^{13} \text{ cm}^{-2}$) for the graphene/Si/SiO₂ devices (blue marker). The doping may depend on processing conditions and is consistent with data previously reported in graphene–silica systems [171,188–193]. In contrast, the graphene/IOX_{1-43μm} devices, indicated with red markers, show a strong n-doping within range -1.7×10^{14} to $-4.5 \times 10^{14} \text{ cm}^{-2}$, with an average of $-1.9 \times 10^{14} \pm -9.8 \times 10^{13} \text{ cm}^{-2}$ which validates the effect of the IOX layer on the graphene doping. From the average n_s value, the Fermi level (E_F) was calculated to be $-1.61 \pm 0.4 \text{ eV}$ for the graphene/IOX_{1-43μm} devices.

The observed high n_s might be related to a local surface density of positive charge present in the IOX glass layer in which the graphene is in direct contact. A positive surface charge might originate from the excess of K⁺ after the ion-exchange process [194,195]. When the graphene is contacted, electrons are drawn into graphene to neutralize the excess surface charge due to IOX process. Similar examples have been reported in literature where it is demonstrated that a charged substrate surface induces the doping of graphene [176,196]. Although it is clear that the IOX glass is a key element to achieve doping, additional experiments are needed to confirm the doping mechanism and the interplay between the processing steps to make the devices and the substrate composition [170–172,197].

To evaluate the stability of the doping, the R_s of several IOX and Si/SiO₂ devices was measured again after being kept for five months in a dry box. The IOX devices (purple markers in Figure 26a) reveal an increase between 0.100 to 0.160 kΩ/sq. corresponding to a 42 % average increase as compared to the initial R_s . The Si/SiO₂ devices reveal a similar increase of $\sim 0.100 \pm 0.8 \text{ k}\Omega/\text{sq}$, corresponding to a 5% average increase compared to the initial R_s . Given that the increase in R_s after 5 months is of a similar

Chapter 4: Tuning electrical functionality of a transparent surface made of graphene

magnitude for both IOX and Si/SiO₂ devices, we understand that the 42% increase for the IOX is only large in the context that the initial starting R_s was low. We believe that the increase in R_s after 5 months is probably not due to the IOX substrate, but more likely related with a combination of atmospheric exposure, which is known to degrade the graphene, and degradation induced by the Al₂O₃ encapsulation layer. In this regard, future work should consider alternative encapsulation techniques that maintain an effective moisture barrier and therefore the initial quality of the transferred graphene over time.

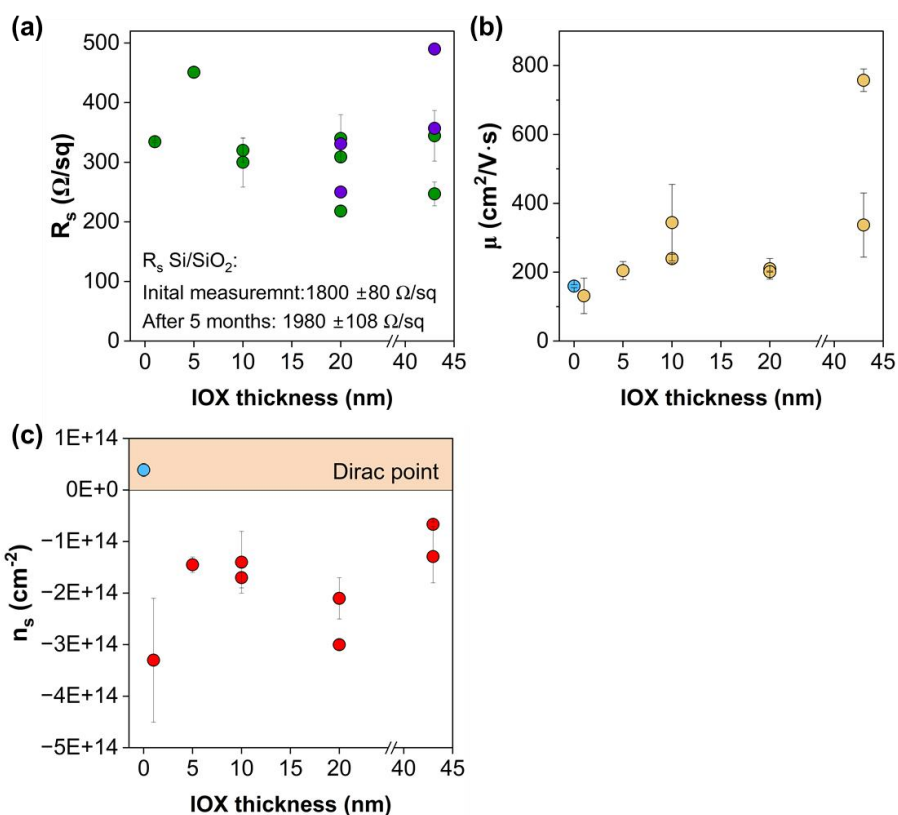


Figure 26 The evolution of (a) R_s (b) μ_H and (c) n_s with IOX layer thickness. Each marker and error bars represent the average and standard deviation of D1 and D2. Samples included in the statistics are $1 \times 1 \mu\text{m}$, $1 \times 5 \mu\text{m}$, $2 \times 10 \mu\text{m}$, $2 \times 20 \mu\text{m}$ and $2 \times 43 \mu\text{m}$. In graph (a) purple markers represent the R_s for the IOX devices remeasured after 5 months. The corresponding values for the Si/SiO₂ reference sample is provided in the inset of graph a. The values of μ_H and n_s for the Si/SiO₂ reference samples are indicated with blue markers in graphs b and c. In some cases, the error bars were smaller than the markers and are not visible.

4.4 Applications and future work

The results presented in this Chapter could enable a route towards a host of previously inaccessible applications of graphene where the combination of low sheet resistance, strong n-doping and high E_F , obtained on a transparent glass substrate, are important. For example, one application could be low work function transparent electrodes for energy conversion and electron emission applications such as OLED, LEDs, and solar cells. Secondly, the demonstrated high n_s , corresponding to E_F of -1.61 eV, could be interesting for plasmonic applications, which for graphene devices has so far been limited to mid-infrared and longer wavelengths [198–201]. As frequency of plasmonic excitation scales according to $\sqrt{E_F}$, the graphene/IOX system could be subsequently nanostructured into, for example, nanodisk or nanoribbon geometries, for making plasmonic devices operating in the near-infrared region.

4.5 Conclusions and outlook

As described herein, IOX Corning® Gorilla® glass was found to naturally modify graphene doping without the need of additional post-treatment (e.g. thermal poling under applied potential). Sheet resistance and Hall measurements performed at room temperature demonstrate high and reproducible doping levels of graphene placed in direct contact with IOX glass leading to graphene with an unexpectedly high n_s (-10^{13} cm⁻² or higher). The negative values obtained with IOX glass were found to be 1-2 orders of magnitude larger than the positive values on undoped silica glass substrate.

Chapter 5

Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

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This chapter presents an application of the low temperature metal dewetting process introduced in Chapter 3. The work described in this chapter and partly in Chapter 3 was performed with other members of the Optoelectronics group, in particular Alessia Mezzadrelli, and also in collaboration with Corning Incorporated. I fabricated the majority of the samples and I contributed to the design, optical measurements, data analysis and paper writing.

Shared touchscreen environments are becoming ever prevalent in our advancing society, facilitating the way we buy tickets, order food, and provide feedback to name a few examples. However, their frequent use by hundreds of people in a short space of time, provides the perfect environment for harbouring harmful germs and bacteria. Moreover, in these applications, where repeated spray-based sanitisation methods are impractical, the need for transparent surfaces to inherently be antimicrobial has become important. This chapter implements the low temperature fabrication of metallic nanostructures described in Chapter 3 to obtain transparent coatings with antimicrobial (AM) functionality that

are also durable and long lasting. The coatings are easy to clean, maintain their AM functionality, optical and wetting properties over a long period of time, whilst also being fabricated in a way that is industrially scalable. We anticipate this innovative method of imparting AM function into transparent surfaces will be useful in many applications of technological interest such as touch-enabled public displays. This work has resulted in the filing of a Patent application in 2023 entitled “*Antimicrobial surface with high transparency and durability using discontinuous metal islands*”.

5.1 Introduction

The COVID19 pandemic highlighted the potential of surfaces to harbour harmful microorganisms by contamination with infectious droplets from sneezing, coughing, speaking and breathing. Now more than ever, the importance of effective disinfection practices for surfaces with constant and repeated use has become a priority. In the first instance, surface contamination is combatted by spraying the surface with an alcohol-based disinfectant, soap or antimicrobial wipes. While effective in the short-term, these procedures are impractical for multi-user surfaces and require continuous re-application to clear any microbes present on the surface. Furthermore, the chemicals in sanitisers are damaging to water streams, detrimental to indoor air quality and are often packaged in non-recyclable bottles that end up in landfills. Accordingly, a need exists for functional surfaces that are persistently antimicrobial, resistant to general use wear-and-tear and sufficiently transparent to retain their functionality. Transparency typically includes high light transmission combined with low scattering (haze). In the following we provide a brief overview regarding the current status of transparent AM surfaces with particular attention to technologies developed for touch screen application.

5.2 State of the art AM Solutions for display and touchscreen applications

The strategies that have been developed to impart AM functionality into transparent surfaces can be broadly divided into 4 categories, outlined in Figure 27, where green text indicates most popular commercially available products. The following provides a brief overview of each method. Table 3 presents a non-exhaustive list of commercial AM screen protection technologies for mobile devices, laptops, tablets and kiosks.

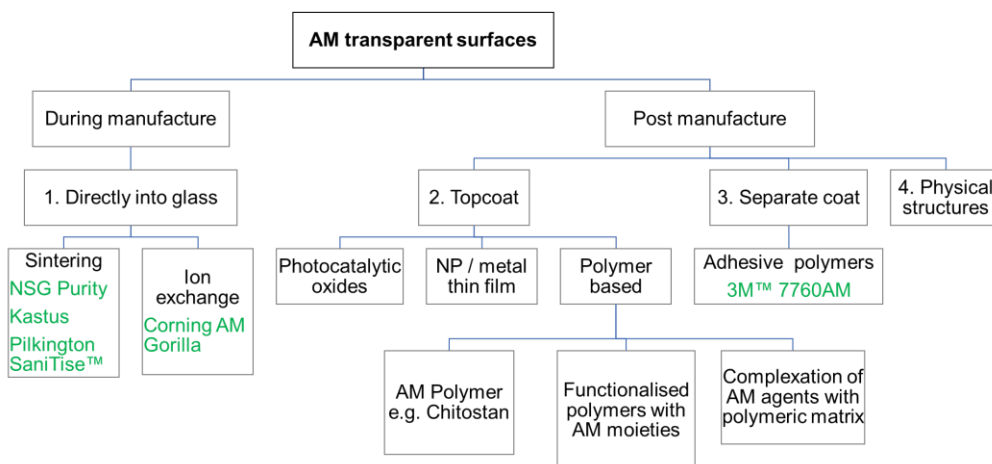


Figure 27 Strategies to impart AM function into transparent surfaces. Green text indicated commercial products referenced in Table 3.

5.2.1 Sintering and Ion-exchange processes

These methods require infusing various AM agents, typically silver (Ag) or copper (Cu) in the form of nanoparticles (NPs) or photocatalytic metal oxides films, e.g. titanium dioxide (TiO₂) or zinc oxide (ZnO), directly into the glass surface during manufacture. This can be achieved by either sintering or ion-exchange processes. The process of sintering involves the application of the AM agent onto the glass surface through either spray or dip coating. The coating is then annealed to temperatures in excess of 600

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

°C. The high temperature facilitates the creation of a durable, permanent hard coat in the top layer of the glass [202,203]. Conversely in ion-exchange processes, the AM agent integration is achieved through a chemical infusion process. The glass is heated inside a bath containing Ag/Cu salts. Diffusion gradients drive the exchange of $\text{Cu}^{2+}/\text{Ag}^{+}$ ions into the glass surface with the simultaneous out-diffusion of Na^{+} ions. Thus, an AM layer comprising a few microns deep is formed in the surface of the glass [204,205].

Both sintering and ion exchange produce highly durable coatings, which may be over-coated with functional layers for example, anti-fingerprint (AF) coatings. Sintered coatings have witnessed huge success in the market place with current world leader Kastus, employing this method for its AM display glass [206]. Pilkington and NSG have also developed silver ion-containing sintered AM coatings. Meanwhile Ion-exchange is the technology behind world leading 'Antimicrobial Corning® Gorilla® Glass', that is widely used as a cover glass for display applications.

Despite their success and easy implementation with existing glass manufacturing infrastructure, both strategies come with several limitations. Firstly, the use of silver as a raw material introduces significant cost considerations. Secondly, the high processing temperatures required for fabrication, precludes the use of these techniques for emerging flexible display modules. In this regard, alternative strategies (2-4 in [Figure 27](#)) have been developed for post-glass manufacture.

5.2.2 Coating methods

In a second approach the AM agent may be contained within a coating that is fabricated on top of the glass substrate. The use of polymers has received great interest as they are a low-cost option, that can be easily prepared and functionalized, by solution processes without the need of high temperature or vacuum deposition methods [207]. Polymer-based coatings can be further subdivided into; (a) application of polymers that have an intrinsic AM function e.g. Chitosan (b) incorporation/complexation of the charged AM agent (metallic ions, metals, metal oxides, nanoparticles) into the polymer matrix [208–210],

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

or in a nanocomposite with SiO₂ [211–215] and (c) functionalization of the polymer with AM agents e.g. quaternary ammonium compounds (QACs) [216].

By loading or embedding AM agents into supporting polymers, the release of Cu ions can be controlled. The intentional prolongation of ion release confers sustained AM functionality, maintaining the coatings efficacy over an extended period. However, despite their popularity and recent success in the marketplace [217,218], polymer coatings are often not practical under conditions where chemical durability is desired. Moreover, the inherent durability of the polymer is less than that of the underlying glass, potentially limiting the overall product's lifespan.

5.2.3 Separate coating

In this method a plastic/glass protective cover containing an AM agent is separately fabricated and then adhered to the display glass module. This method is particularly popular for disposable coatings for example mobile or tablet protector films.

5.2.4 Physical structures

Physical structures are fabricated in top coat or directly into the glass. In contrast to approaches 1-3 which release active AM agents, this approach relies on surface nanostructures that are biocidal by combination of mechanisms including anti-adhesion properties that prevent bacterial attachment and nanometre sized structures that are capable of perforating bacterial cell membranes [219,220].

Table 3 Commercially available transparent AM coatings indicating fabrication method, coating properties.

Company Coating name	Coating AM agent	Fabrication	Properties	Comments	Ref.
NBD technologies InvisiPrint® MBED	Silane based thin film coating	Spray/dip/wipe	Oleophilic Hydrophobic ETC 93% transparent	ISO 22196 results Not EPA registered.	[221]
Kastus (Irish) Antimicrobial film	Cu / Ti based coating nanoparticle	Sintering T>600°C	>95% transparent	Market leader in screen protectors	[206]

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

NSG Purity	Photo-catalytically activated TiO ₂	Sputtering T>600°C			
Corning (US) Antimicrobial Corning® Gorilla® glass	Ag ions ion infused into glass surface	Ion-exchange T>600°C	EPA registered	EPA registered	[222]
Pilkington (UK) SaniTise™	Pilkington SaniTise™ TiO ₂ thin film	Pyrolytic hard coat T>600°C	90.5% transparent	Photocatalytic effect UV activated	[223]
3M™ Durable Protective Film 7760AM	Aftermarket PET adhesive film with an Ag ion containing hard-coat layer	Low T	Transparent	12-month shelf life due to humidity sensitivity EPA registered	[218]

Table 4 A comparison of the present study with previous works directed towards creating transparent Antimicrobial (AM) or antiviral (AV) coatings

Coating	Agent	Fabrication method	AM efficacy	AV efficacy	%T	Ref.
This work; SiO ₂ embedded Cu DNPs coatings on glass	Cu ions	Sputtering and dewetting	Up to 99.99%	Not reported	70-85	
PVA/ZnO PVA/Ag PVA/ZnO & Ag Disposable protective coatings	Ag/Zn ion	Spin coating a mixture PVA/AgNO ₃ PVA/zinc acetate 80 °C		Not reported	75	[224]
PVF/AQCS/SiO ₂ NP/Cu ions PVF/AQCS/SiO ₂ NP/AQCS/Cu ions	ACQS / Cu ion supported on SiO ₂ NP	layer-by-layer (LbL) assembly of bactericidal polymers	99-100%			[213]
PDA/Cu PDA/Cu ₂ O NP on glass	Cu ion/ Cu NP Supported on EDTA	Solution processes AQCS & EDTA covalently grafted to PVD for complexation with Cu ions	96% S. aureus 99.8% P. Aeruginosa		73-75	[208]
PDA/Cu ₂ O	Cu ion	Spray coated (electroplateless deposition) <100°C	99.99% P. Aeruginosa	99.98 SARS-CoV-2	40-80	[209]
SiO ₂ / Cu SiO ₂ / Ag On borosilicate	Ag/Cu ion	<100°C	>99.99% P. Aeruginosa 99.18% S. aureus	99.98% SARS-CoV-2	71-75	[225]

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

Polymeric salts PSS-Bz-Ag and PSS-Bz bound to PSS		FA-CVD 150 °C	99.8% S. aureus		88-91	[211] [226]
Cu ₂ O-Zeolite/Polyurethane film	Cu ions	Polymeric salts 50 °C	SARS-CoV-2			[210]
(PVA)-based Cu NP-graphene coating	Cu NP/Cu ion	Flow coating on PET and PVC	99.99% E. coli 99.99% S. aureus	99.94% for SARS-CoV-2		[227]
Cu NP/ Ag NP on nanostructured PET/PE films	QAC	Dip coating on tempered glass	Not reported	Influenza A/H1N1/WSN/1933 virus	>85	[228]
Conical nanopillars with Ag / Cu NPs	Ag / Cu NP/ions	Atomisation spray, thermal nanoimprint	Not reported	99.99% for SARS-CoV-2		[229]
Tetraethoxysilane (TEOS) and Q ₄ N ⁺ -Si(OEt) ₃	QAC	Sol-gel on glass	99.99% E. coli 99.99% S. aureus	Not reported	>85	[216]
Tertiary amine 2-(dimethylamino)ethyl methacrylate on glass	QAC	Atom transfer radical polymerization	99.99% E. coli 99.99% S. aureus	Not reported		[230]

5.2.1 Review of the antimicrobial properties of Copper and copper-based materials

Within the family of AM materials, Cu is registered as a self-sanitizer by the U.S. Environmental Protection Agency (EPA). Furthermore, in 2021 its' antiviral (AV) properties were also recognized after it was proven to inactivate 99.9% of SARS-CoV-2 virus particles within two hours [231]. As such, Cu-based materials have gained popularity in place of Ag-based and polymeric solutions owing to the comparably lower raw material cost and the wide spectrum of AM and AV activity against different species of microbes [108,111,208,212,232–234].

The AM activity of pure Cu/Cu-oxide surfaces is attributed to their ability to release free Cu ions (i.e. Cu⁺ and Cu²⁺) by aqueous corrosion processes [235,236]. The dominant process(es) taking place are determined by the prevailing environmental (e.g. relative humidity, temperature) and chemical conditions (e.g. air constituents, sweat contaminants). Once released, the Cu⁺/Cu²⁺ species exert cytotoxic effects by participating in

Chapter 5 Highly transparent, antimicrobial and durable copper nanostructured surfaces on glass

cyclic redox reactions at the cell surface [237]. For example, charged ions accumulate on the negatively charged domains of the bacterial membrane, altering its permeability and causing leakage of intracellular components [238]. In addition, ion channels within the membrane also permit the transport of ions into bacterial cells where they continue to release ions, which subsequently generate intracellular ROS including hydrogen peroxide (H_2O_2), superoxide ($\text{O}_2^{\bullet-}$), hydroxyl radical ($\bullet\text{OH}$), and singlet oxygen [239]. These species induce oxidative stresses to intracellular components, denature proteins, alter the structure of DNA and de-regulate cellular metabolism [240–243]. A full review of the AM mechanisms of copper-containing surfaces can be found in references [212,244].

This Chapter describes a method of creating transparent AM nanostructured copper coatings (TANCs) on glass substrates. Nine criteria were set out; (1) the coated glass surface must have an AM function that is >99.9% effective against bacteria using the EPA dry test requirement, as described in [Section 5.3.1](#). (2) the coating should be passive, i.e. not requiring additional activation from external sources (e.g. UV light); (3) the Cu release rate should be controlled such that the coating is permanently AM and yet still transparent; (4) the coating should impart the desired AM function without altering the original performance of the substrate; (5) the metallic colour of the Cu film or nanoparticles when deposited on the substrate should not impact the transparency of the original substrate, in particular, the nanostructures should be fabricated in such a way to minimise wavelength dependent light absorption and scattering; (6) The nanostructures must be durable and retain their AM property, after repeated and extended use. Generally, surfaces having nanostructures often lack durability due to the removal of the nanostructures by repeated use (e.g., friction), such as by wiping with a cleaning cloth, frequent contact with a pants pocket or purse during removal and insertion, touching with a human finger, and/or chemical interaction with the environment or cleaning solutions; (7) the coatings should be resistant to oxidation since the oxidation of Cu into CuO_x leads to a lessening of the AM effect; (8) electrically insulating function of touch-activated devices must be maintained; and (9) cover glass for displays is

Chapter 5 Highly transparent, antimicrobial and durable copper nanostructured surfaces on glass

typically thin (<0.5mm in thickness). Herein, 0.3 mm thick ion-exchanged glass was used. This glass is typically used for touchscreen products. The processing temperature must be <400°C, as to avoid affecting the depth of layer or compressive stress characteristics of the glass or ion-exchanged glass.

The copper is obtained on the glass surface in the form of dewetted nanoparticles (DNPs) by an RTA process, described in [Chapter 3, Section 3.3](#). The RTA of the Cu films is performed at low temperature (390°C), i.e. sufficiently close to the critical temperature at above which dewetting of the continuous film is observed and below the glass softening temperature (strain point) of the substrate, to intentionally introduce a degree of inhomogeneity into the contact angle, size and morphology of the particles obtained such that the plasmonic resonance effect on the colouring of the coating is kept within acceptable values. Additional dielectric layers of an inorganic oxide, for example SiO₂, are deposited on top to encapsulate the dewetted particles onto the surface and enhance their durability against the environment, external chemical agents and mechanical forces.

Based on the copper stability, and on the binding interactions between copper and the material of the dielectric layer, the copper release rate can be tuned. The durable transparent antimicrobial nanostructured coating, abbreviated to 'TANC' herein, is presented schematically in [Figure 28](#). It comprises: a transparent substrate (1) upon which an optional titanium adhesion layer is first deposited, a second layer comprising of copper dewetted nanoparticles (Cu DNPs) (2) obtained through metal dewetting and with an average particle size and distribution to obtain high optical transmission, limited haze and colour, a third SiO₂ layer (3) to embed and encapsulate the Cu DNPs to the surface as well as protect the Cu from oxidation. This layer is within approximately 90% of the average particle height of the Cu DNPs. Finally, an anti-fingerprint (AF) Easy-to-Clean (ETC) coating is deposited on top of the embedded Cu DNPs, layer (4).

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

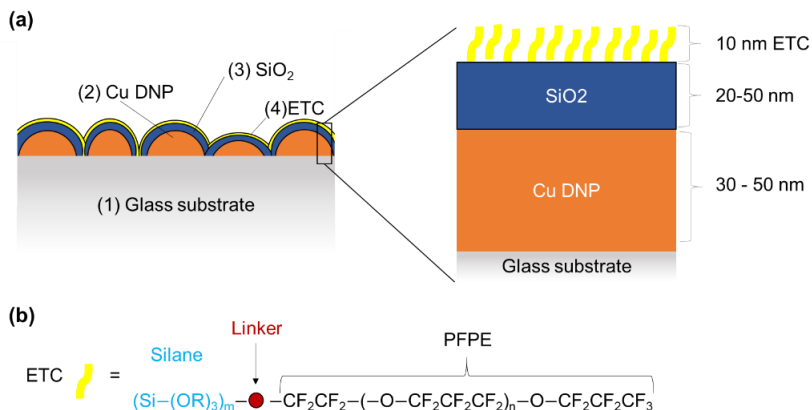


Figure 28 (a) Schematic illustration of the cross section of the TANC comprising 1 the glass substrate with optional adhesion layer, 2 copper or Cu₂O dewetted nanoparticles, 3 inorganic oxide embedding layer and 4 an easy to clean fluorosilane. The variation in contact angle the particle makes with the substrate is shown in the figure together with the related effects on thickness of covering layer. Dimensions are representative but not to scale. Zoomed area shows the cross section of the coating with representative dimensions. (b) General chemical formula of ETC Optool UD509, PFPE-silane monomer, which can have variable number of silane groups, m, and variable length of PFPE chain, n.

The ETC coatings have been adopted by the touch screen and display industries due to their oleophobic, hydrophobic, and excellent wear resistance properties. In this thesis, we selected an ETC from Daikin Chemicals (Optool UD509) due to its high contact angle with water (116°) and low coefficient of friction (COF) (~0.03) [245]. Optool UD509 belongs to the group of high molecular weight alkoxy silane functionalized perfluoropolyether (PFPE) compounds. The general structure, presented in Figure 28b, consists of three parts: i) the silane functional group, ii) the linker 'L' and iii) the PFPE chain. The silane group forms a strong covalent bond with the pre-deposited SiO₂ to create a uniform monolayer of thickness around 10 nm. Meanwhile the PFPE group gives the coating a low surface energy with hydrophobic self-cleaning properties. This property causes the oils and dirt from fingerprints to “bead up,” making it “easy to clean” upon wiping with a dry cloth. The linker has length between 2 - 20nm, to ensure that there is a sufficient distance between the Si atom and the terminal fluorocarbon group, such that water/moisture from the ambient environment can contact the coating and transport Cu ions from the coating to the microbes at the surface.

Being hydrophobic the ETC may also act as a secondary barrier (or blocking layer), slowing the release of copper (since access of water with coating may be reduced) and further improving the durability to prolong the overall longevity of the surface of the AM coating.

5.3 Fabrication of TANCs

The deposition techniques used herein were previously described in [Section 3.2.2](#). Ion-exchanged glass substrates from Corning Incorporated (glass code 2320) with a size of 2x2 inch and 0.3 mm thickness were sonicated in conventional organic solvents for 10 minutes and dried with an N₂ stream. A magnetron sputtering system (ATC Orion 8, AJA International, Inc.) was used for the metal depositions. A pre-deposition cleaning of the substrates was performed by exposing the substrates to an Ar plasma (bias power 40 W, pressure 8 mT, Ar flow 20 ssc/min) for 5 min. An ultrathin titanium (Ti) adhesion layer with a thickness of 2 nm onto the flat glass substrates was deposited from a target of 99.7% purity with a DC power of 100 W and a working pressure of 2 mTorr in an argon atmosphere (20 ssc/min). This was followed by an ultrathin Cu film with a thickness of 3.5 nm as shown in [Figure 29a](#). The Cu film thickness was controlled by the sputtering time. The depositions were performed at a base pressure between about 10⁻⁷ and 10⁻⁸ Torr, room temperature, 100 W of Direct Current (DC) power, and 20 standard cubic centimetres per minute (scc/min) of pure argon (Ar). The working pressure was 1.5 × 10⁻³ Torr, the extrapolated deposition rate was 0.0454 nm/s for Ti and 0.142 nm/s for Cu, and the target–substrate distance was 35 cm with a rotation speed of 60 rpm. To obtain nanoparticles, the samples were subjected to a rapid thermal annealing (RTA) process as shown in [Figure 29b](#). The RTA was carried out in the Tsunami TM RTP-600S system at the temperature of 390 °C, below the glass transition temperature of the substrate, for 600 s. High-purity N₂ gas (1 atm pressure) was used to prevent oxidation of the metal film. After RTA, 10-25 nm of SiO₂ was deposited conformally onto the Cu nanoparticles by using E-beam evaporation system (Lesker LAB 18 Thin Film Deposition System), as shown in [Figure 29c](#). The deposition was performed at a base pressure of about 10⁻⁷ and 10⁻⁸ Torr, room

Chapter 5 Highly transparent, antimicrobial and durable copper nanostructured surfaces on glass

temperature. The SiO₂ E-beam evaporation rate was set to 1 Å/s as measured by a quartz microbalance. Thickness ranged from 0 - 50 nm to provide partial coverage of the nanoparticles whilst allowing optimisation of the durability and AM property of the coating. As a final step, the nanostructured surface was coated with a low surface energy coating, also known as an easy to clean (ETC) coating. Both continuous and patterned ETC coating methods were tested to obtain the best coating performance. Prior to the ETC application, the coated substrates were cleaned with an oxygen plasma of strength between 50-300 W for a time of 2 - 5 minutes. The ETC used was a fluorinated silane (Optool UD509) obtained from Daikin Chemicals. Optool UD509 was diluted to 0.005-0.024 % by weight in a fluorinated solvent (Novec HFE7200, 3M Company) to facilitate application to the surface while also helping to control density, thickness, and morphology of the coating. The ETC was deposited onto the substrate by spray-coating using an airbrush. The airbrush was held 2 inches away from the AM coating and sprayed for 20 seconds to give even coverage. The pressure of the airbrush was varied between 6 to 35 psi. Finally, the ETC was cured at 150°C, <10 min or in a desiccator at room temperature (RT) for 2 days. The curing step is required to adhere the silanes to the coating. The coating was then rinsed or sonicated in fluorinated solvent (Novec™ HFE7200 from 3M Company) for a time of 3-5 minutes to remove any un-reacted but physically adsorbed ETC. In this work, AM efficacy against *S. Aureus* was performed on two sets of TANCS (Set A and Set B), with varying SiO₂ thickness, fluorosilane concentration and oxidation conditions, according to [Table 5](#).

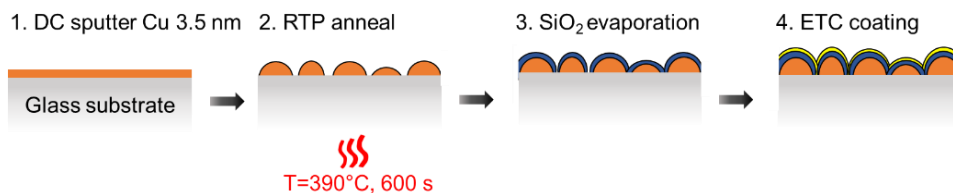


Figure 29) Fabrication of transparent and AM nanostructured Cu surface (TANCS) by (1) DC sputtering of 3.5 nm Cu onto a glass substrate, (2) Low temperature annealing of Cu to form dewetted nanoparticles, (3) Evaporation of an inorganic oxide, e.g. SiO₂, embedding layer and (4) spray coating of a polymer coating, e.g. fluorosilane based easy to clean (ETC). Note that the contact angle the particle makes with the substrate is not representative and varies between 60 -100° typically for low temperature de-wetting processes.

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

Table 5 TANCS coatings (A and B type) together with control (ctrl) samples.

Set	Plasma (Duration / Time)	SiO ₂ (nm)	Fluorosilane concentration %
Ctrl: Uncoated glass	-	-	-
Ctrl: Stainless steel	-	-	-
Ctrl: Cu pure	-	-	-
A	50 W 2min	20 – 25 -30- 35 - 50	0
		20 – 25 -30- 35 - 50	0.012
		35 – 50	0.024
B	300 W 5 min	0 – 10 - 15	0
		15 – 25	0.005
		0 – 10 -15 - 25	0.012
		10 -15	0.024

5.3.1 Antimicrobial (AM) efficacy testing

Bactericidal efficacy testing on the TANCS coatings and stainless steel (SS), uncoated glass and Cu control samples was performed as described in the EPA test for efficacy of Cu alloy surfaces as a sanitizer [246]. Each coupon was tested in duplicate. Prior to AM testing all coupons were cleaned by immersion in a 75% ethanol solution followed by rinsing with deionized (DI) water. The coupons were then sterilized by exposure to UV light at 254 nm, for a duration of 15 minutes. For the preparation of the inoculum, a 20 μL aliquot of thawed bacterial *Staphylococcus aureus* AT 6538 (*S.Aureus*) culture was added to 10 mL Tryptic Soy Broth. The bacterial suspension was incubated at 36 °C for 48 h. The culture was subsequently centrifuged and allowed to settle. The supernatant was removed and pellet was resuspended in 6mL of phosphate buffer saline (PBS). The upper two thirds of the suspension were aspirated and the optical density at 600 nm (OD₆₀₀) was measured to obtain the bacterial density estimation. The cell culture was diluted with PBS to achieve a bacterial inoculum concentration near the target value 1.0×10^6 colony-forming units (CFU) mL^{-1} . Organic soil load containing 250 μL fetal bovine serum (FBS) and 50 μL TritonX was added to 4700 μL of the inoculum to aid in spreading. Each coupon was inoculated with 20 μL of inoculum (Figure 30a). The inoculum volume was spread evenly over a central 1x1 inch test

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

area of the coupon using bent sterile pipette tips. The 20 μL on the coupon typically dried within 5-15 min in ambient conditions. Once dry, the coupons were incubated in a controlled environment set at 42 % relative humidity (RH) and 23 $^{\circ}\text{C}$ for a period of 2 hours. Following the 2-hour exposure period, the coupons were neutralized in Lethen broth (GenLab). Ten-fold serial dilutions of the neutralized solutions were plated using standard spread plate technique on Tryptic Soy Agar plates and incubated for 48 h at 36 $^{\circ}\text{C}$ to yield countable numbers of survivors (approximately 20–200 colonies per plate). This range was selected because below 20 CFUs gives poor counting statistics and above 200 CFUs the bacteria grow too close together.

5.3.2 Calculations of log and percentage of reductions.

The calculation of the value of the AM activity is based on the \log_{10} difference between the mean number of bacteria surviving on the TANCS and the mean number of bacteria surviving on the glass cover slip control samples [246]. Example calculations and all of the raw data are provided in Appendix A.

The experiments were performed in duplicate. First the geometric mean (GeoMean) of the number of organisms surviving on two control surfaces and two TANC surfaces was determined by [Eq. 5.3.1](#):

$$\text{Geo Mean (CFU/mL)} = \left(\frac{\text{Sample1} + \text{Sample2}}{2} \right) \quad (5.3.1)$$

where 'Sample X' represents the number of CFU/carrier on the TANC or control sample.

The log reduction (LR) was calculated by [Eq. 5.3.2](#):

$$\text{LR} = - \text{Log} \left(\frac{\text{Geo Mean of TANC survivors}}{\text{Geo Mean of control survivors}} \right) \quad (5.3.2)$$

The percentage (%) reduction of organisms surviving on the TANC surfaces over organisms surviving on parallel control surfaces was determined by Eq. 5.3.3:

$$\% \text{ reduction} = \left(\frac{\text{Geo mean of control survivors} - \text{Geo mean of TANC survivors}}{\text{Geo mean of control survivors}} \right) \cdot 100 \quad (5.3.3)$$

For the coatings to be approved as a 'self-sanitising', the AM test must demonstrate at least a 3-LR within the specified contact time. This corresponds to a 99.9% reduction in CFUs.

5.3.3 Stipulated wear testing

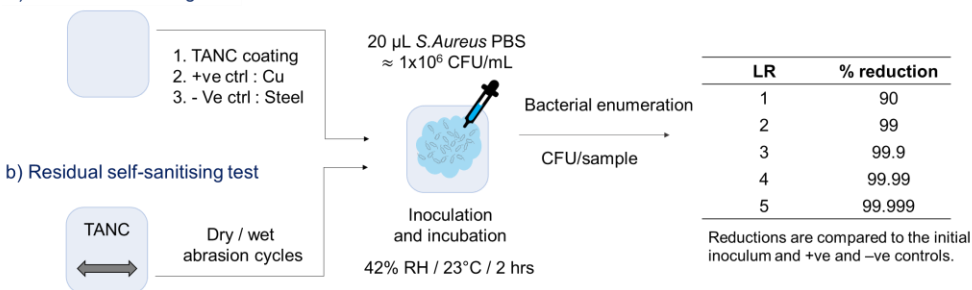
TANCS were subjected to a cleaning regimen suitable for electronic glass display covers based on EPA test method for the efficacy of copper surfaces as a sanitizer [246]. The cleaning regimen was designed to test the durability of the TANCS against abrasion from wiping with a cleaning cloth, frequent contact with a pants pocket or purse during removal and insertion, touching with a human finger, and/or chemical interaction with the environment or cleaning solutions. The abrasion procedures simulate regular touch and a worst-case scenario of 2× cleaning every day for up to 2 years. Simulated wear was performed using an Elcometer 5750 Taber® Linear Abrader, schematically shown in Figure 30b. For wet abrasion, the cleaning solution was prepared with isopropanol (IPA) and deionized (DI) water (70:30). A cloth was saturated with the cleaning solution and attached to the abrader head using double-sided adhesive tape. No additional accessory weights were added to the spline-shaft of the linear abrader (base load of 350 g) in order to keep the pressure similar to that applied by repeated touch or cloth wipes. This process was repeated for a certain number of cycles, such as 700 - 1200 cycles (1400-2400 passes of the wet or dry cloth), to simulate wear and cleaning for up to 2 years.

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

After completion of the wear cycles, the ‘worn’ surfaces were tested for bacterial efficacy against *S.Aureus* using the EPA testing procedure detailed in [Section 5.3.1](#), as well as other optical and water contact angle properties. The “cloth” used in the durability tests is made of a standard material that is typically marketed and sold for use with electronic device touch screens (e.g., BIOPURE™ 70% IPA wipes, or “Just Add Water” personal electronics cloths available from E-CLOTH™), and thus does not readily impart scratches or damage to such a touchscreen surface. The “cloths” can also be the typical disinfecting wipes sold by LYSOL™ and CLOROX™, which are not typically marketed for touchscreen devices but can be used on them without readily imparting scratches or damage. Further information on typical setup conditions for the durability test are as follows: sample size 50 x 50 mm; weight 680 g; stroke length 18 mm; collet 1-inch diameter; speed 40 CPM. In a wet test, four wipes were stacked so as to maintained moisture due to capillary action; however, if wetness dissipated throughout a long (1200 cycle) test, then the used wipes were replaced with new wipes. If desired, for a single durability test that spans several days, the old wipes can be replaced with new wipes every day. It is not believed that the results are affected by using old or new wipes, provided that the moisture condition is maintained (e.g., dry conditions in a dry test and liquid conditions in a liquid test).

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

a) Initial self-sanitising test



(b)

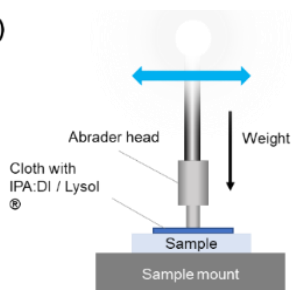


Figure 30 (a) Initial and residual self-sanitising test protocols defined by the EPA for the quantification of the AM efficacy of Cu-containing surfaces. (b) Stipulated wear testing setup for the residual self-sanitising test as described in 5.3.3.

5.3.4 ICP-MS mock testing to determine % of leached copper from TANCS

The number of Cu ions from the coating that equilibrate with those in the liquid inoculum in the AM test was estimated using a mock test that mimics the AM test – the mock test keeps all conditions the same as the AM test (Figure 30a) except the mock test has no bacterium in the inoculum. The control and test coupons are treated with the same cleaning and sterilization process as for the EPA AM test (Section 5.3.1). 20 μL aliquot of inoculum (without bacteria) was added to the central 1 cm^2 area of the TANCS. The leaching was performed in a controlled environment set at 42 % RH and 23 °C for a period of 2 hours. The leachate was collected from the coating by using 2x150 μL of PBS in the exposed 1

inch² region, rinsing and removing the rinse solution into a tube. The amount of Cu in the leached solution was determined using ICP/MS detection. Positive and negative controls were run with pure Cu and stainless-steel coupons, respectively. The optical response of the coating after mock testing in the region 350-750 nm was also obtained.

5.3.5 Morphological, Optical, Mechanical and Antimicrobial Characterizations of the coatings.

The optical transmission spectra of the coatings in the wavelength range 380-750 nm were acquired using a spectrometer (Perkin Elmer LAMBDA 950). All of the reported transmission spectra represent the substrate and coating i.e., bare (uncoated) glass + Ti adhesion layer + dewetted Cu + SiO₂ + fluorosilane. Haze measurements were obtained using a BYK Haze-Guard iPro system. The wetting characteristic of the coated and uncoated substrates was determined by measuring the water contact angle (WCA) using a drop shape analysis system (DSA-100, Krüss GmbH). Five measurements at different points of each sample were taken, and the average and standard deviation reported. Scanning Electron Microscopy (SEM) images were obtained using a FEI-SEM, FEI Inspect F).

5.4 Results and discussion

5.4.1 Morphological, optical and electrical properties

As depicted schematically in [Figure 31](#), the size and morphology of the Cu DNPs can be quite varied, due to the low temperature conditions of the dewetting process and thin precursor copper film. In [Chapter 3, Section 3.3](#), a theoretical modelling of the low temperature dewetting together with a comparison of the simulated and experimental optical spectra provided insight into the advantage of low temperature dewetting for obtaining highly transmissive Cu DNP surfaces.

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

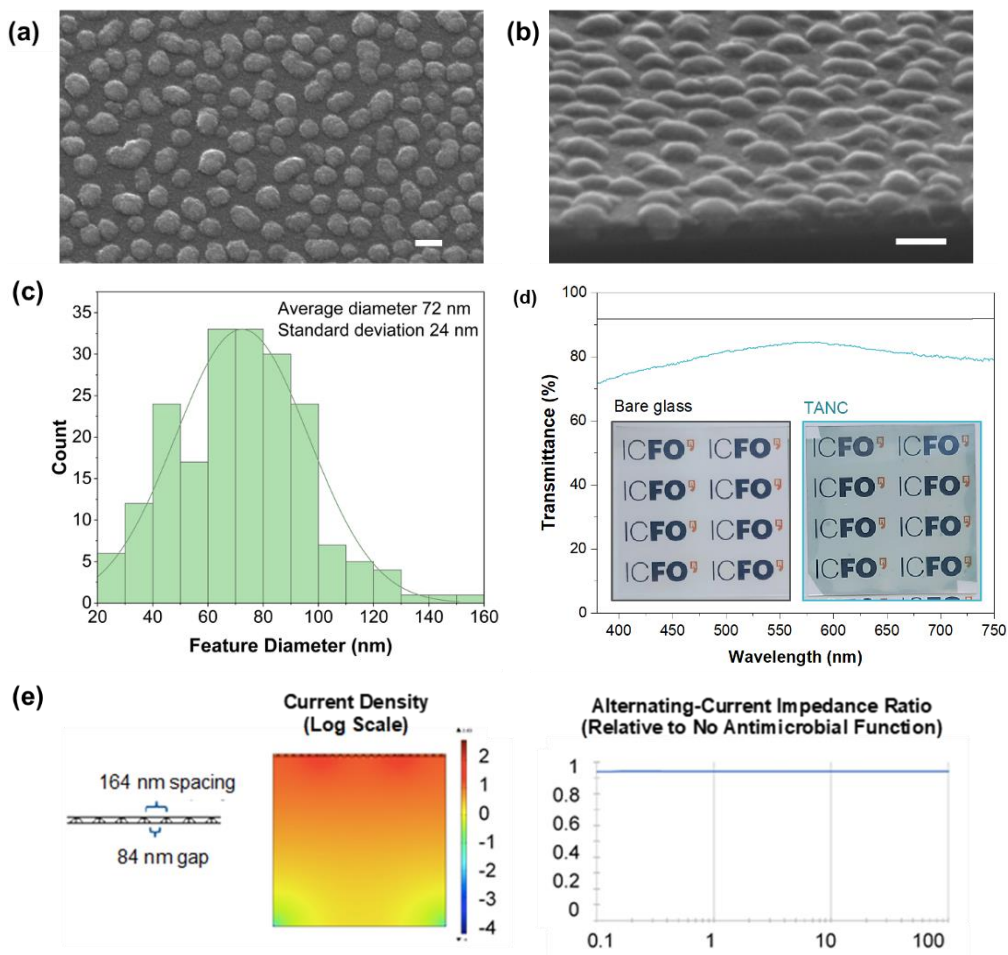


Figure 31 Top down (a) and side on (b) SEM micrographs of TANCS coatings. The parameters of the SEM scan are as follows. HV 15.00 kV; det ETD; magnification 160,000x; WD 9.9 mm; spot 3.0; tilt 0° (a). tilt -15°(b). The scale bar is 500 nm; (c) Particle size distribution analysis using ImageJ); (d) Transmission spectra of representative TANC (blue line) as compared to the uncoated bare glass substrate (black line). Inset shows photographs of bare glass (left) and TANCs (right); (e) Finite Element Model Prediction for TANCS obtained from 3.5 nm Cu UTMF. The graph shows the alternating-current impedance ratio of an TANC in accordance with one aspect relative to an otherwise identical bare glass substrate. The lateral-surface impedance predictions demonstrate that capacitive touch performance can coexist with this dewetting antimicrobial process.

The shape of the Cu DNPs (a and b) varies from flat hill to spherical-like. In some instances, particles are interconnected while others are separated up to around 60 nm. The average diameter and standard deviation is 72

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

nm \pm 24. Likewise, the average particle height was 64 ± 20 nm and average contact angle was $35^\circ \pm 12^\circ$. Note that in the case where the particle is non-spherical the diameter refers to the longest lateral edge to edge distance of the feature. The average of the longest lateral dimension is calculated using ImageJ [120] by measuring a representative number of Cu DNPs and averaging the result on a numbers basis. "Average height" was also calculated by measuring a representative number of Cu DNPs and averaging the result on a numbers basis.

The large dispersion of particle size and shape and interparticle distance induces a broadening and softening of the plasmonic resonance. The broadening of the resonance gives the coating a transparency without strong dependence on wavelength and the also leads to low scattering (haze) $> 1\%$. Thus, the TANCS remain visually close to the neutral colour of the substrate and have a transmission between 70-80% that is almost independent of wavelength in the visible range. The inset photograph in Figure 31d demonstrates the visual appearance is such that the functionality of touchscreen devices would be retained

Furthermore, product modelling for capacitive touch devices was performed for the Cu DNPs using the Finite Element Model, Figure 31e. The results are for Finite Element Model Predictions for the dewetting case that result in Cu DNPs with a 164 nm spacing and 84 nm gap, based on the SEM analysis. The graph shows the alternating-current impedance ratio of a TANC in accordance with one aspect relative to an otherwise identical bare glass substrate. The predictions show that TANCs do not impact the frequency dependence of the surface-lateral electrical impedance in the 1MHz to 100MHz frequency range required by touch-enabled devices, indicating that the TANCs surfaces would retain touch screen functionality.

5.4.2 AM activity of TANCS

Mock and AM testing was performed on TANCs, whose conditions are presented in Table 5. Note that the mock tests are performed without bacteria for the reason that it is difficult to run safe measurements with

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

microorganisms. Though we cannot conclude whether the presence of the microorganism would alter the rate of Cu dissolution, we assume that the main driver is the PBS solution and that any additional effect that the microorganism may have would not be significant by comparison. In other words, the rate of Cu dissolution due to the PBS >>> rate of consumption of Cu due to the presence of microorganisms. It is also important to acknowledge that the results presented herein should be interpreted with consideration of their processing conditions. Standardized test conditions were provided by the EPA, which is used by the majority of manufacturers for determining the antimicrobial activity of Cu-containing surfaces. The conditions of the test are very much more invasive with respect to the real-world environment, utilising a wet inoculum and elevated temperature and humidity, and as such, it does not guarantee efficacy *in situ* where conditions may differ. In fact, it is generally accepted that AM surfaces under wet conditions perform better due to accelerated rate of Cu dissolution [247–249]. It may also be that the salts contained within the buffer may complex with the ‘free’ Cu ions and reduce their bioavailability to the bacteria thereby suppressing the toxic effects of metal excess [250]. Future work should also consider ‘dry testing’ approaches to better emulate the real working conditions [251].

A practical requirement for touchscreen application is the ability to continually release Cu in optimal concentrations over a long period of time without compromising the overall transparency, durability, and functionality of the coating. [Figure 32](#) plots the data of LR from AM test against the data of Cu leaching from the mock test. The LR correlates positively with the amount of Cu leached into the solution up to ~4 mg/L after which increased Cu dissolution does not significantly increase the LR. By this, the minimum inhibitory concentration of Cu (MIC-Cu) needed in solution to reach the EPA requirement of 3-LR, equivalent to 99.9% kill, was determined to be ~2 mg/L. The bacterial killing mechanism could be explained by diffusion of mobile Cu ions through the SiO₂ and fluorosilane capping layers to the coating’s surface where they interact with and kill the suspended/floating microbes. The diffusion of Cu ions is mediated by a liquid vehicle - e.g. cleaning solvents, surface moisture or the PBS solution hosting the bacteria. Based on a MIC-Cu of ~2mg/L and,

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

assuming a uniform distribution of microorganisms in the fluid, the number of ions, n , available to each microorganism is estimated to be on the order of 10^{11} . This is orders of magnitude over the natural intracellular concentration of Cu atoms/ions in *S. Aureus*, which is reported to be in the region of 10^4 to 10^5 [252]. Therefore, it is reasonable to assume that TANCS impose their AM activity by releasing Cu in sufficient concentrations for these specific bacteria.

For assessment of the optical properties, the transmission of the coatings in the visible region was measured before and after mock testing. [Figure 32b](#) shows the optical spectra and photographs corresponding to TANCS leaching <2 mg/L Cu (squares) and >4 mg/L Cu (circles). Both cases show an increase in transmission after mock testing in the region of the plasmonic resonance associated with the Cu DNPs. This can be explained by reduced plasmonic coupling, as Cu dissolves into solution, the DNPs decrease in dimensions, reducing the interactions that give rise to plasmonic coupling.

The distinction between Set A and B lies in the strength and duration of oxygen plasma cleaning treatment prior to the fluorosilane application. Set A TANCS were treated with 50W for 2 minutes whilst Set B were treated with 300 W for 5 minutes (Table 5). The inset photographs in (b) show prototypical examples of TANCS from both sets after mock testing where the marked central region denotes the mock testing area. A distinction in the color of the central region after mock testing is observed where Set B maintains a color close to the original coating whilst Set A has a more evident color loss. The release of Cu species into the PBS droplet, is influenced by the Cu solubility within the coating. It is likely that the different oxygen plasma treatment supports the difference in the leaching data between Set A and B TANCS.

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

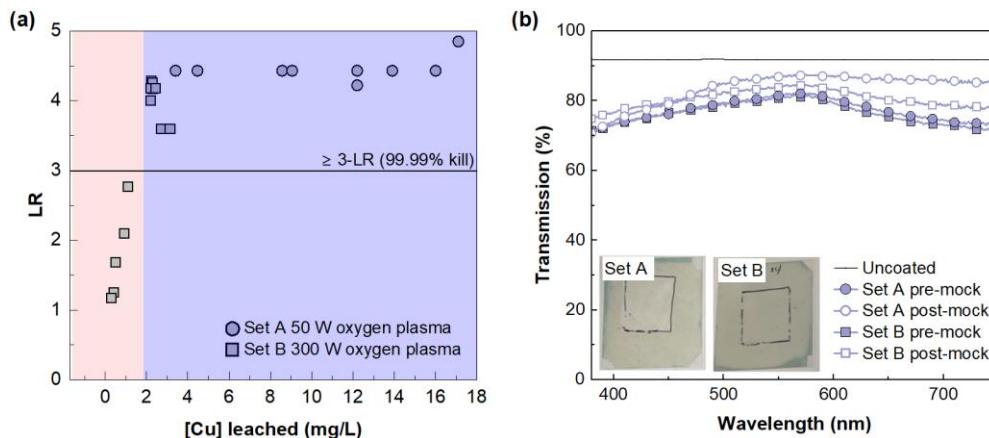


Figure 32 (a) LR vs [Cu] leached. The EPA-prescribed 3-LR, corresponding to >99.99% reduction in bacterial colony counts, is marked with a black line. The blue and pink shaded regions correspond to the [Cu] concentration range above and below which a 3-LR was observed, respectively. *The comparison between LR and [Cu] leached assumes that the majority of the ions are held in the liquid phase and not consumed by the microorganisms i.e. rate of Cu dissolution due to the PBS \gg rate of consumption of Cu due to the presence of microorganisms. (b) Transmission spectra of representative TANCS. For both graphs, the circle and square markers represent TANCS from sets A and B, respectively. Inset of (b) shows photographs of Set A and Set B after mock testing where the marked central region shows the testing area.

It is evident from the plot in [Figure 32a](#) that some of the TANCS in [Table 5](#) leach Cu excessively above the MIC-Cu determined to be ~ 2 mg/L. From a coating longevity point of view, excessive Cu leaching is undesirable. In cases where [Cu] leached \gg MIC-Cu, we propose that the Cu is being released in a burst like manner. The migration of chloride ions into the TANC facilitates the fast generation of Cu ions such that the effect of the SiO₂ thickness is masked. To combat this and increase the longevity of the TANCS, we increased both the fluorosilane concentration and the SiO₂ thickness in order to control the rate of Cu dissolution.

The results are presented in [Figure 33](#) which plots the LR from the AM test and [Cu] leached during the mock test vs. SiO₂ thickness and fluorosilane concentration for TANCS treated with (a) 50 W and (b) 300 W oxygen plasma. First, we observe that Set A TANCS leached up to 4 times more Cu than Set B for the same SiO₂ thickness and flurosilane concentration. The lower Cu dissolution rate in Set B is likely due to a higher (300 W) oxygen plasma treatment that may have partially oxidized the underlying Cu,

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

thereby reducing its solubility. Second, we note that all TANCS from Set A demonstrated a >4-LR in the AM test irrespective of SiO₂ thickness, except with the 0.024 % fluorosilane coated TANCS, where the LR and [Cu] leached scaled with SiO₂ thickness concentration. The same trend was observed in Set B TANCS, though, the effect of SiO₂ thickness was also observed for the lower (0.012%) fluorosilane concentration. It is likely that for TANCS with high concentration fluorosilane high oxygen plasma treatment (Set B), the migration of chloride into the TANCS is reduced and the burst release mechanism is suppressed. In such a way, a method of controlling the Cu dissolution to within the optimal range above MIC-Cu is demonstrated. Overall, a combination of SiO₂ thickness, fluorosilane concentration and oxidation of the underlying Cu is required to achieve the optimal Cu release and LR.

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

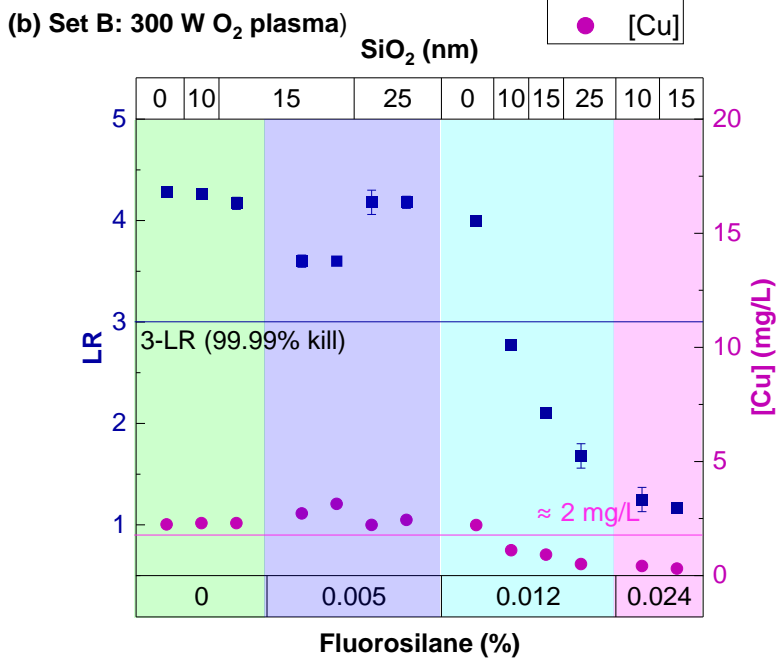
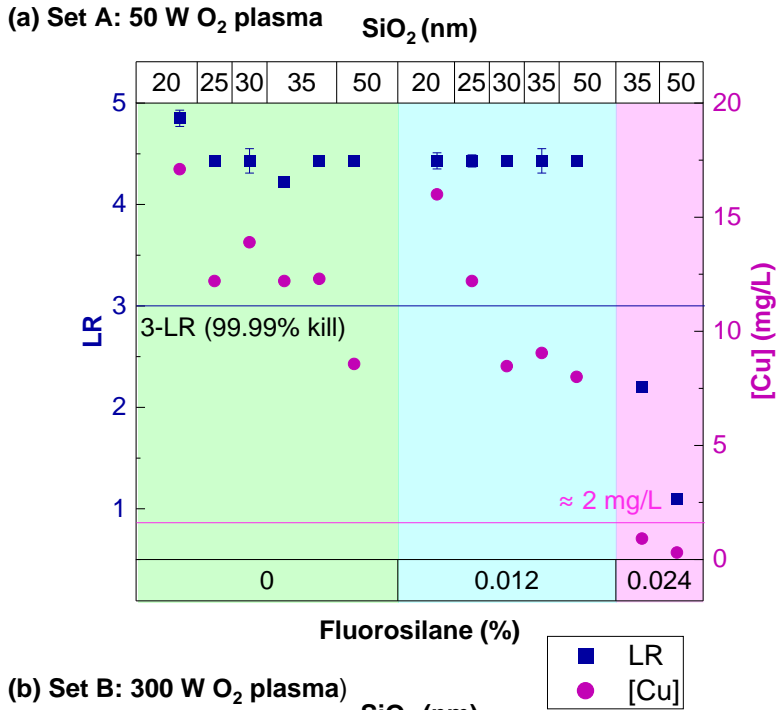


Figure 33 Plots of LR and [Cu] leached as a function of SiO₂ thickness and fluorosilane concentration for (a) 50 W and (b) 300 W oxygen plasma treated TANCS. Error bars represent the standard deviation of two samples. Note that in some cases, the error bar is smaller than the marker and not visible

Chapter 5 Highly transparent, antimicrobial and durable copper nano-structured surfaces on glass

Finally, WCA of the coatings before and after AM testing. The ETC coating imparts a contact angle $>90^\circ$ and changes by less than 5% after the AM test. [Table 6](#) shows that for the selected embodiments of Set A, after AM testing, the change in water contact angle of the antimicrobial article surface varies by less than 5% from the initial contact angle value of the coating measured before testing. For other samples, the variation is as low as 3% or less than 1%. The results of the AM testing illustrate good performance of the AM surface in terms of retaining a high-water contact angle.

Table 6 Water contact angle (WCA) of Set A TANCS before and after AM testing.

Sample ID	SiO ₂ (nm)	Conditions	Mean WCA before EPA test (°)	SDev. (°)	Mean WCA after EPA test (°)	SDev. (°)
Ctrl Glass coverslip	-	-				
Ctrl Steel	-	-				
Cu metal	-	-				
1-A	20	As rcd	59	3.2	56	7.4
2-A	25	As rcd	61	1.3	58	1.6
3-A	30	As rcd	49	4.8	51	3.2
4-A	35	As rcd	37	3.6	30	6.5
5-A	50	As rcd	42	2.1	40	2.4
6-A	20	0.012 % ETC	110	1.9	98	2.9
7-A	25	0.012 % ETC	107	4.3	97	1.5
8-A	30	0.012 % ETC	101	5.7	95	1.9
9-A	35	0.012 % ETC	107	4.3	102	1.6
10-A	50	0.012 % ETC	108	2.7	99	1.8
11-A	35	0.024 % ETC	118	0.4	119	0.1
12-A	50	0.024 % ETC	120	0.8	116	1.0

“WCA” is contact angle; “SDev.” is standard deviation. The contact angle was measured at five locations and averaged.

5.5 AM durability

Touchscreens are continuously exposed to various types of contact and wear. Therefore, durability and resistance to general wear and tear is an important reliability feature for AM coatings. Durability against wiping and cleaning as prescribed by European Centre for Disease Prevention and Control (ECDC) guidelines for infection control, was tested by subjecting the TANCS to the equivalent of up to 2 years of wear (see methods [Section 5.3.3](#)) and then testing their AM, optical and wetting properties. Identical TANCs (each with 25 nm SiO₂ and 0.012% fluorosilane) were fabricated. The first sample was immediately AM tested, and the second sample was AM tested after 730 or 1200 abrasion cycles with a Lysol® or IPA impregnated scouring pad on the coating surface, respectively. The results are presented in [Figure 34](#). All TANCs demonstrated a > 3-LR against *S. Aureus* even after abrasion testing. The TANCs also maintained their wetting and optical characteristics post-abrasion, revealing a less than 5% average gain in transmission and between 10-15% reduction in contact angle with respect to the initial value. The maintenance of the high WCA, demonstrates that the fluorosilane is a robust topcoat that does not degrade with repeated wiping. Overall, the results of the abrasion testing suggest that the embedded Cu DNPs are reasonably durable in terms of retaining AM activity, optical properties and high-WCA (>90).

Chapter 5 Highly transparent, antimicrobial and durable copper nanostructured surfaces on glass

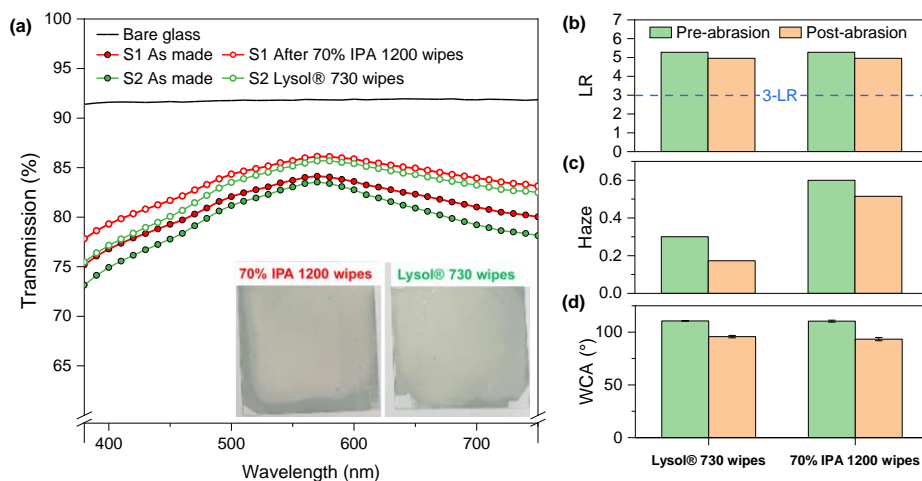


Figure 34 (a) Transmission, (b) LR, (c) Haze and (d) WCA of TANCS before and after wet abrasion testing with IPA (1200 wipes) and Lysol® (730 wipes). The inset of (a) shows the TANCS after wet abrasion testing on the central region. The visual appearance of the central wiping region remains close in color to the outer region, indicating a good durability of the coating to repeated wipes with cleaning sanitizers.

5.6 Conclusion

This work incorporates Cu DNPs into a transparent and AM nanostructured Cu surface (TANCS) for glass substrates. The TANCS demonstrated a > 99.9% effectiveness against *S. Aureus*, and have a colour-neutral optical transparency between 70-80% in the region 380-750 nm. Moreover, the TANCS are easy to clean and retain their AM efficacy, optical and wetting properties even after durability testing. In addition, they are fabricated in a way that is industrially scalable. The proposed AM TANCS may be useful in applications of technological interest such as multi-user transparent touch activated surfaces.

Chapter 6

Conclusions & Outlook

6.1 Conclusions

Ultrathin materials and nano-structures are key elements in developing multifunctional transparent surfaces. Combining optically transparent substrates with ultrathin materials with advanced functionalities, such as antimicrobial or electrically conducting could have a significant impact in multiple applications, including display screens, transparent solar cells and transparent antimicrobial coatings. This thesis has been focused on the development of low temperature growth and processing of ultrathin and nanostructured materials to create transparent multifunctional surfaces for optoelectronic and biological applications through easy to implement, scalable methods. The main achievements of this thesis are summarised by its objectives:

Objective 1: Develop scalable techniques to transfer 2D materials, such as graphene, MoS₂ and nanostructured metals onto transparent flexible substrates at low temperatures

- Chapter 3 demonstrated a simple and fast technique to obtain high thermal processing materials and nano-structures on low strain-point flexible substrates. The method utilises water-soluble polished salt substrates, a well-known material that can stand the high temperatures involved during the growth, and can provide a fast and clean transfer onto the flexible target substrate due to the

easy dissolution of the salt in water. Moreover, employing salt as a sacrificial substrate avoids the detrimental effects of harsh-etchant based transfer processes.

- The use of NaCl salt substrates for the material growth and transfer was verified, for the first time, with two prototypical materials, dewetted gold nano-particles and MoS₂. The method demonstrated preservation of coverage and structural quality of both materials after transfer to PET substrates. The proposed method offers universal applicability for various 2D materials and nanostructures, supporting polymers, and final substrates, thus facilitating the easy fabrication of flexible 2D material-based electronics and optoelectronics.

Objective 2: Find the optimum substrate-graphene combination for increasing doping and the electrical conductivity of transparent surfaces.

- The development of a method of obtaining a highly transparent conductive surface of graphene on an ion-exchanged glass was demonstrated in Chapter 4. Specifically, an n-doping in the order of -10^{13} to -10^{14} cm⁻² was obtained. Such high n-doping levels in graphene originating from the interaction with the substrate underneath have never been observed before.

Objective 3: Use ultrathin metals and subsequent nanostructuring for increasing the antimicrobial activity of transparent surfaces

- The development and optimisation of novel, Cu-nanoparticle-based antimicrobial coatings on glass that are transparent, durable and retain their antimicrobial efficacy, optical, electrical, and wetting properties after regular and repeated use over a long period of time, whilst also being fabricated in a way that is industrially scalable, was demonstrated in Chapter 5. Furthermore, unlike traditional high temperature sintering and ion-exchange techniques, the AM coatings presented in this thesis are fabricated using low temperature techniques compatible with a wider range

of technologically relevant substrates, for example, cover glass for display modules. Thus, the approach demonstrates the potential to address one of the largest sources of fomite-driven nosocomial infections, namely displays and other surfaces requiring transparency and electrical/ capacitance activity.

6.2 Outlook

The methods developed in this thesis represent a significant stepping stone towards the implementation of nanostructured and ultrathin materials on low thermal budget transparent substrates for applications such as transparent conductors and antimicrobial coatings for glass. Nevertheless, further developments will be necessary to achieve practical implementation.

The demonstrated proof-of-concept growth and transfer technique using NaCl ([Chapter 3](#)) could easily be extended to other 2D materials, heterostructures and nanostructures, as well as alternative water-soluble crystalline growth substrates, such as ZnO for a wide range of applications, including advanced electronic and optoelectronic devices.

As for the graphene/IOX systems, whilst a substantial increase in the graphene surface potential (-1.61 eV) and about a factor of 10 decrease in sheet resistance was demonstrated ([Chapter 4](#)), the sheet resistance gradually increased by about 40% after exposure to ambient conditions. This doping instability is considered as one of the biggest challenges to realizing the practical applications of transparent graphene electrodes. With this in mind, it would be promising to pursue methods of improving the doping stability over time, with, for example, the use of alternative encapsulation techniques. Secondly, whilst it is clear that the IOX glass is a key element to achieve doping, additional experiments with other modified glasses would be needed to confirm the doping mechanism and the interplay between the processing steps to make the devices.

With these developments, the graphene/IOX system demonstrates potential to realize a host of previously inaccessible applications including low cost, compact photonic devices operating in the NIR/VIS wavelength range and low work function transparent electrodes for energy conversion and electron emission applications such as OLED, LEDs, solar cell, and touchscreen applications. One area to explore could be subsequent nanostructuring into, for example, nanodisk or nanoribbon geometries, for making plasmonic sensing devices operating in the near-infrared region.

Finally, this thesis demonstrated a novel method to achieve durable transparent antimicrobial surfaces. One challenge when using Cu-based nanostructures as high-touch surfaces is the oxidation, corrosion and aging of the surface. Since the oxidation of copper(0) or copper(I) oxide into copper(II) oxide has a lessening effect on the antimicrobial action of a surface, strategies that minimise the oxidation of Cu should be explored. One line of investigation, for example, could involve dewetting UTMFs of a Cu-Zn alloy. Another inquiry, aimed at facilitating practical applications, could be a systematic exploration of the antimicrobial functionality of TANCs during indoor atmospheric exposure conditions, including factors such as deposited sweat and cyclic wet/dry air conditions.

Broader questions remain over the antimicrobial mechanism(s) of metallic species, especially for such instances as those in Chapter 5, where the mechanism likely involves a complex interplay between the surface feature shape, size and geometry as well the inherent antimicrobial nature of both Cu and Cu oxides. In this regard, studies further examining the survival of bacteria as a function of measured surface oxidation and wettability would prove vital in understanding the role of the bacteria/surface interaction.

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APPENDIX

A

Table 7 Staphylococcus aureus CFU results for Set A and B **Figure 32** and **Figure 33**

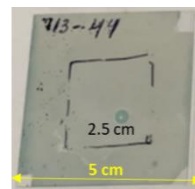
Sample ID	SiO ₂ (nm)	Conditions	GeoMean (CFU/ml)	Standard Deviation	LR
Ctrl Glass coverslip	-	-	5.22 x10 ⁵	1.4 x10 ⁵	-
Ctrl Steel	-	-	5.37 x10 ⁵	1.6 x10 ⁵	-0.01
Cu metal	-	-	20	0	4.42
SET A (50 W O₂ Plasma, 2 minutes)					
1-A	20	As rcd	20	0	4.42
2-A	25	As rcd	20	0	4.42
3-A	30	As rcd	20	0	4.42
4-A	35	As rcd	20	0	4.42
5-A	50	As rcd	20	0	4.42
6-A	20	0.012 % ETC	20	0	4.42
7-A	25	0.012 % ETC	20	0	4.42
8-A	30	0.012 % ETC	20	0	4.42
9-A	35	0.012 % ETC	20	0	4.42
10-A	50	0.012 % ETC	6.32	4.24	3.92
11-A	35	0.024 % ETC	1650	0	2.50
12-A	50	0.024 % ETC	4.15 x10 ⁴	0	1.10
SET B (300 W O₂ Plasma, 5 minutes)					
1-B	0	As rcd	27.4	0	4.28
2-B	10	As rcd	28.7	0	4.26
3-B	15	As rcd	35.3	0	4.17
4-B	15	0.005 % ETC	131	0	3.6
5-B	25	0.005 % ETC	34.5	0	4.18
6-B	0	0.012 % ETC	52.2	0	4
7-B	10	0.012 % ETC	886	0	2.77
8-B	15	0.012 % ETC	4150	0	2.1
9-B	25	0.012 % ETC	1.09 x10 ⁴	0	1.68
10-B	10	0.024 % ETC	2.94 x10 ⁴	0	1.25
11-B	15	0.024 % ETC	3.53 x10 ⁴	0	1.17

Appendix

AM calculations

The inoculum has a concentration of 5.22×10^5 CFU/ml = 522 CFU/ μ L

If 20 μ L of inoculum is used for each coupon it gives $20 \times 522 = 10440$ CFUs per coupon



$$\begin{aligned}\text{Volume of Cu in test area} &= \text{Test area} \times \text{thickness of Cu deposited} \\ &= 2.5 \text{ cm}^2 \times 3.5 \times 10^{-7} \text{ cm} \\ &= 8.75 \times 10^{-7} \text{ cm}^3 \text{ of Cu}\end{aligned}$$

$$\begin{aligned}\text{Total Mass of Cu in test area} &= \text{density of Cu} \times \text{volume of Cu} \\ &= 8.96 \text{ g/cm}^3 \times 8.75 \times 10^{-7} \text{ cm}^3 \\ &= 7.84 \times 10^{-6} \text{ g Cu per coupon}\end{aligned}$$

Inductively coupled mass spectroscopy (ICP-MS) results

Procedure:

1. 20 μ L of PBS was pipetted onto the test area of 2.5 cm².
2. After 2 hours 2 \times 150 μ L of PBS was used to wash the leachate from the coating.
3. The total Cu content in the leachate and wash (total volume of 320 μ L) was determined by ICP-MS.

Calculation of mass of Cu in leachate and % Cu leached:

$$\text{Mass (g) of Cu in leachate} = \frac{c}{v} \quad (\text{Eq. 1})$$

c is [Cu] in g/L

v is total volume (L) (leachate + wash = 20 μ L + 300 μ L)

$$\% \text{ Cu mass leached} = 100 * \left(\frac{\text{Cu mass in leachate}}{\text{Total Cu mass deposited}} \right) \quad (\text{Eq. 2})$$

Appendix

Example 1 : 50 nm SiO₂ + ETC (S_1123) 3.41 ppm (mg/L) Cu ions released into 320μL PBS gives:

$$\text{Mass} = 0.00341 \text{ g/L} \times 320 \times 10^{-6} \text{ L} = 1.09 \times 10^{-6} \text{ g of Cu}$$

$$\% \text{ mass leached} = 100 * (1.09 \times 10^{-6} \text{ g} / 7.84 \times 10^{-6} \text{ g}) = 13.9 \%$$

Example 2: 25 nm SiO₂ + ETC (S_1096): 12.9 ppm (mg/L) Cu ions released into 320μL PBS:

$$\text{Mass} = 0.0129 \text{ g/L} \times 320 \times 10^{-6} \text{ L} = 4.13 \times 10^{-6} \text{ g of Cu}$$

$$\% \text{ mass leached} = 100 * (4.13 \times 10^{-6} \text{ g} / 7.84 \times 10^{-6} \text{ g}) = 52.7\%$$

Example 3: 20 nm SiO₂ + ETC (S_1101) 16 ppm (mg/L) Cu ions released into 320μL PBS gives

$$\text{Mass} = 0.016 \text{ g/L} \times 320 \times 10^{-6} \text{ L} = 5.12 \times 10^{-6} \text{ g of Cu}$$

$$\% \text{ mass leached} = 100 * (5.12 \times 10^{-6} \text{ g} / 7.84 \times 10^{-6} \text{ g}) = 65.1\%$$

AM efficacy calculations:

Example Sample 6-A:

Geo Mean of glass coverslip control survivors = control glass = 5.22×10^5

Geo Mean of TANC survivors = 20

$$LR_{\text{TANC}} = \text{Log} \left(\frac{5.22 \times 10^5}{20} \right) = 4.42$$

$$\% \text{ reduction} = \left(\frac{5.22 \times 10^5 - 20}{5.22 \times 10^5} \right) \times 100 = 99.99\%$$

